



Design and Manufacturing of a DTL prototype power coupler

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Abstract

The design and manufacturing of a 1 MW RF power coupler intended for the CERN Linac4 drift tube linac (DTL) prototype has been undertaken within the HIPPI framework. This HIPPI note summarizes the RF and thermo-mechanical design, describes the mechanical structure and reviews the results achieved at the end of this HIPPI task.

Introduction

The design and manufacturing of a 1 MW RF power coupler intended for the CERN Linac4 drift tube linac (DTL) has been undertaken within the HIPPI framework. This HIPPI note summarizes the RF and thermo-mechanical design, describes the mechanical structure and reviews the results achieved at the end of this HIPPI task.

RF Design

The RF design is based on a short circuited waveguide with a coupling iris connecting the waveguide to the accelerator cavity. The advantage of this design compared to other solutions is the ability to change the coupling constant by changing the length of the RF short circuit. The critical parameters of this design are the size of the coupling iris and the distance of the waveguide to the accelerator cavity.

The RF design has been done using HFSS simulations. In these simulations, the geometry was reduced to a half cell of the problem and the full DTL tank was accounted for by estimating the corresponding external Q value from the Q value of the full structure. The parameters have then been optimized in order to find the required Q value.

The dependency of the external Q value on the short circuit position was calculated as well as the frequency shift corresponding to a certain Q value. These parameters are required for the cavity design and the tuning of the coupler in the final installation. The power dissipation in the waveguide and the coupling iris has been estimated in two extreme cases and serves as a basis for the thermo-mechanical design.

The RF design of the DTL coupler has been done by Pierre-Emmanuel Bernaudin from CEA, Saclay [1].

Thermo-mechanical Design

Following the RF design, the cooling pipes have been dimensioned according to the heat loss distribution found for 15% duty cycle at 1 MW of RF power. The total power to be absorbed is found to be 255 W in the connecting guide and 44 W in the waveguide flange. Two cooling pipes are therefore foreseen on the connecting waveguide, another cooling pipe has to be placed in the waveguide flange, and further two cooling pipes are attached to either wide side of the wave guide. The cooling pipes have a diameter of 10 mm and provide for water cooling at a flow speed of 2 m/s corresponding to a flow of 9.4 l/min. The corresponding heat transfer coefficient is $10 \text{ kW/(m}^2 \text{-} \text{K})$.

The waveguide, flange and connecting guide have been simulated thermo-mechanically using a finite element method (FEM) and taking the heat transfer to the water into account. The resulting stresses and deformations have been analyzed in detail including the 1 bar pressure difference due to evacuation of the coupler. The mechanical structure consists of stainless steel sheets of 6 mm thickness which are reinforced by the flanges and fins providing the required stiffness of the structure.

The base temperature of the water is set to 25° C and the maximum temperature in the connecting guide is found to be 48° C. Von Mises stresses were found to be lower than 100 MPa except in small areas of stress concentration. Deformations remain below 0.1 mm in the flange area of the connecting guide which is acceptable with respect to the Helicoflex vacuum joint requirements and below 0.3 mm on the wave-guide structure.

The thermo-mechanical design has been undertaken at the LPSC, Grenoble [2].

Construction

Based on the RF and thermo-mechanical design studies, the manufacturing drawings of the DTL coupler have been prepared. The wave-guide including a connecting flange and a short circuit plus an additional short circuit plate for tuning the coupling factor has been constructed by LPSC, Grenoble during the year 2006.



Figure 1: DTL coupler wave-guide with cooling circuits and vacuum flange sections.

Figure 1 shows the WR2300 half-height wave-guide with a vacuum flange that will be connected to the RF window providing for the vacuum to atmospheric pressure transition. On the right hand-side the flange to the connecting wave-guide section can be seen featuring a cooling circuit. At the rear end of the wave-guide structure, a short-circuit is connected to the wave guide. Fins on the broad face of the wave guide provide for the mechanical strength and rigidity that is required to stand the atmospheric pressure against the vacuum inside the wave-guide. The whole structure is assembled from stainless steel sheets of 6 mm thickness by welding. A copper cooling pipe on the broad face of the wave guide was soldered to the stainless steel wave-guide to provide for cooling.

The DTL coupler has been finished and delivered to CERN in November 2007. Tests at high RF power will take place only after delivery at CERN of the prototype drift tube linac structure being built by the Russian institute VNIIEF, which is currently delayed by about 18 months. Shortly before installation, the DTL coupler shall be copper plated.

Acknowledgements

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References

[1] P.-E. Bernaudin, "RF design of a DTL power coupler", CARE/HIPPI Document-2005-002

[2] E. Vernay, J.-M. De Conto, D. Bondoux, "Thermomechanical study of the HIPPI/LINAC4 DTL coupling port. Results for the 'connecting guide' part.", CARE/HIPPI Document-2005-010

ANNEXES: Drawings











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CERTIFICAT DE TEST D'ETANCHEITE A L'HELIUM

Date; 16/11/2006	ate ;	16/11/2006
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Commande LSPC

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Client SMGOP 5 rue P Valerien Perrin ZI La Tuilerie 381701 SEYSSINET-PARISET

Détection : global - au jet

Signal de tolérance : 1.10-10 Atm.cm3/8.He

 Désignation
 Nº Plan
 Résultais obtenus
 Observations

 Port de couplage
 3.10-9 Atm.cm 3/sec
 BON

Valeur de la fuite étalon : 1-10-7 Atm.cm3/sec +10%

Controleur : Yves MEYRIEUX-BOURG

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