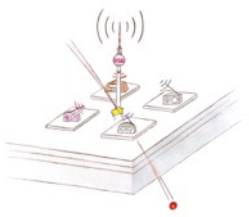


The “1 μm ” project



Resistive Read-out in Silicon Detector offers the possibility to reach unprecedented position resolution using large pixels and thin sensors

- Impact parameter resolution, sensor accuracy, material budget
- Requests at future colliders
- Resistive readout in silicon detectors
- Charge sharing: RSD main formula
- Reconstruction method
- Results: laser, beam test → All results obtained using RSD1 from FBK
- Read-out electronics
- Application of Machine learning algorithms
- Future directions
- Publications, contributors
- Extra topics (not for the presentation)



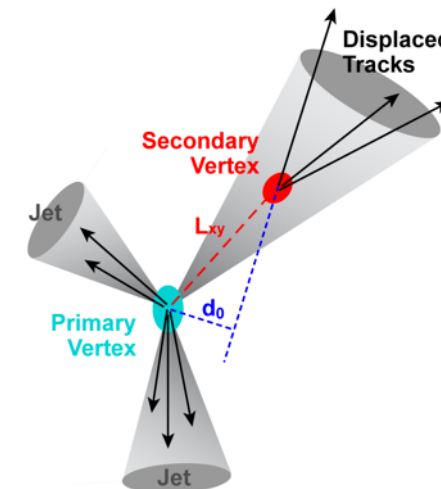


Impact parameter resolution in silicon detector



The capability of distinguishing secondary vertexes is often expressed by the impact parameter resolution σ_{d_0}

$$\sigma_{d_0}^2 = \sigma_{Geom}^2 + \sigma_{MS}^2$$



The geometrical precision σ_{Geom} depends on the **accuracy of the single sensor** σ_x

- First layer as close as possible to the beam line
- Last layer as far as possible
- **Smallest possible σ_x : very accurate sensors**

The average multiple scattering σ_{MS} depends on the material budget of the sensors and services

- Low mass beam pipe
- Place services far away
- **Smallest possible σ_{MS} : very thin sensors**

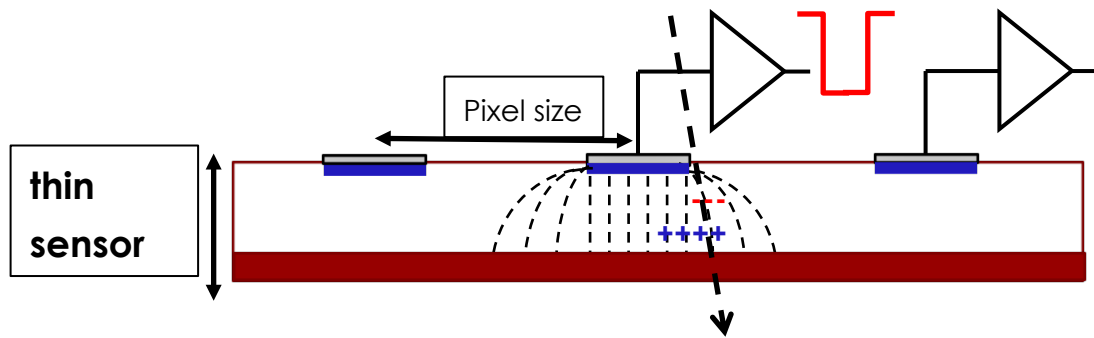
The sensors need to be very accurate and very thin

Sensor accuracy σ_x and readout



Binary readout

where the only information is hit/miss (0,1)



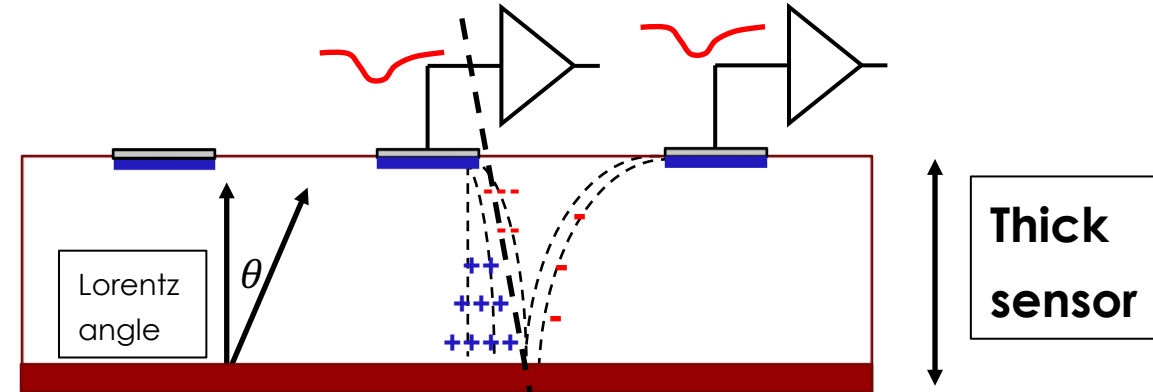
$$\sigma_x = k \frac{\text{pitch}}{\sqrt{12}}, k \sim 0.5 - 1$$

- σ_x depend on the pixel size
pixel = 100 μm \rightarrow $\sigma_x = 20 \mu\text{m}$
- σ_{MS} small : sensors might be thin

Thin, NOT accurate

Analog readout

where the amplitude of the signal is recorded

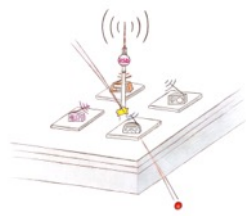


$$x_i = \frac{A_i x_i}{\sum_1^2 A_l x_l}$$

- $\sigma_x \ll$ pixel size
- σ_{MS} large
Sensors have to be thick to maintain efficiency
- Need B field (or floating electrodes)

Accurate, NOT thin

The sensors are either very accurate OR very thin



Request at future accelerators

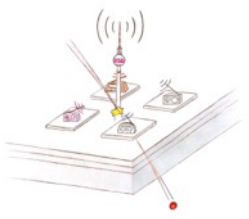
Facility:	FCC-ee	ILC	CLIC
σ_x [μm]	~ 5	< 3	< 3
Thickness of tracker material [μm of Si]	~ 100	~ 100	~ 100
Hit rate [$10^6/\text{s}/\text{cm}^2$]	~ 20	~ 0.2	1
Power dissipation [W/cm^2]	0.1 – 0.2	0.1	0.1
Pixel size [μm^2]	25 x 25	25 x 25	25 x 25

$\sigma_x = 5 \mu\text{m}$ && $\sigma_{MS} \sim 100 \mu\text{m}$ && *air cooled*

Very difficult to achieve

- tiny pixels with binary readout: technologically very difficult (power, bumps, services)
Monolithic (MAPS...)?
- The reason for small pixels is the position accuracy not occupancy → almost empty detector

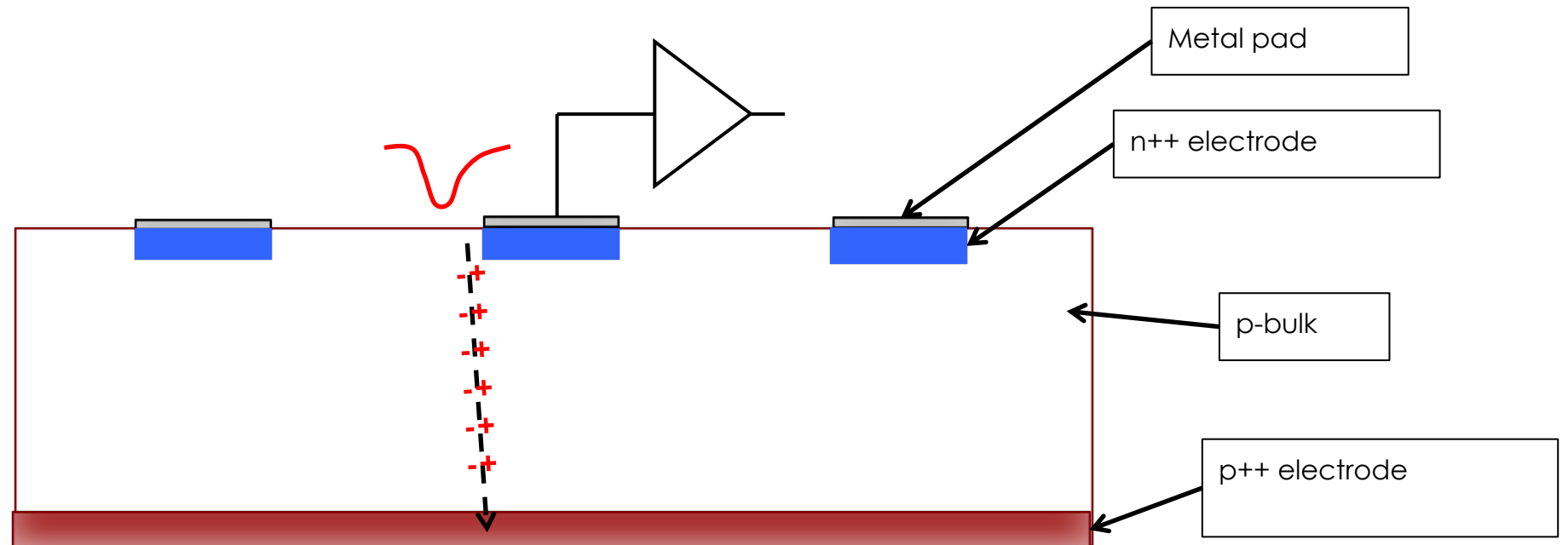
Good temporal resolution is also very challenging with so many pixels and not enough power

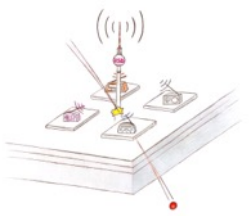


Signal formation in DC-coupled silicon sensor



The e/h are drifting, producing direct charge induction in the n++ layer (Ramo's theorem)

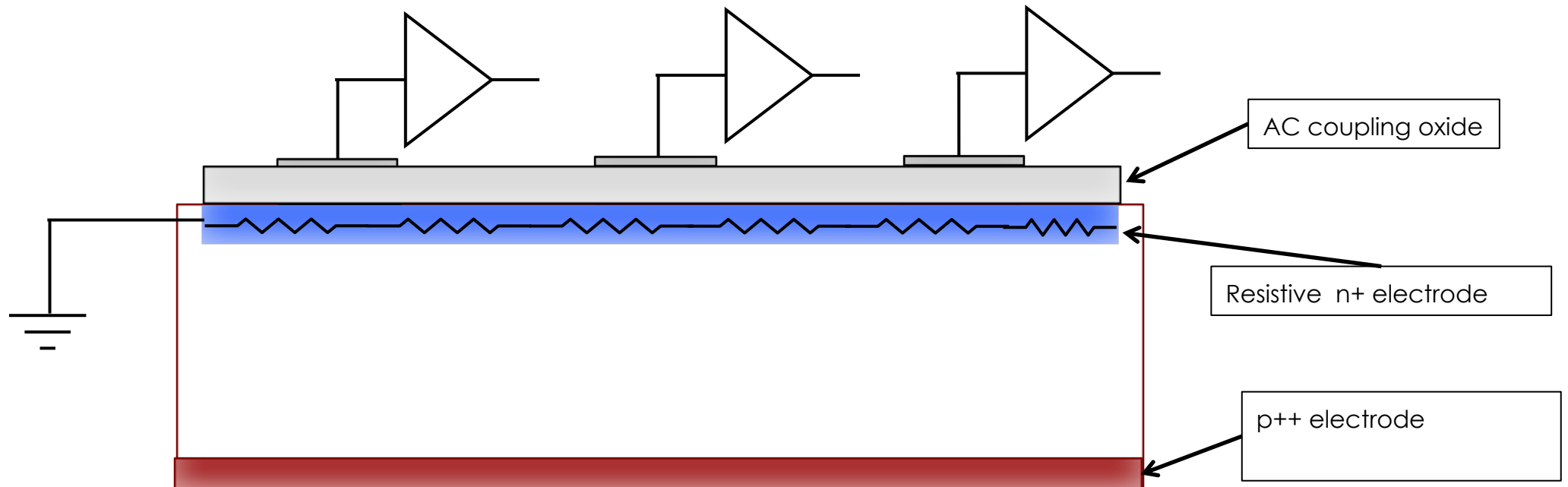




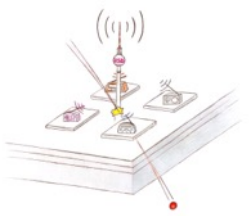
Resistive readout



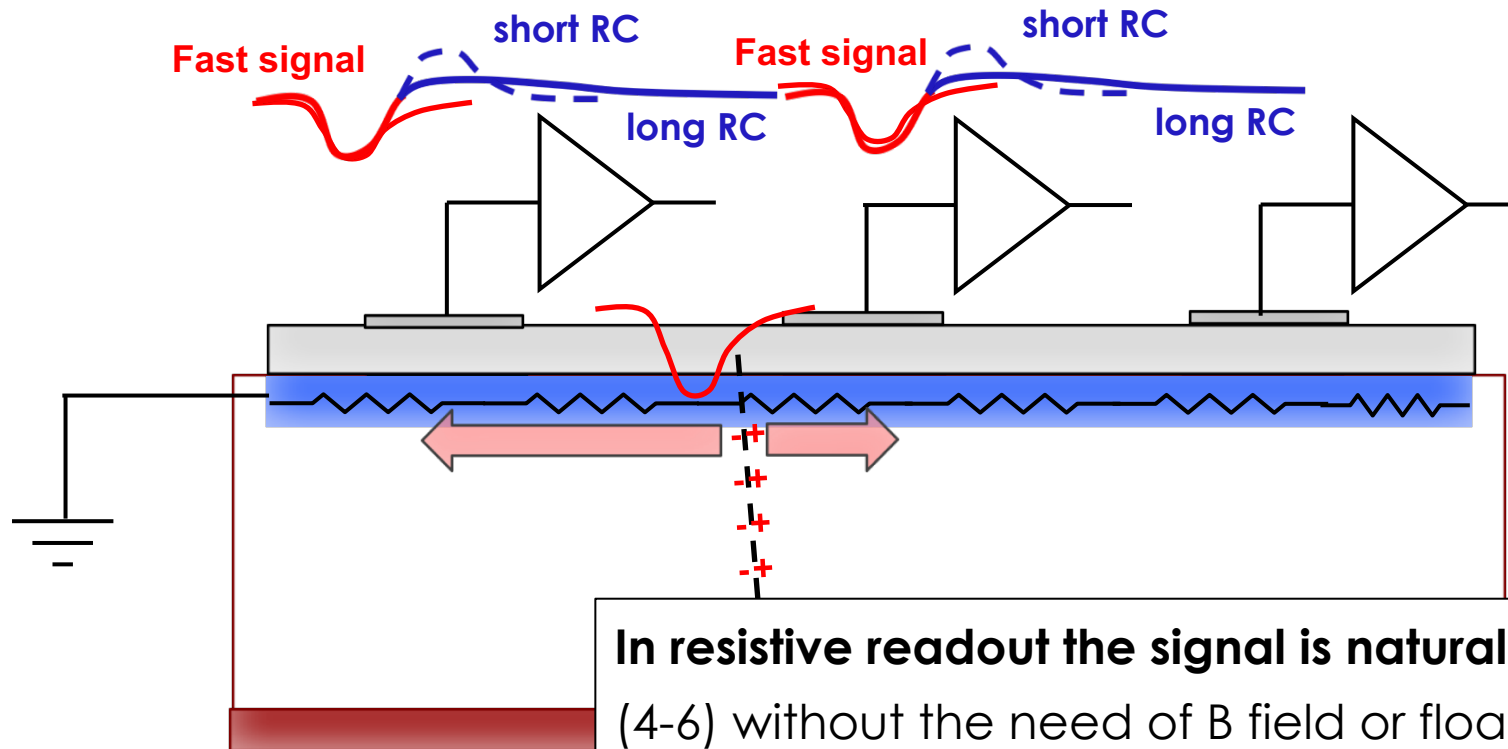
- 1) Extended the n++ electrode over the whole Si surface
- 2) Make the n++ electrode resistive \rightarrow n+
- 3) Add AC-coupling readout



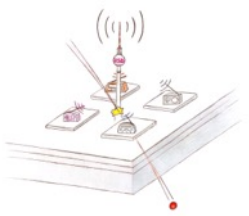
Signal formation in resistive readout



- The signal is formed on the n+ electrode ==> no signal on the AC pads
- The AC pads offer the smallest impedance to ground for the fast signal
- The signal discharges to ground



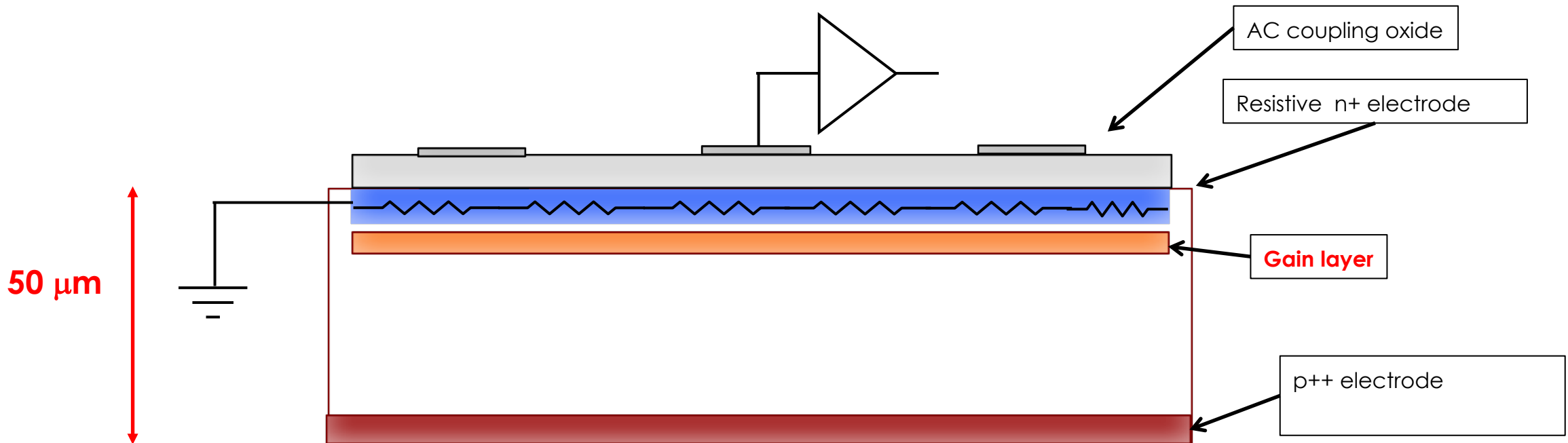
In resistive readout the signal is naturally shared among pads (4-6) without the need of B field or floating pads
Problem: sharing a small signal leads to inefficiency



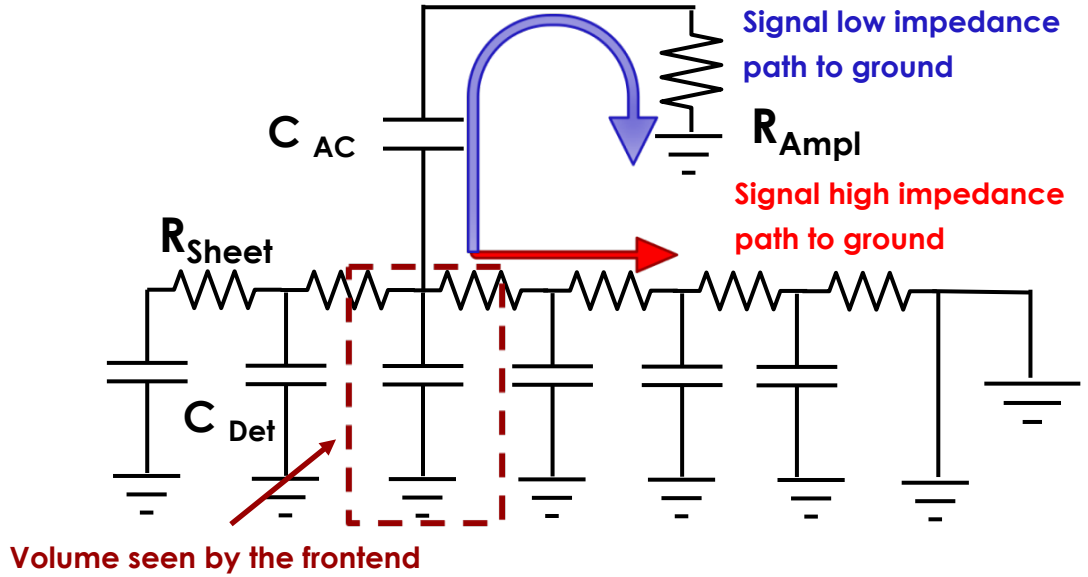
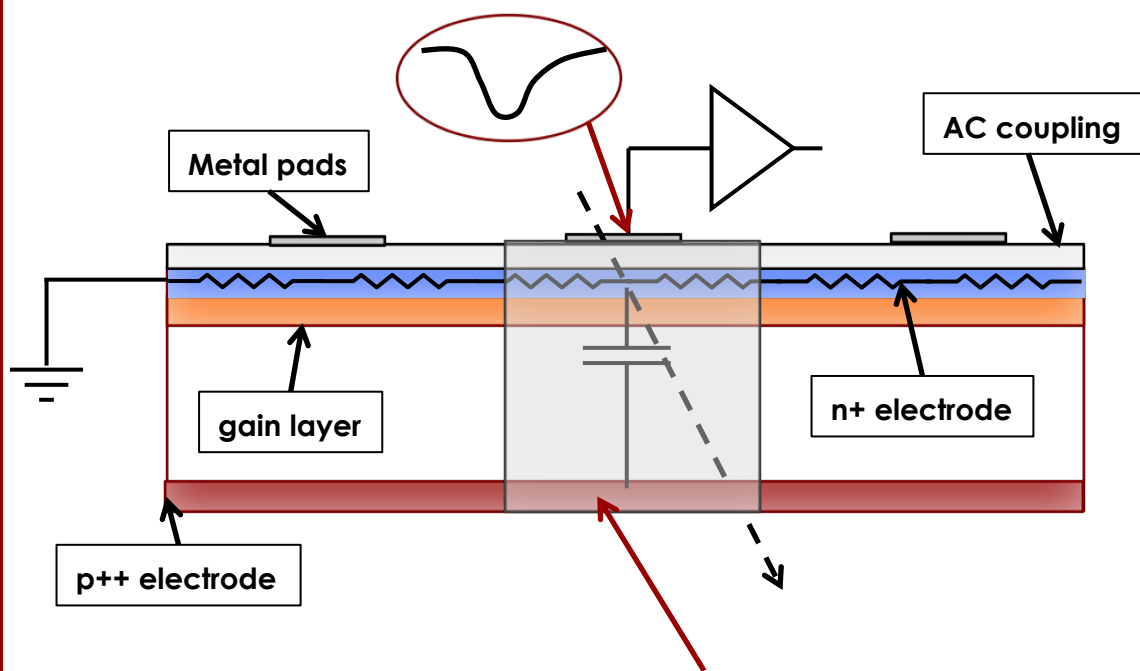
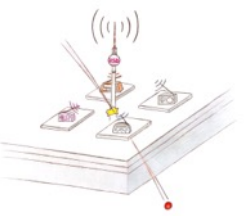
Combining internal sharing and internal gain



- 1) Extended the n^{++} electrode over the whole Si surface
- 2) Make the n^{++} electrode resistive $\rightarrow n^{+}$
- 3) Add AC-coupling readout
- 4) Add internal gain to maintain 100% efficiency even with signal sharing
- 5) Make the sensor thin to reduce material budget and enhance timing performance

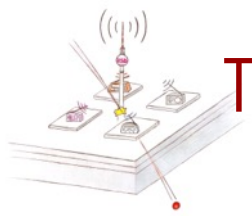


Resistive readout: why does it work?

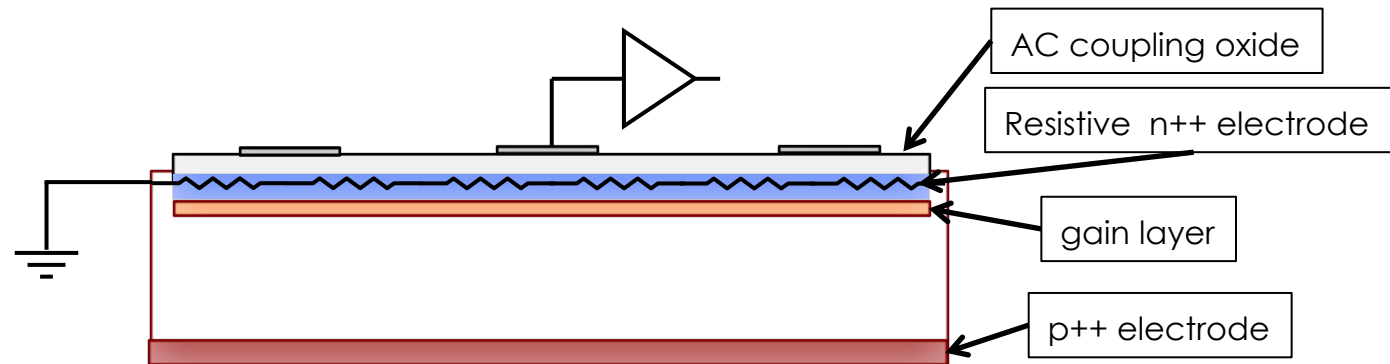


The resistive n+ electrode limits the geometrical volume seen by the read-out: given the high frequencies involved, the capacitive path to ground is more favorable than the resistive path

- Rather small capacitance: $\frac{1}{C_{Tot}} = \frac{1}{C_{AC}} + \frac{1}{C_{Det}} \sim \frac{1}{C_{Det}}$
- The AC pad discharge time is: $R_{Sheet} * C_{AC} \sim 2 \text{ k}\Omega * 3 \text{ pF} \sim 4 \text{ ns}$
- The signal rise time is increased by: $R_{Ampl} * C_{Det} \sim 100 \Omega * 1 \text{ pF} \sim 100 \text{ ps}$



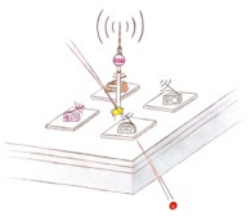
Timeline of the Resistive readout sensor: AC – LGAD / RSD



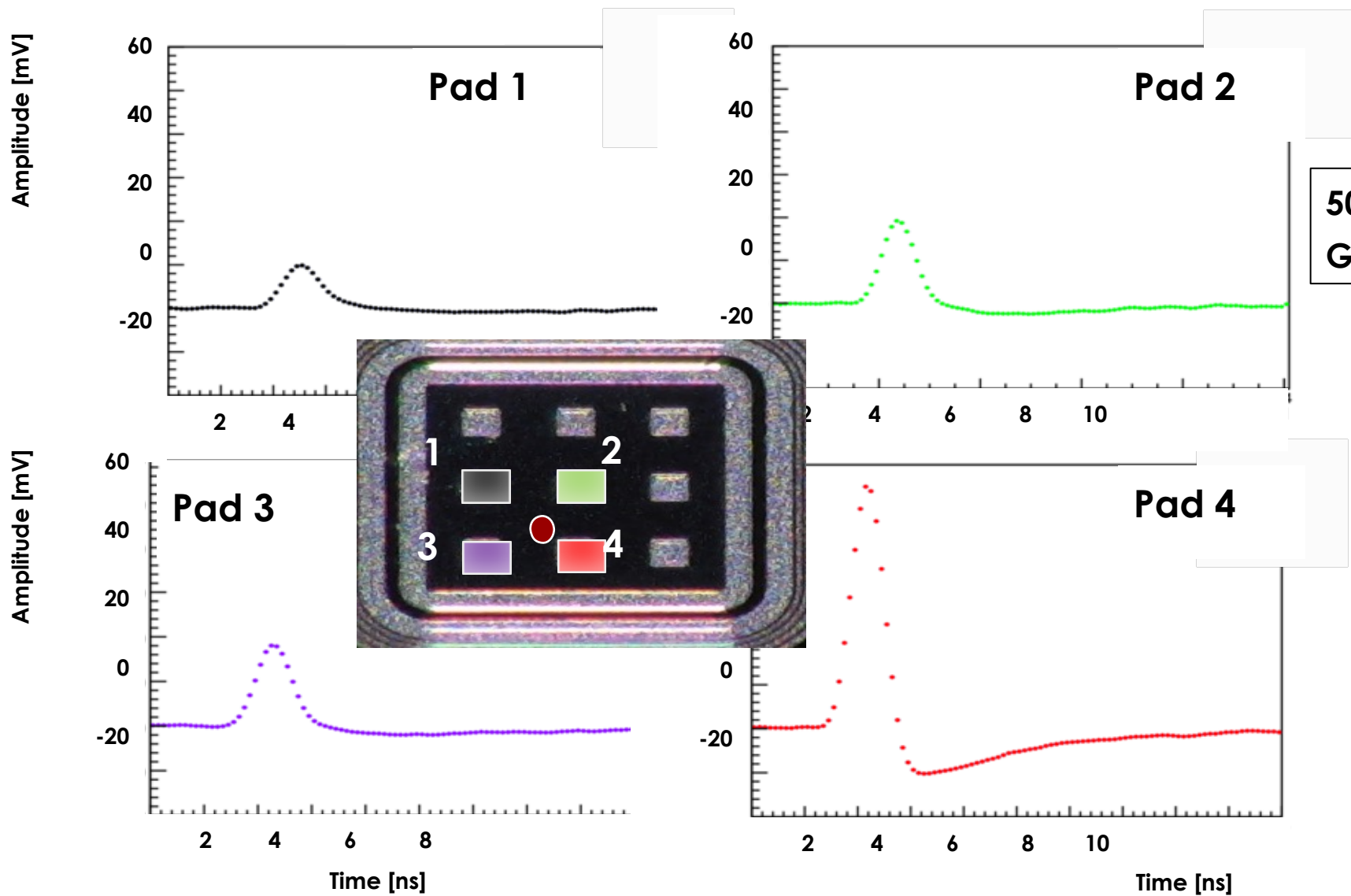
These sensors enjoy a double name: the **key technological features** are the “**resistive n+ layer**”, necessary to produce the local AC coupling, and **gain** to avoid inefficiency and allow small material budget.

AC-LGAD (AC-coupled Low-Gain Avalanche Diode) or **RSD** (Resistive Silicon Detector).

- AC-LGAD were proposed at the TREDI 2015 conference [1].
- The sensors presented here are manufactured at FBK within the RSD project (INFN) [2],[3].
- CNM produced AC-LGAD sensors in 2017 [4]
- BNL produced AC-LGAD in 2019 [5].
- Results shown from beamtest are from [6]
- The application of Machine Learning is [7]
- First results on AC-LGAD strips at beam test [8]



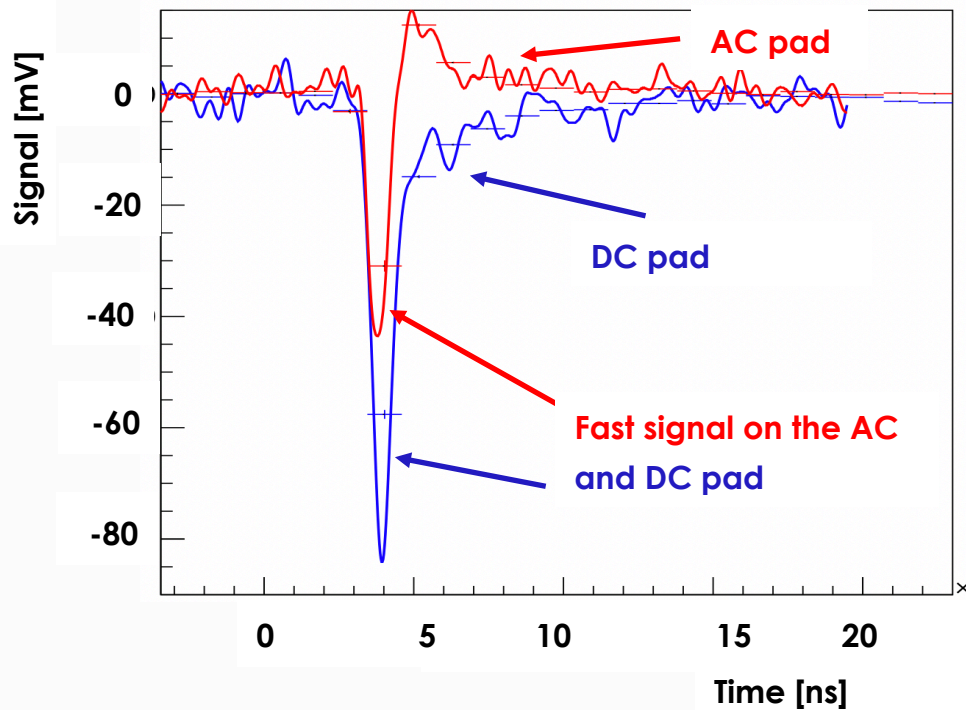
Example of signal sharing



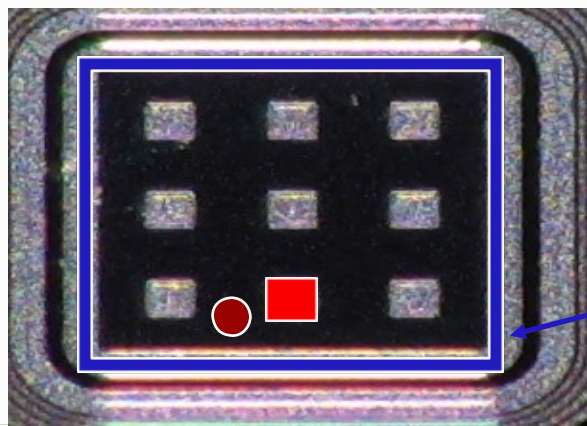
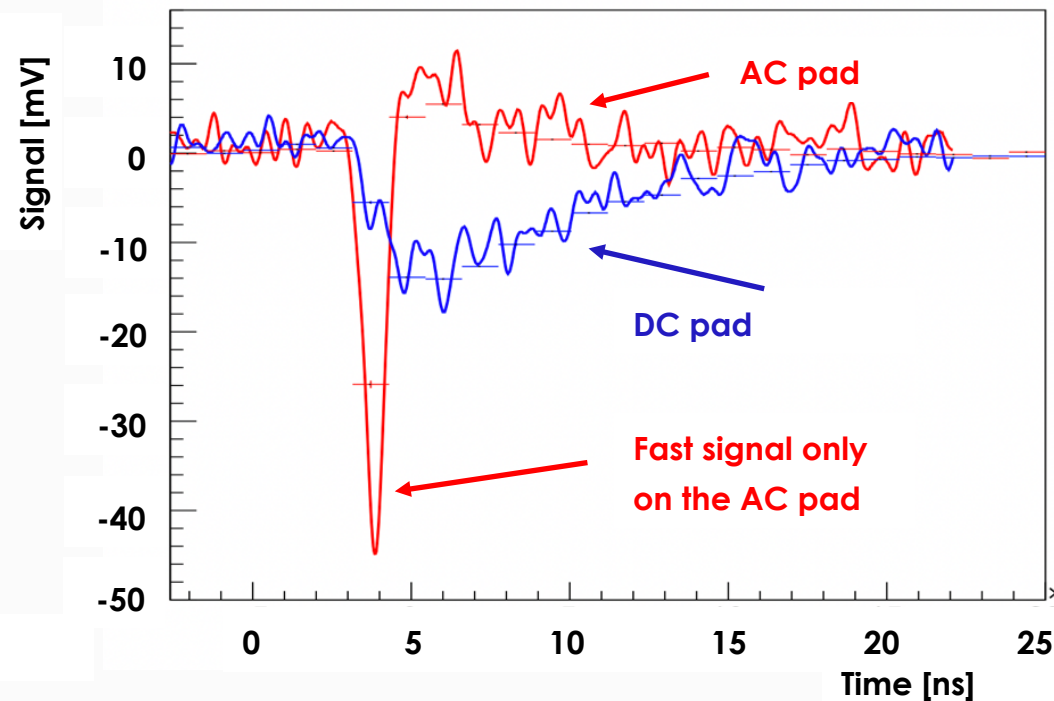
50-mm thick RSD,
Gain ~ 20

The laser is shot at the position of the red dot: the signal is seen in 4 pads

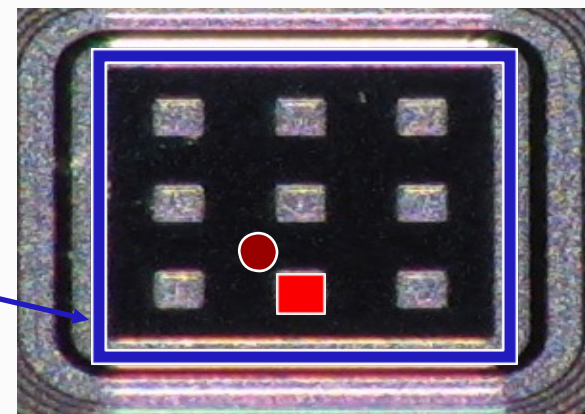
Particle impact point in the outer sensor region

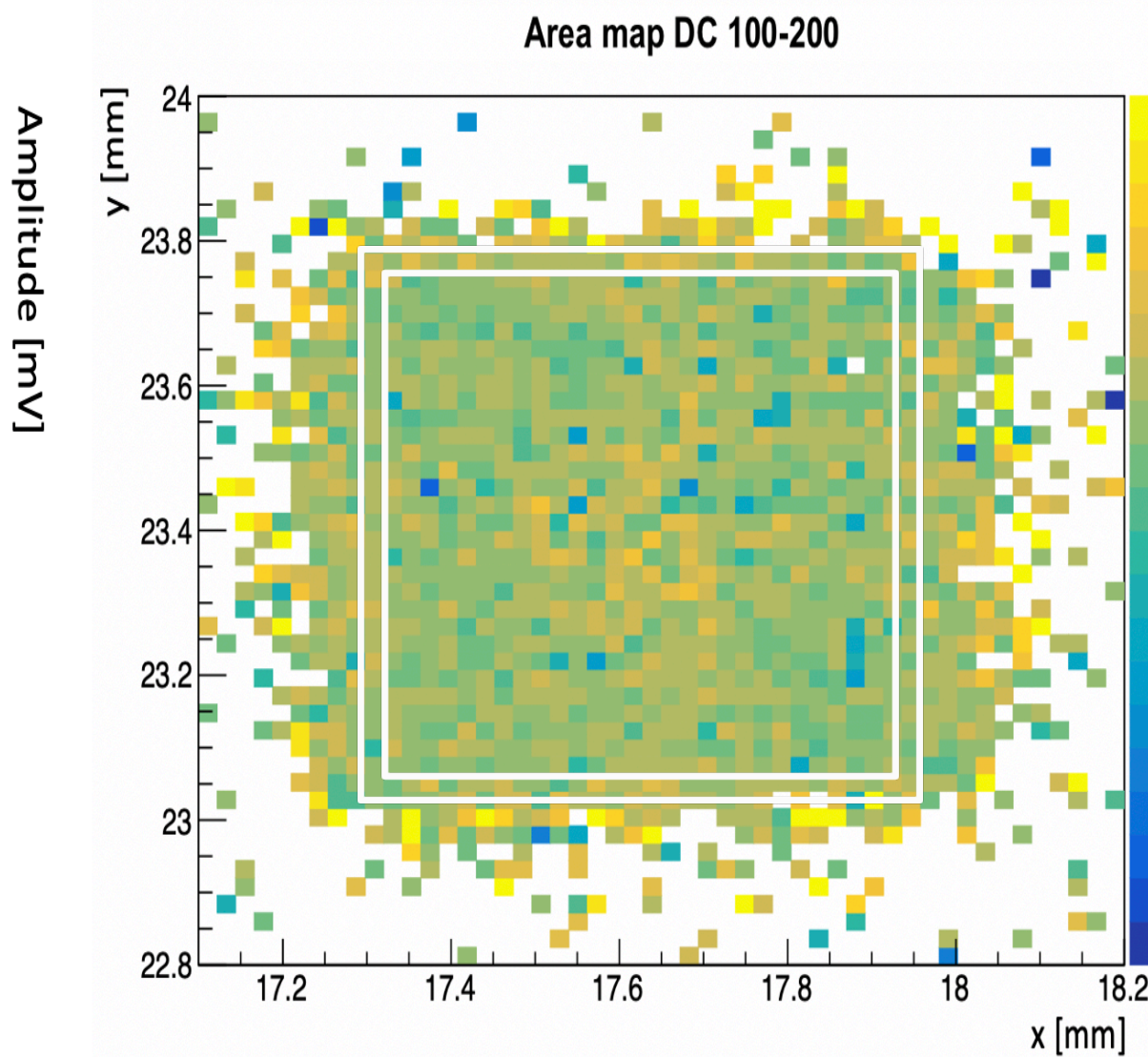
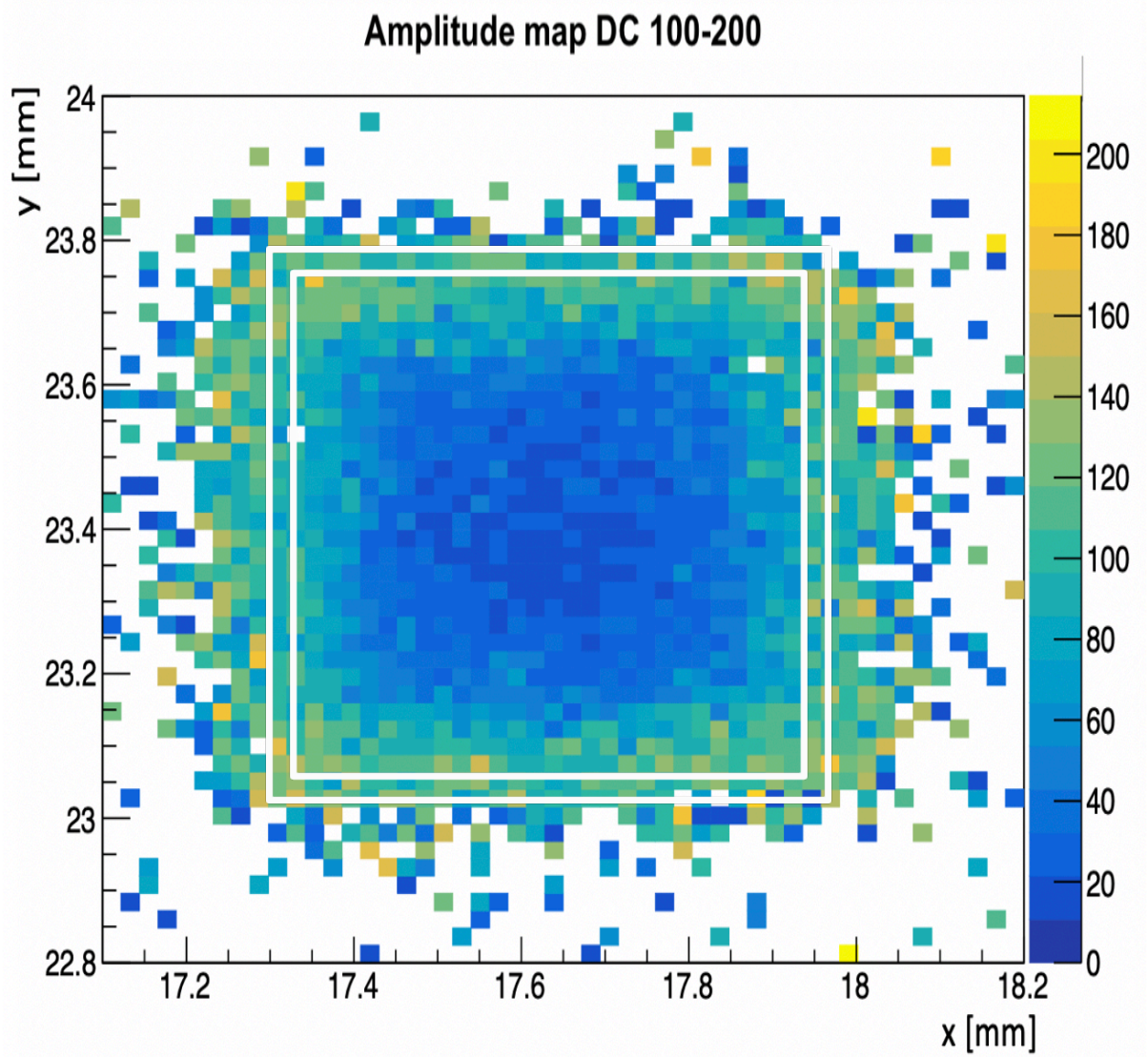


Particle impact point in the inner sensor region

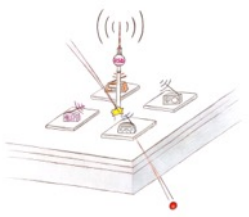


DC contact



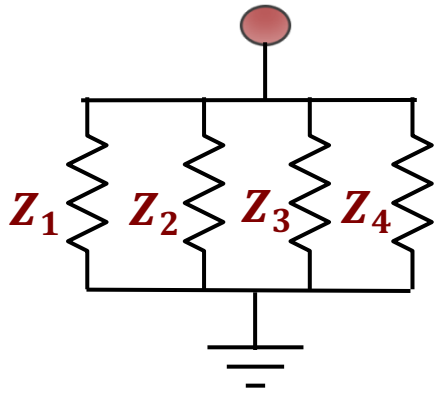


Charge sharing in RSD

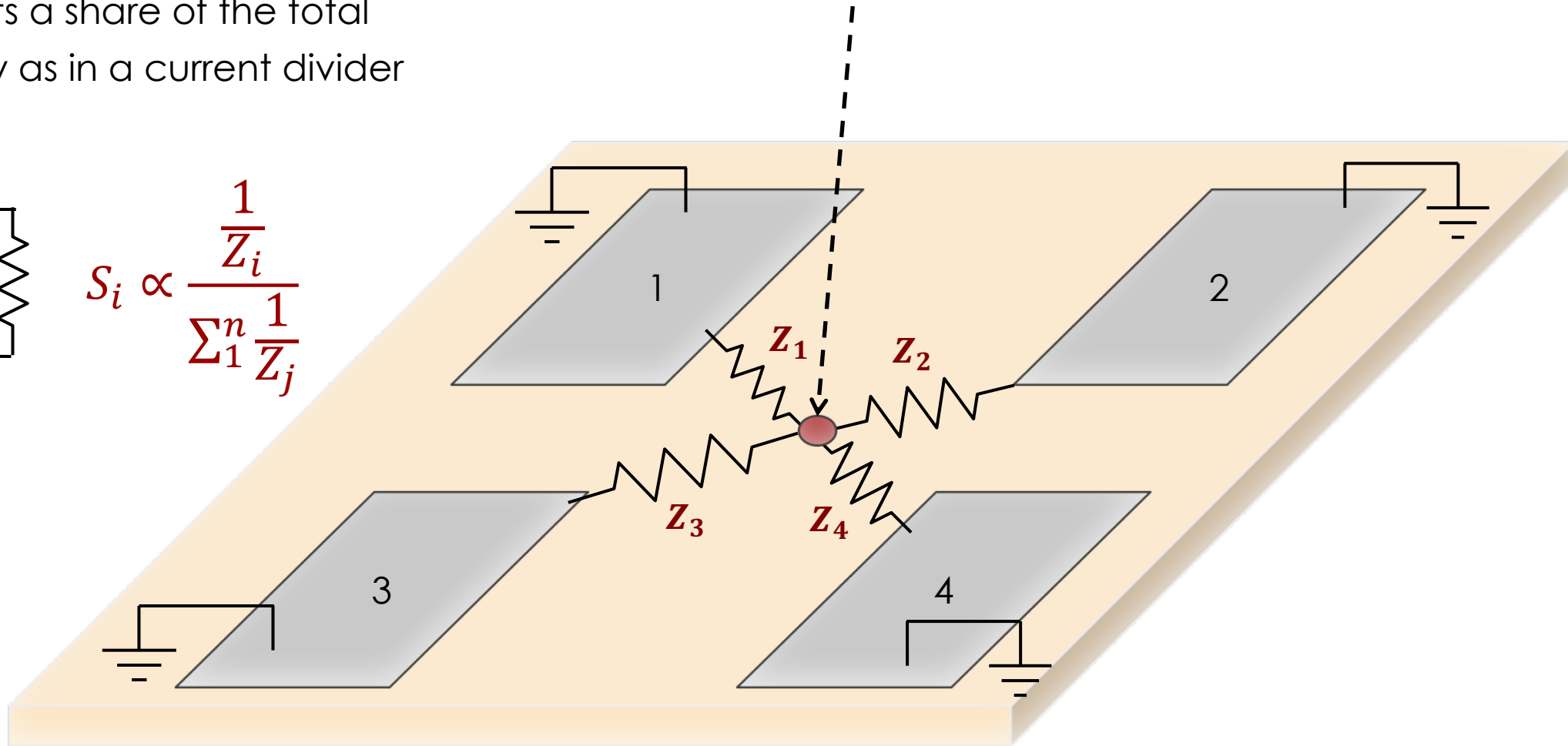


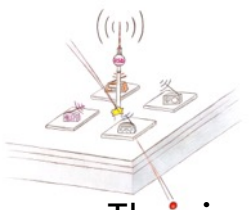
The signal sees several impedances in parallel, and it is split according to Ohm's law.

Each pad gets a share of the total signal, exactly as in a current divider



$$S_i \propto \frac{1}{Z_i} \frac{1}{\sum_{j=1}^n \frac{1}{Z_j}}$$





How to calculate Z_i



The impedance Z seen by a propagating signal does not increase linearly with the distance r since the signal spreads on a larger area

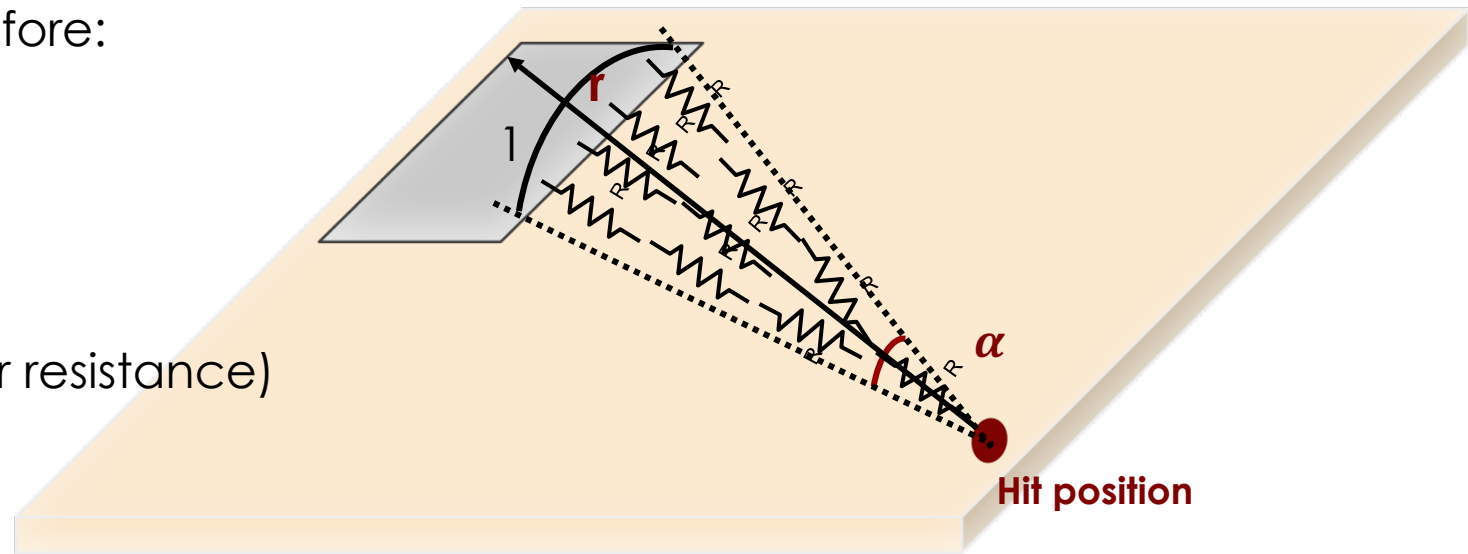
The resistance R per unit distance decreases as the circumference C becomes larger

$$Z(r) \propto \frac{dr}{\alpha r}$$

The impedance Z up to radius r is therefore:

$$Z(d) \propto \frac{1}{\alpha} \int_1^d \frac{1}{r} \propto \frac{\ln(d)}{\alpha}$$

where α is the angle (larger pad, smaller resistance)



RSD main formula



The fraction of signal seen in each pad is:

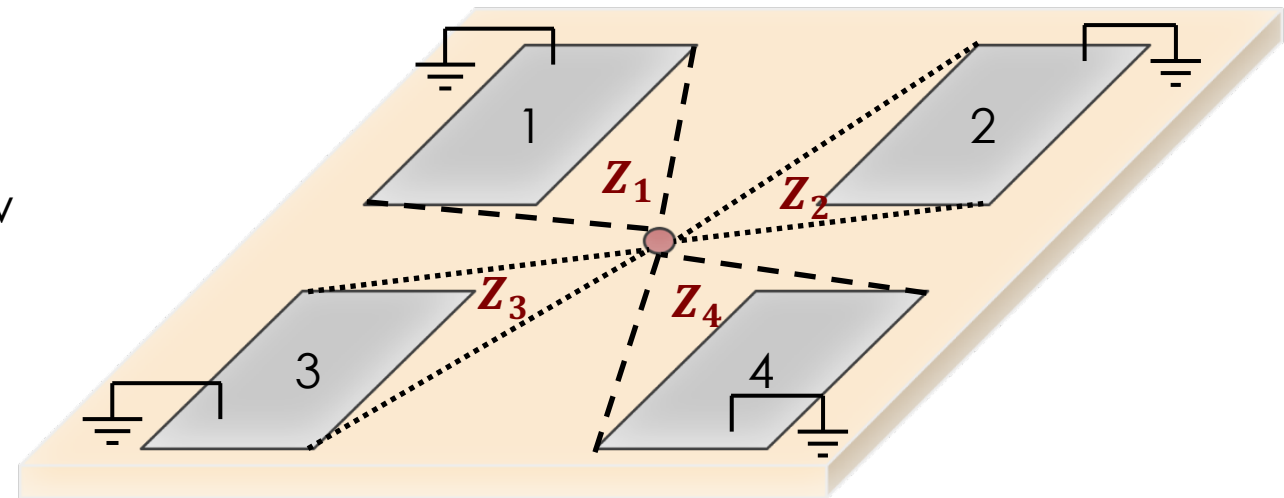
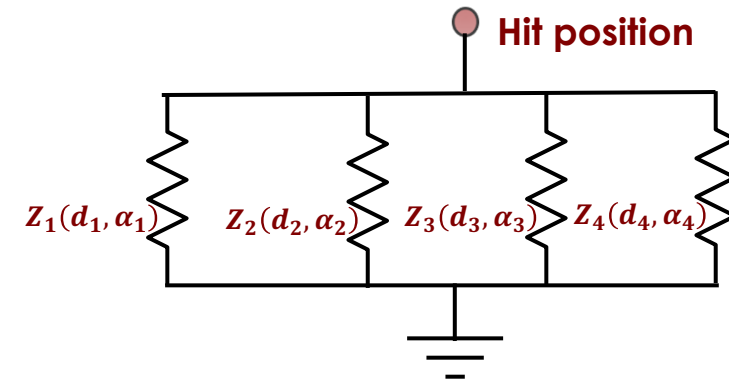
$$S_i(\alpha_i, d_i) = \frac{\frac{\alpha_i}{\ln(d_i)}}{\sum_1^n \frac{\alpha_j}{\ln(d_j)}}$$

where:

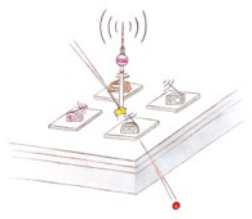
- d_i = distance hit-pad
- α_i = angle of view hit-pad

Important points:

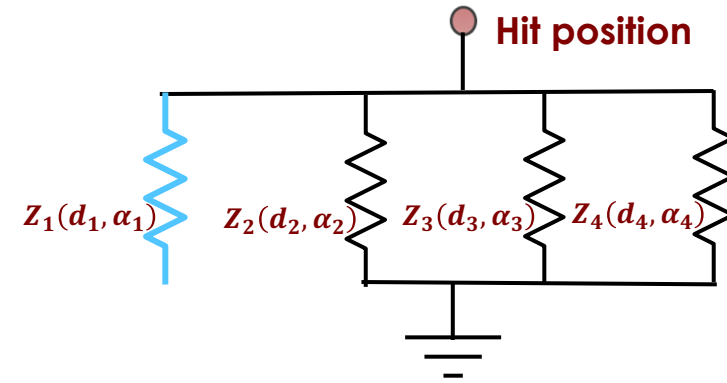
- The signal seen in a pad depends upon how many other pads are nearby
- A signal can be seen by 2,3 or 4 pads, depending on the hit location



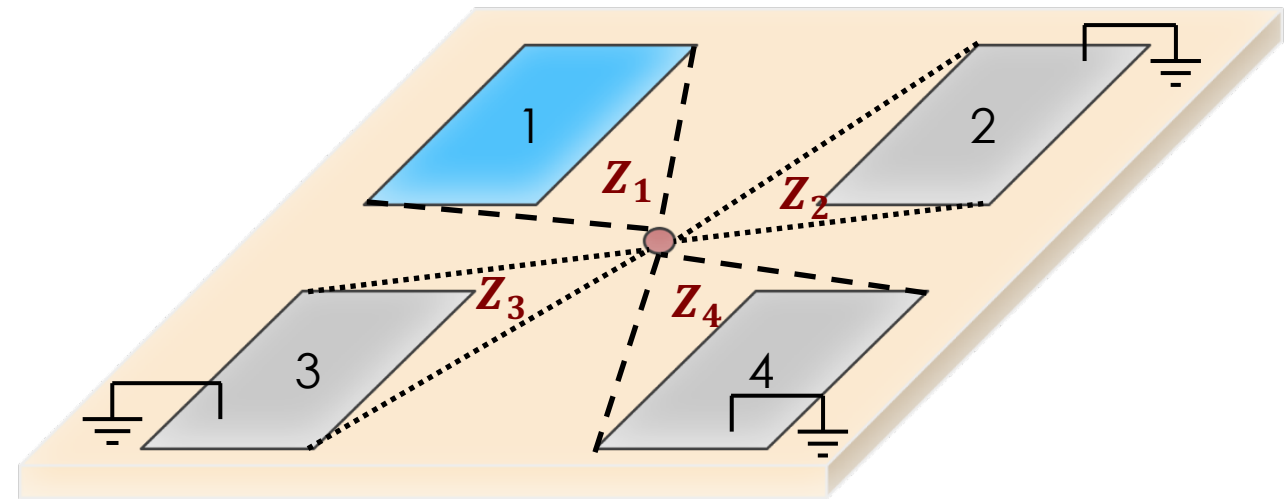
RSD main formula – floating pads



$$S_1(\alpha_1, d_1) = \frac{\alpha_1}{\ln(d_1)} = 0$$
$$\sum_1^n \frac{\alpha_j}{\ln(d_j)}$$

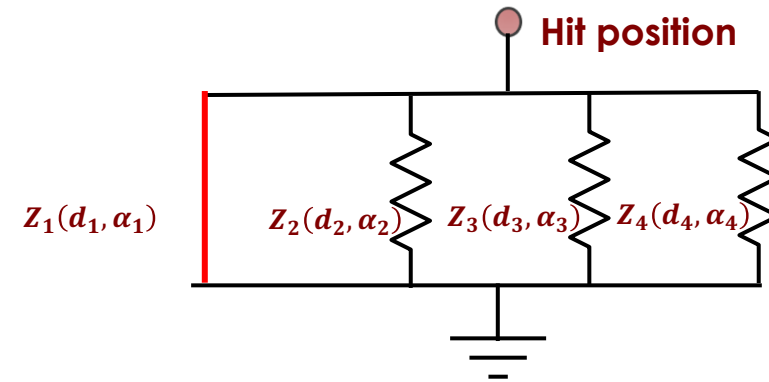


A floating pad does not contribute to the signal sharing, there is no path to ground, i.e., no current flow.



RSD main formula – Hit on metal

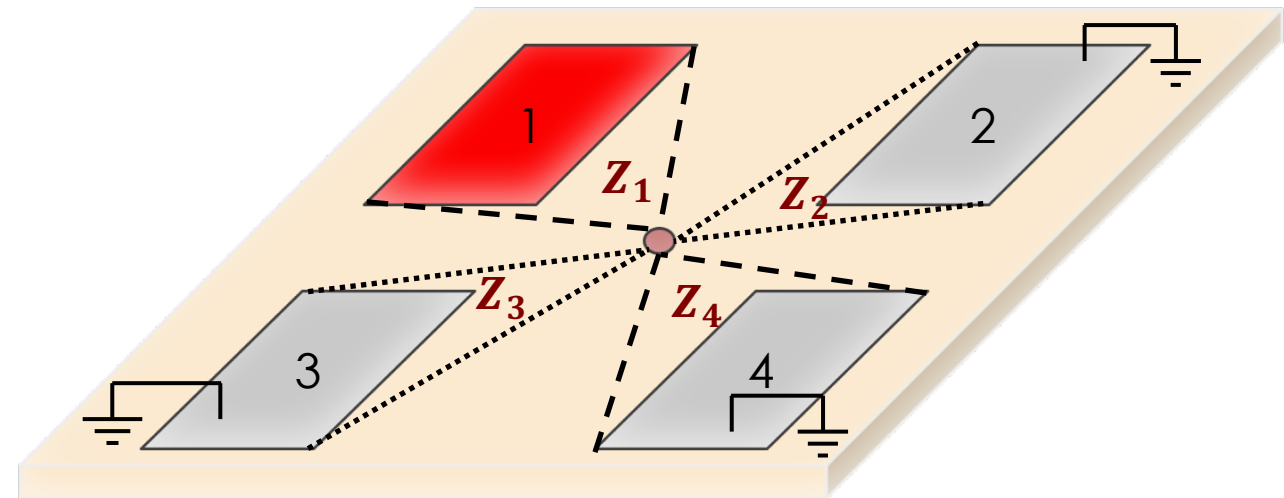
$$S_1(\alpha_1, d_1) = \frac{\alpha_1}{\sum_1^n \frac{\alpha_j}{\ln(d_j)}} \sim S_{tot}$$



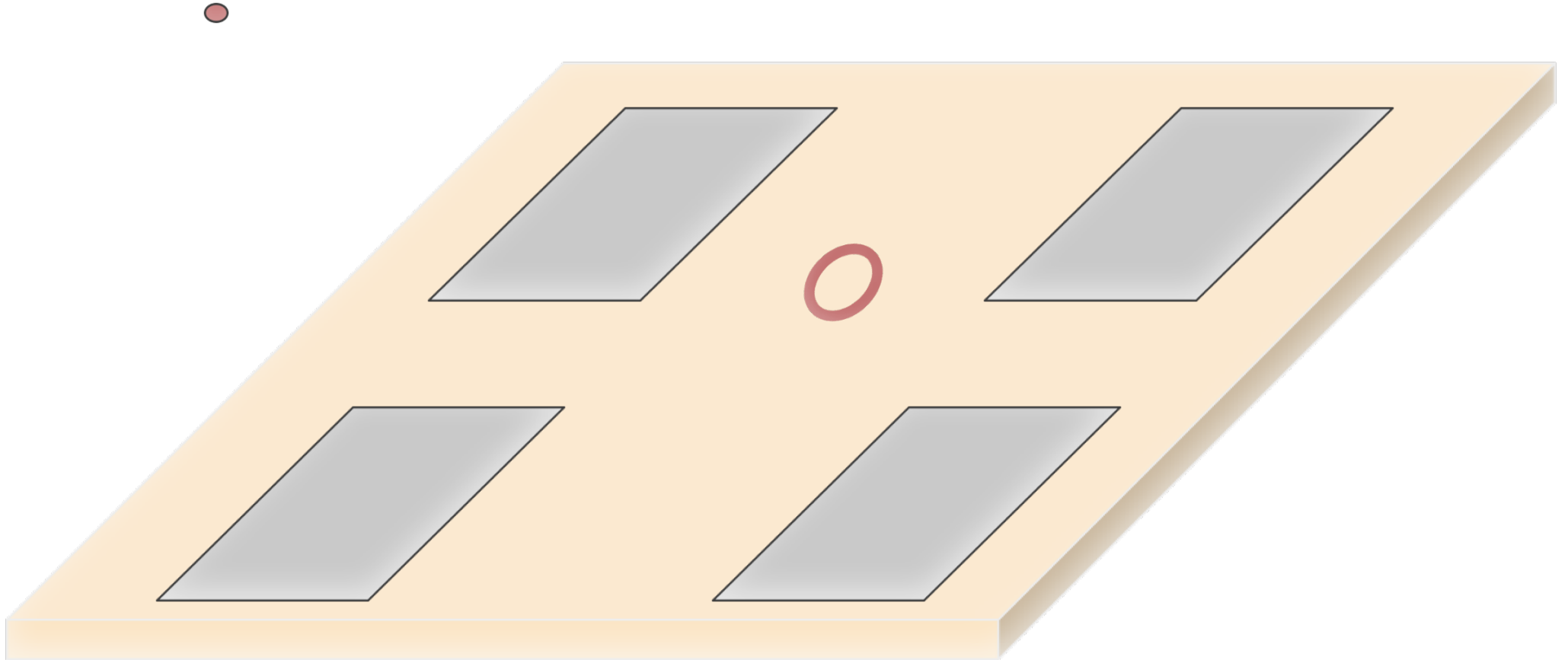
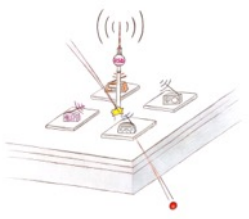
When the hit is on the metal, the impedance to that pad is \sim zero, so the whole signal is in one pad.

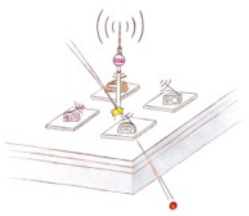
Consequences:

- In the following, signal sharing refers to the area without metal
- Metal pads need a special design



RSD main formula in motion



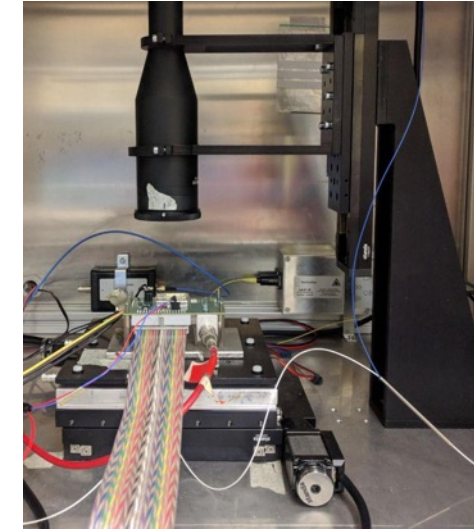


Experimental data: Laser and beam test



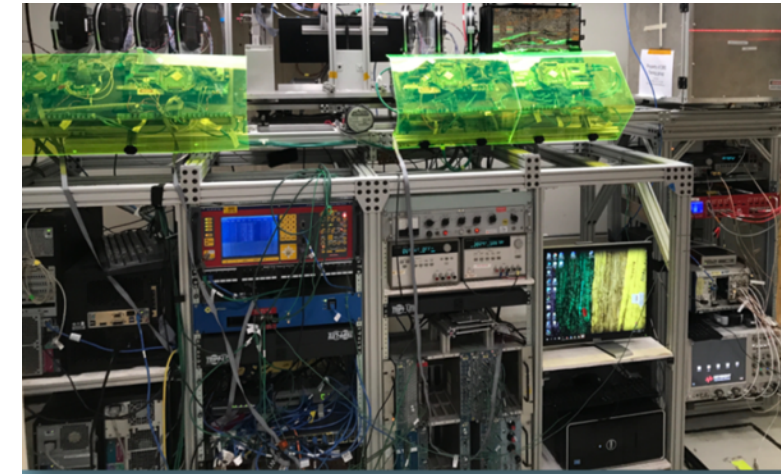
The laser studies presented here are obtained using a “Particular” laser TCT set-up

- Sensors are glued on a 16-channel read-out board.
- The laser is shot in various position via an x-y-z micrometric stage



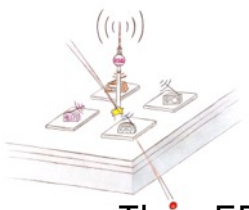
The beam test results have been obtained at FNAL, in collaboration with the FNAL CMS-Timing ETL team

- 120 GeV/c proton beam
- Precise timing determination (~ 10 ps)
- Fairly precise tracking system (~ 35 -40 μm)

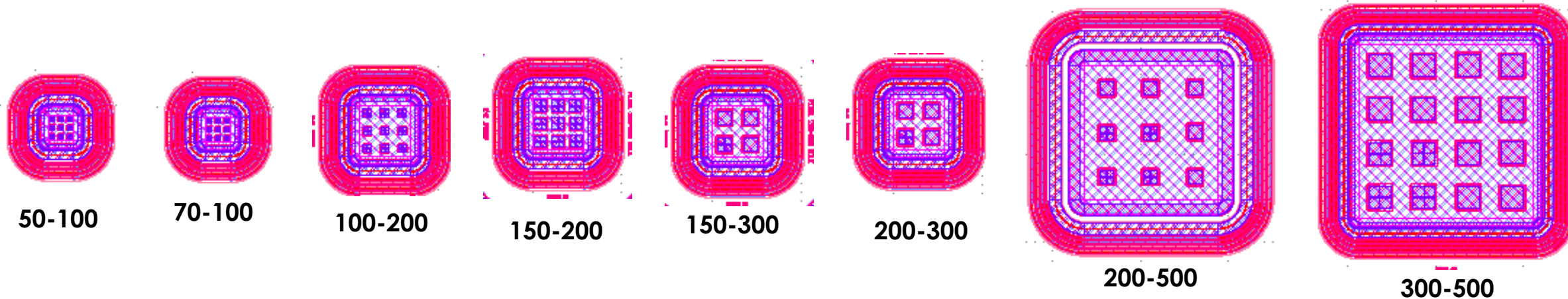


The signals are recorded with a digital oscilloscope (20-40 GS/s, 2-4 GHz BW) for offline analysis

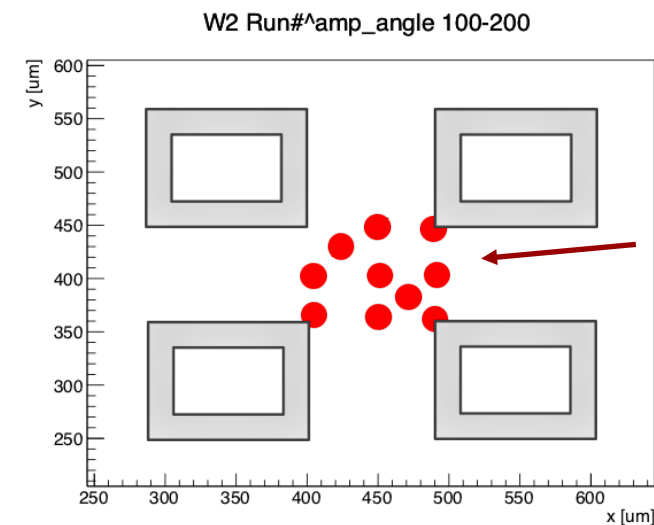
Structures tested (metal-pitch)

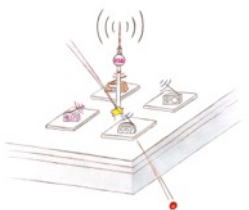


The FBK production RSD1 yielded many samples, of several geometries, exploring the interplay of n+ resistivity, dielectric thickness, metal pad, and pitch



Each sensor was tested with the laser TCT set-up, shining the laser spot ($\sim 10 \mu\text{m}$) in several positions and recording the signals seen by the 4 adjacent pads. The runs were repeated at 3-4 values of gain for each geometry

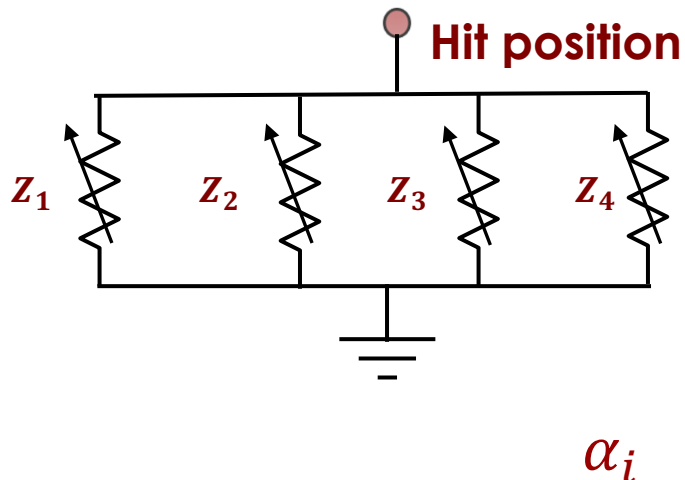




Signal amplitudes as a function of positions – 4 pads

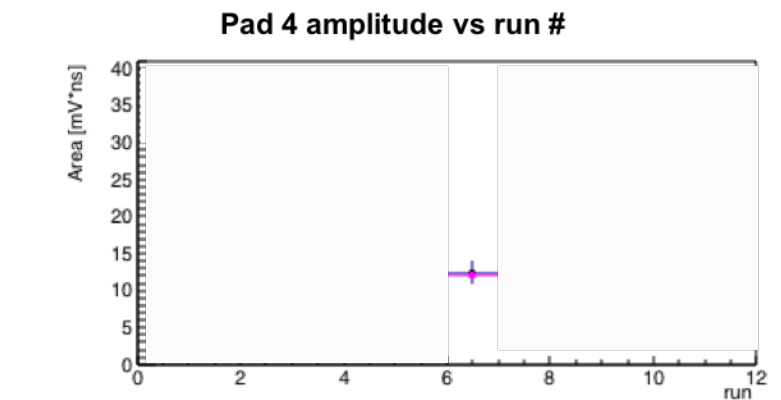
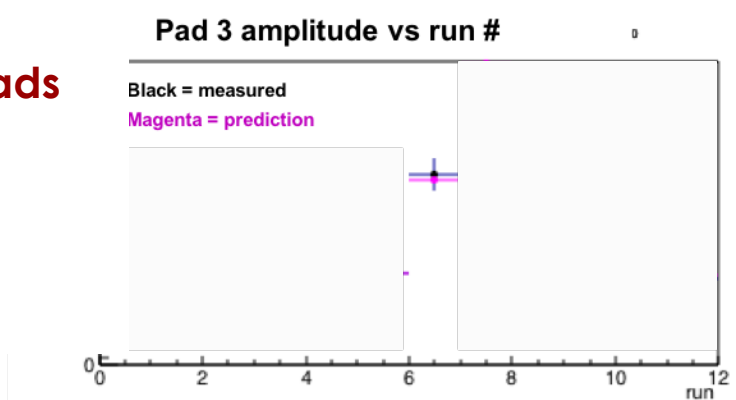
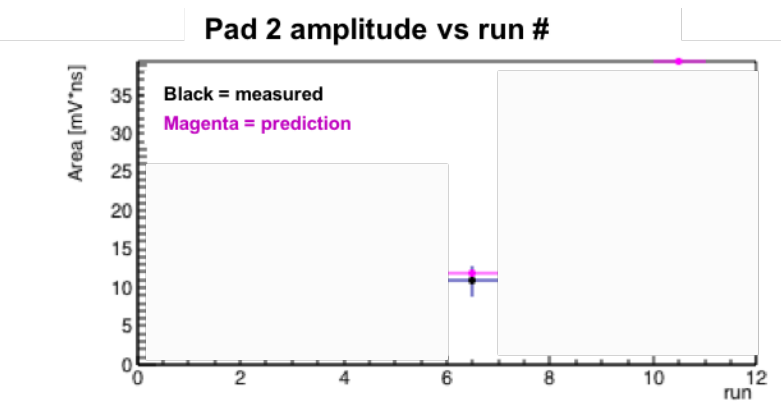
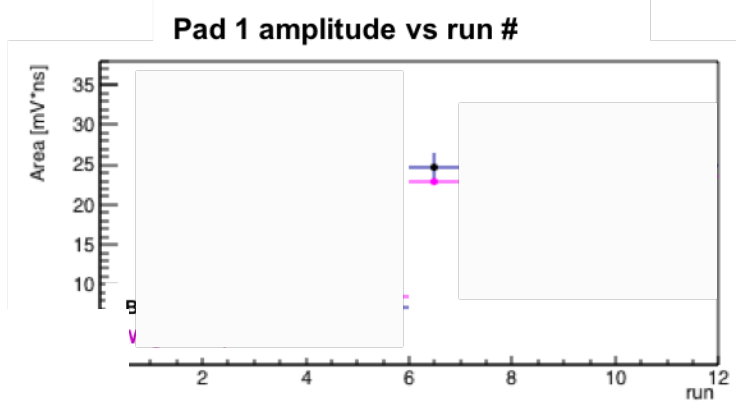
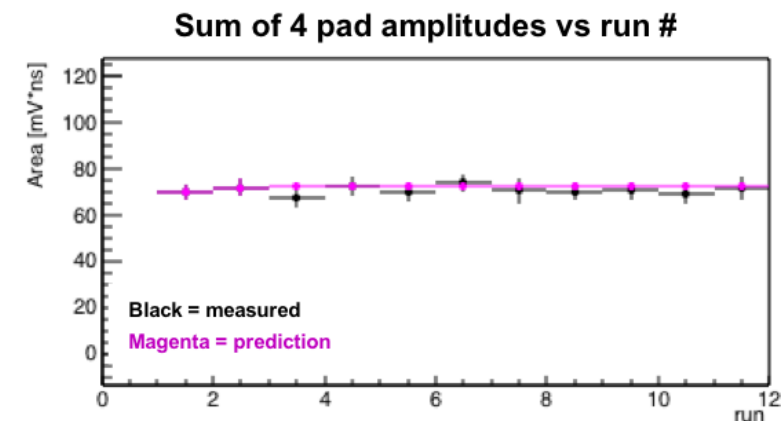
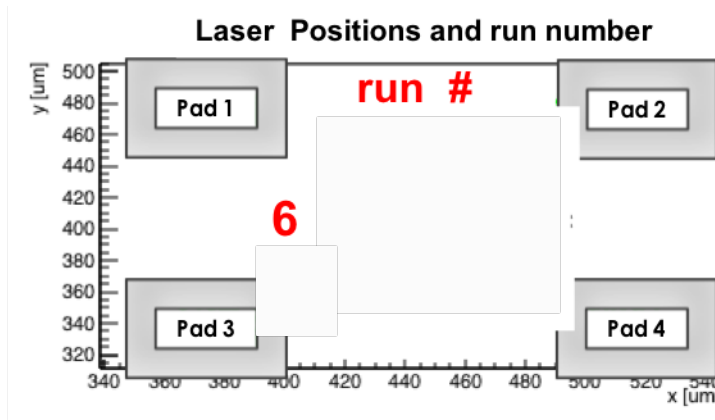


The amplitudes in the 4 pads change together, in a “coordinated way”, as they should in a current divider.

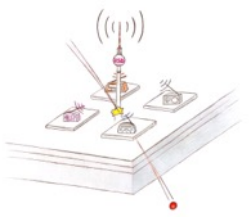


Wrap-up:

- RSD works as a current divider
- The signal is naturally shared among pads
- The RSD main formula works well
 - no free parameters, the magenta points are an absolute prediction
- The total amplitude is fairly constant



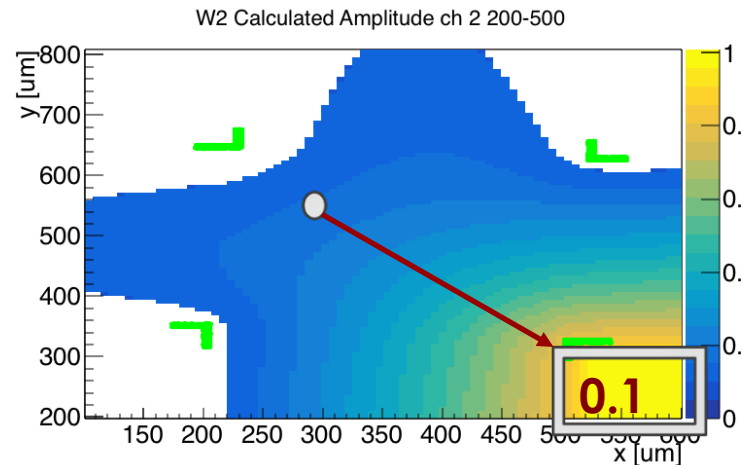
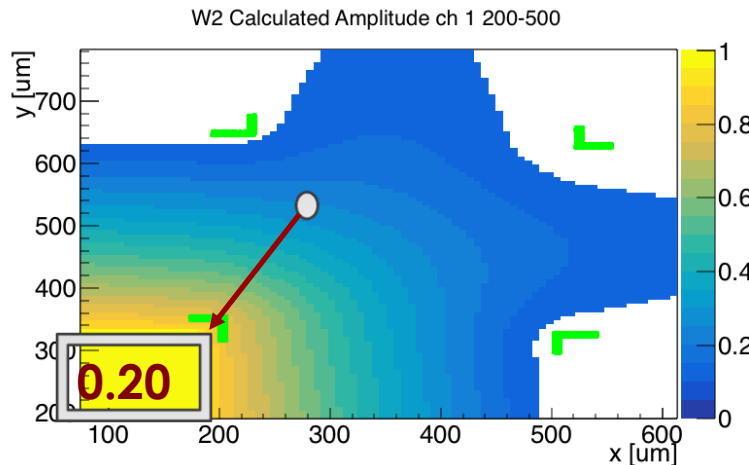
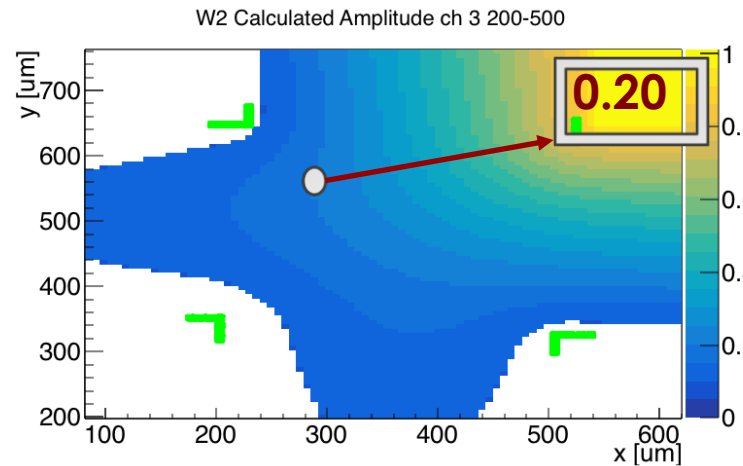
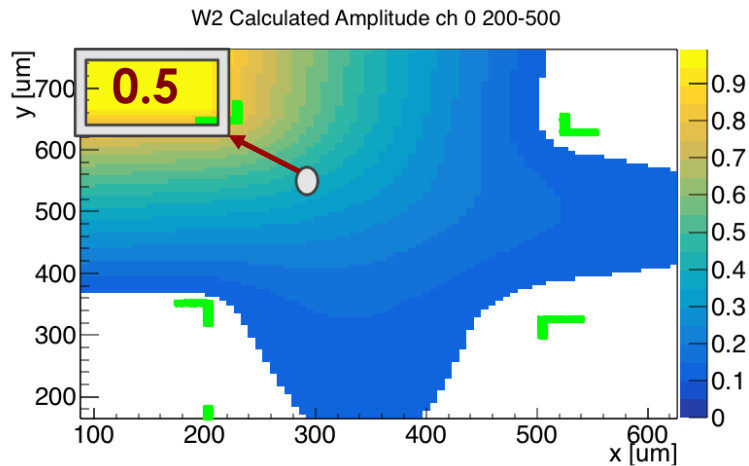
Position reconstruction method



Basic principle: the amplitudes seen by the pads define a unique x-y point

The RSD main formula allows computing for each x-y point the 4 amplitudes seen by the pads

A particle hits in a given position, with relative amplitude in the 4 pads **0.5,0.2,0.1,0.2**

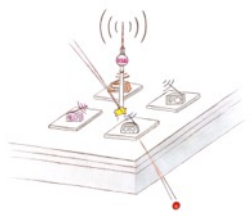


How the hit position is determined?

The x-y positions of a measured hit are the **coordinates of the bin that minimize the difference between the measured and calculated amplitudes of the 4 pads.**

Minimize the quantity:

$$\chi^2 = \sum_1^4 \frac{[S_i^{Meas} - S_i^{Calc}]^2}{\sigma}$$



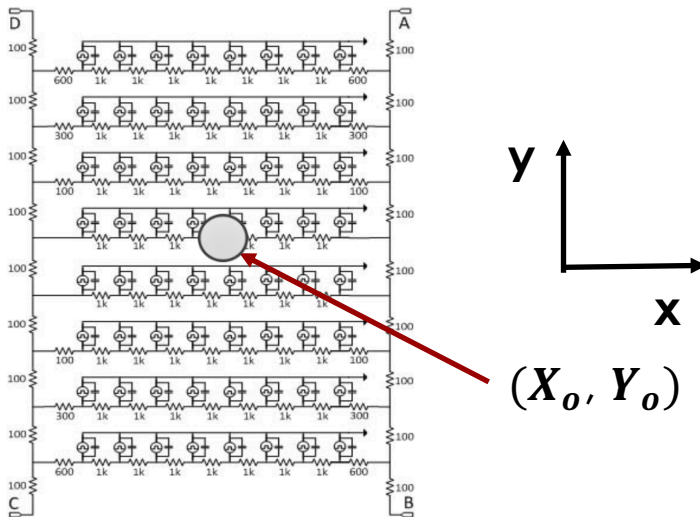
Discretized Positioning Circuit



The readout of an arrays of SiPMs in PET detectors is often performed by connecting them in a matrix of resistors and/or capacitors and measuring the signals at the 4 corners. This technique, called Discretized Positioning Circuit (DCP), is used to reduce the number of readout channel

DPC uses the charge imbalance between the two opposite sides of a square to determine the hit position.

64 SiPM read out by 4 pads

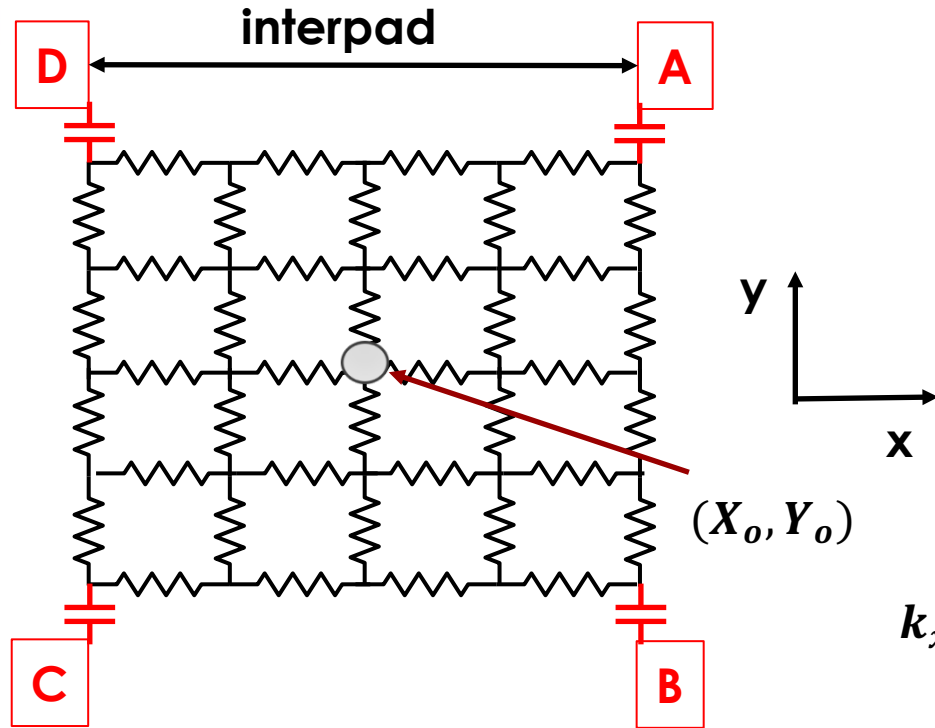


Charge imbalance in the x, y direction

$$X = X_o + \frac{X_A - X_B}{2} \frac{Q_A + Q_B - Q_C - Q_D}{Q_A + Q_B + Q_C + Q_D}$$

$$Y = Y_o + \frac{Y_A - Y_D}{2} \frac{Q_A + Q_D - Q_B - Q_C}{Q_A + Q_B + Q_C + Q_D}$$

RSD as a Discretized Positioning Circuit



$$X = X_o + k_x \left(\frac{Q_A + Q_B - Q_C - Q_D}{Q_A + Q_B + Q_C + Q_D} \right)$$

$$Y = Y_o + k_y \left(\frac{Q_A + Q_D - Q_B - Q_C}{Q_A + Q_B + Q_C + Q_D} \right)$$

$$k_x = \frac{\text{interpad}}{2} * \frac{\alpha_x}{\left(\frac{Q_A + Q_D - Q_B - Q_C}{Q_A + Q_B + Q_C + Q_D} \right)_{x=X_o + \frac{\text{Interpad}}{2}, y=Y_o}}$$

RSD is a hybrid resistors/capacitors DPC circuit

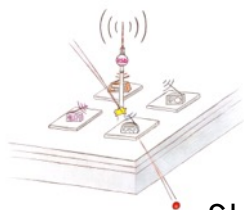
The reconstruction method uses only the signals in the 4 pads to reconstruct the hit position

➔ no need for an analytical sharing law.

➔ $k_{x,y}$ = imbalance parameter along x or y

- Maximum value of the charge imbalance within the pixel
- Needs to be determined experimentally for each geometry

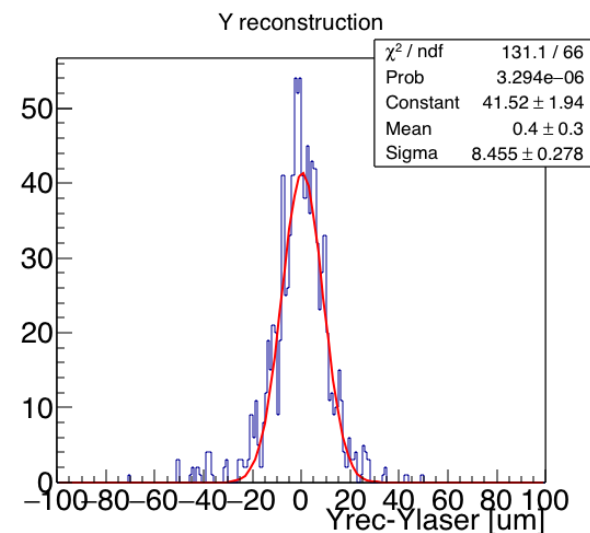
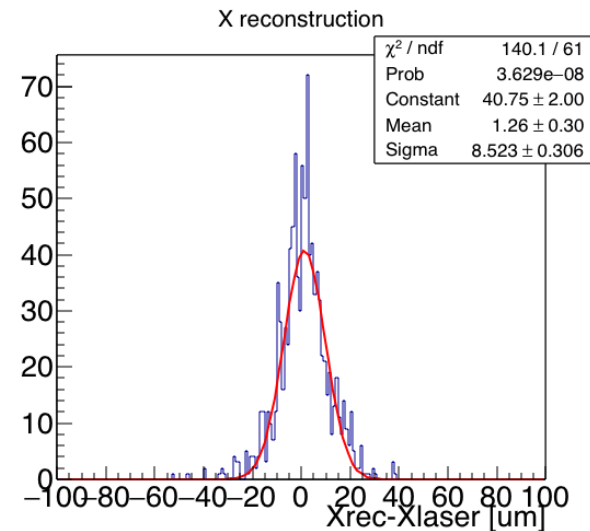
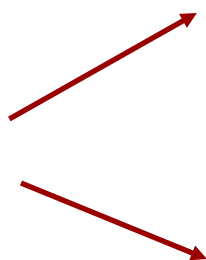
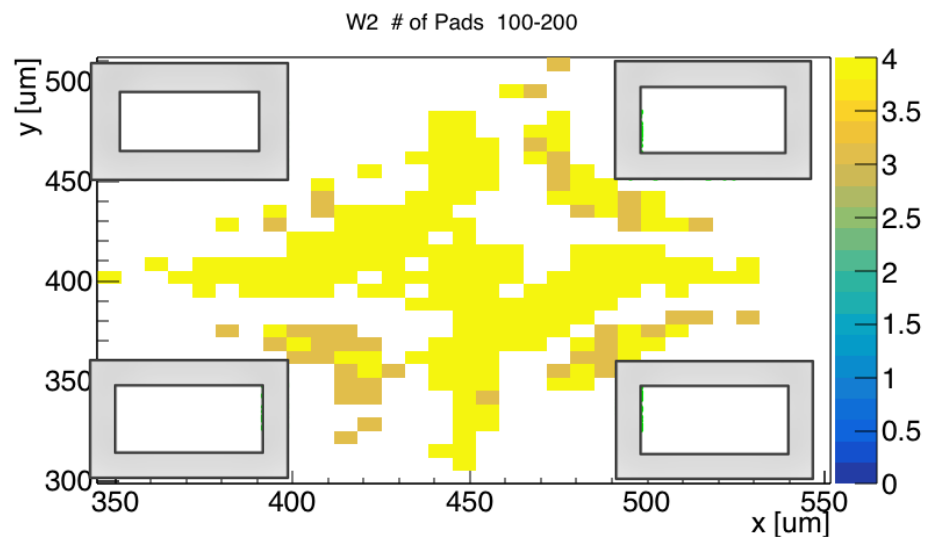
Laser study: position resolution



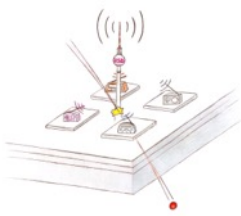
Shooting the laser in many positions, the **spatial precision** can be evaluated. This is done by comparing the position reconstructed using the look-up table to the known laser position.

Geometry: 100 Metal, 200 pitch

Shooting position and # of pads used in the reconstruction



Resolution ~ 8.5 um
Gain ~ 17



Spatial resolution in resistive readout



$$\sigma_x^2 = \sigma_{Jitter}^2 + \sigma_{Sensor}^2 + \sigma_{Reconstruction}^2$$

$$\sigma_{Jitter} = \frac{\sigma_{El_noise}}{\frac{dV}{dx}}$$

Electronic noise

Assume a geometry with only 2 pads:

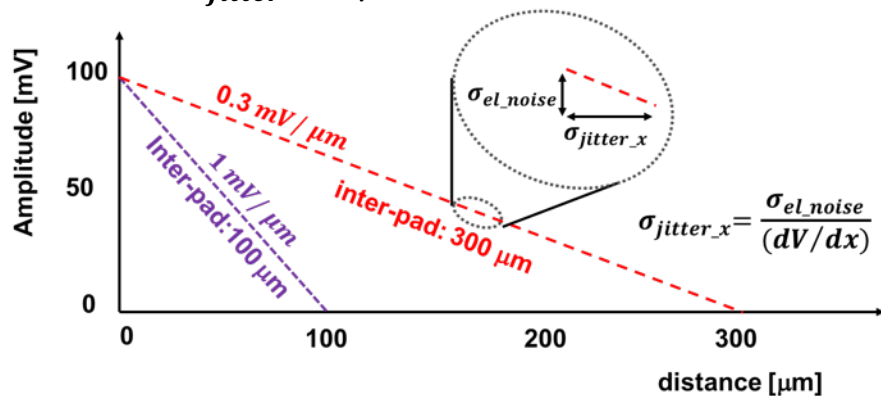
- 100 μm and 300 μm apart
- 100mV signal
- 3 mV electronic noise

100 μm : the signal changes by 1 mV/ μm

$$\rightarrow \sigma_{Jitter} = 3 \mu\text{m}$$

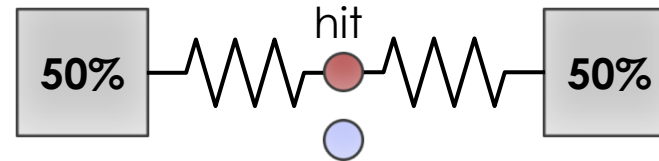
300 μm : the signal changes by 0.3 mV/ μm

$$\rightarrow \sigma_{Jitter} = 9 \mu\text{m}$$

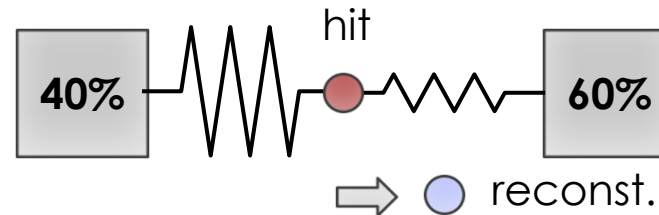


σ_{Sensor}

Sensor non-uniformity



For equal resistivity, 50%-50% sharing indicates the hit is in the middle



If the resistivity is not uniform, the reconstruction shifts the point closer to the smaller resistivity

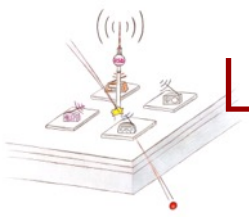
$\sigma_{Reconstruction}$

Algorithm

$$S_i(\alpha_i, r_i) = \frac{\frac{\alpha_i}{\ln(r_i)}}{\sum_1^n \frac{\alpha_j}{\ln(r_j)}}$$

If the predicted sharing is incorrect, the reconstructed position is shifted.

DPC: RSD might not be a perfect DPC, yielding to systematic errors.



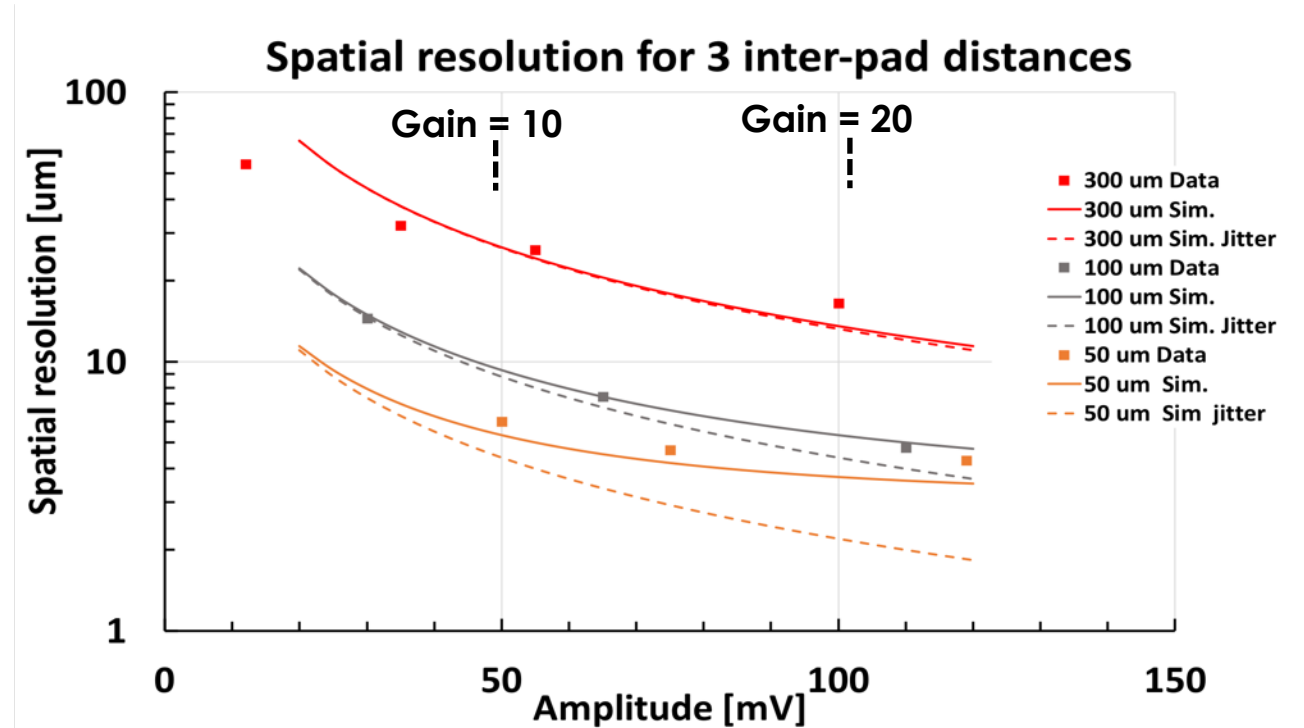
Laser study: position resolution as a function of amplitude



The spatial resolution improves with signal amplitude, plateauing at about 5 um

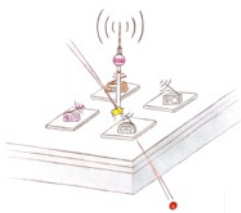
Important points:

- At low signal amplitude, the resolution is dominated by jitter
 - Low noise electronics
- Larger geometries have worse position resolution
 - need high gain
- At high amplitude, the resolution is limited by systematics such as the precision of the amplitude reconstruction and the use of the RSD main formula.

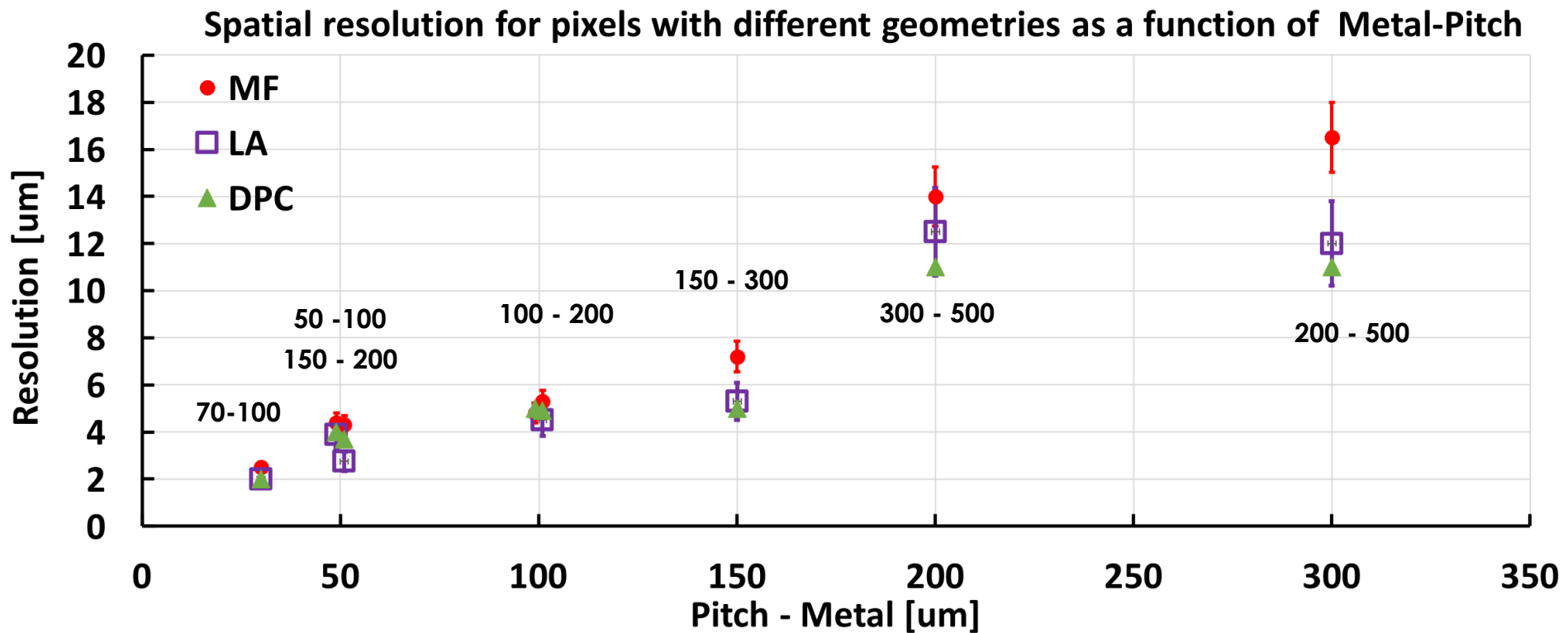


Interpad	Measured Resolution
300 um	17 ± 0.1 (exp.) ± 3.5 (syst.) um
100 um	5.5 ± 0.1 (exp.) ± 3.5 (syst.) um
50 um	4 ± 0.1 (exp.) ± 3.5 (syst.) um

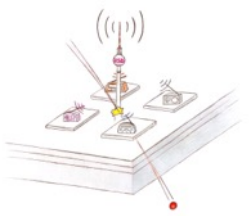
$$\sigma_x^2 = \sigma_{Jitter}^2 + \sigma_{Sensor}^2 + \sigma_{Reconstruction}^2$$



Laser study: position resolution as a function of pixel geometry



RSDs reach a spatial resolution that is about 5% of the inter-pad distance

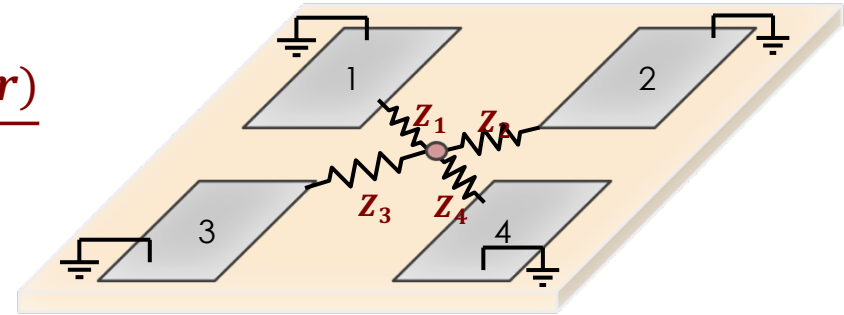


Laser study: signal delay

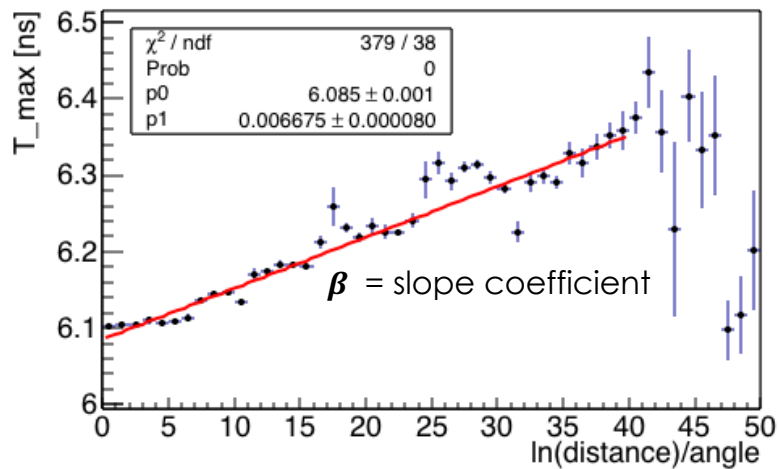


Each pad sees the signal with a delay proportional to the resistance from the impact point to the pad

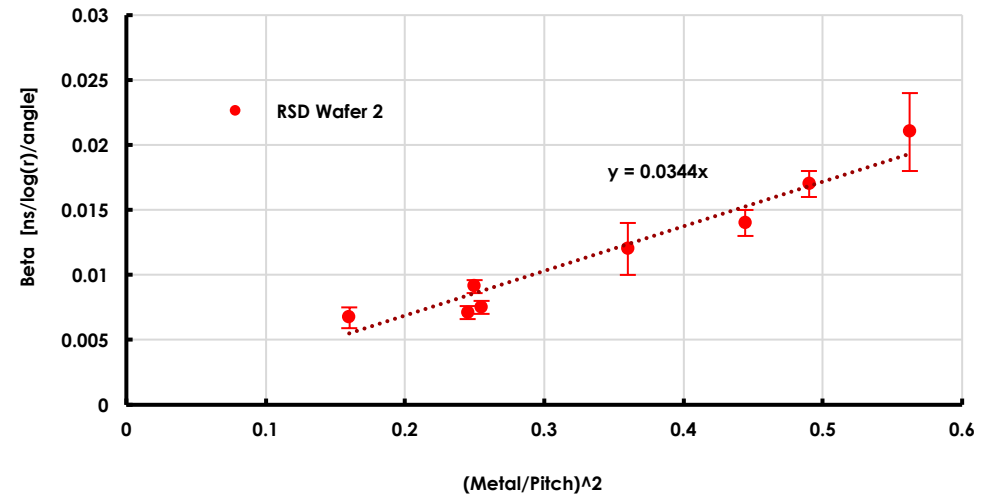
$$\text{delay} \propto \frac{\ln(r)}{\alpha}$$



T_{\max} vs $\frac{\ln(r)}{\alpha}$ for the geometry 200-500



Coefficient β for different geometries



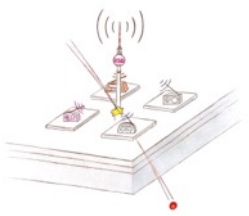
The time of each pad is defined as:

$$t_i^{\text{True}} = t_i^{\text{Meas}} - \beta \frac{\ln(r_i)}{\alpha_i}$$

β depends linearly from $(\text{metal/pitch})^2$ (related to the detector capacitance)

FNAL beam test results

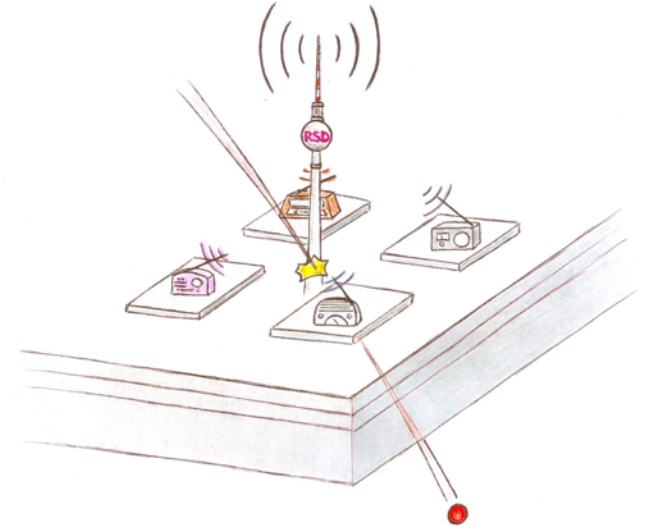
All details in: M. Tornago, 36th RD50 "Latest results on RSD spatial and timing resolution <https://indi.to/2cGQy>



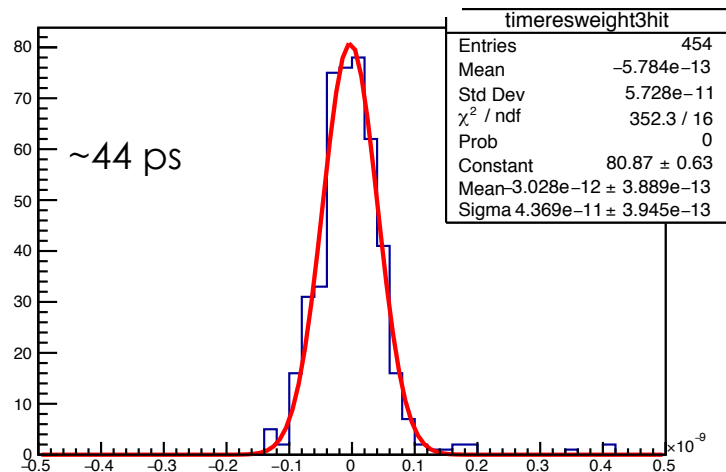
Data taken with RSD 3x3 100-200 and 190-200 geometries

Lesson learnt:

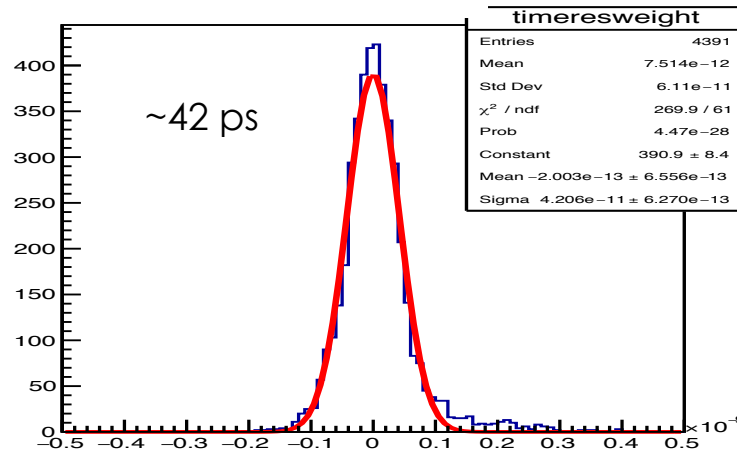
- RSD are ~ 100% efficient
- The RSD x-y hit reconstruction worked very well
- The time resolution is $\sigma_{t\ 100-200} = 44\ ps$, $\sigma_{t\ 190-200} = 42\ ps$
- The metal size (100 vs 190 μm) does not influence the time resolution



100 - 200

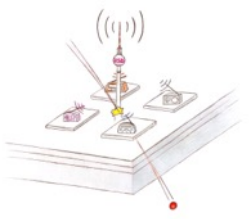


190 - 200



Interesting fact: the combination of n pads does not lead to a $1/\sqrt{n}$ improvement since the effects of non-uniform ionization are fully correlated

→ pads see a copy of the same signal



RSD main formulas



RSD signals are therefore controlled by two equations:

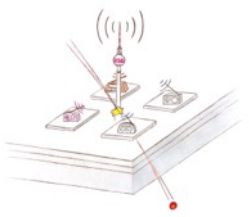
1. the signal sharing among pads

$$S_i(\alpha_i, r_i) = \frac{\alpha_i}{\ln(r_i)} \frac{1}{\sum_1^n \frac{\alpha_i}{\ln(r_i)}}$$

2. the signal delay

$$t_i^{True} = t_i^{Meas} - \gamma \left(\frac{Metal}{pitch} \right)^2 \frac{\ln(r_i)}{\alpha_i}$$

where γ is wafer-specific (n+ resistivity, dielectric thickness)



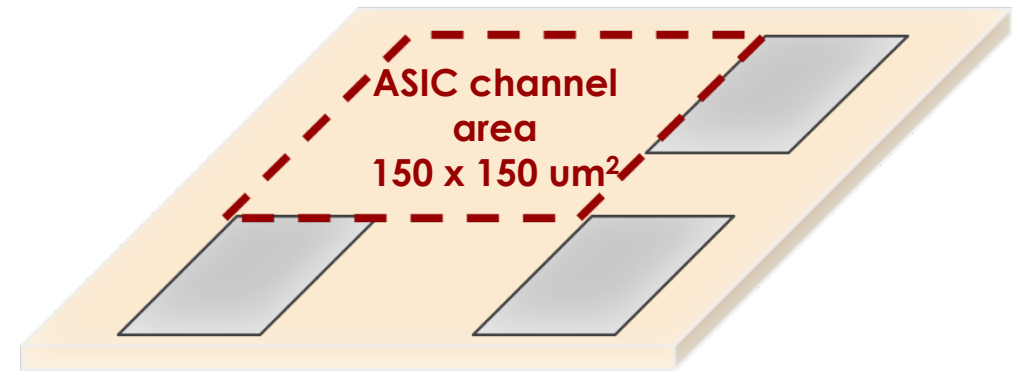
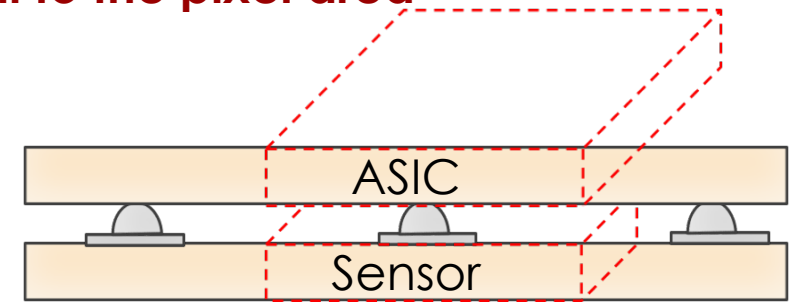
ASIC for RSD



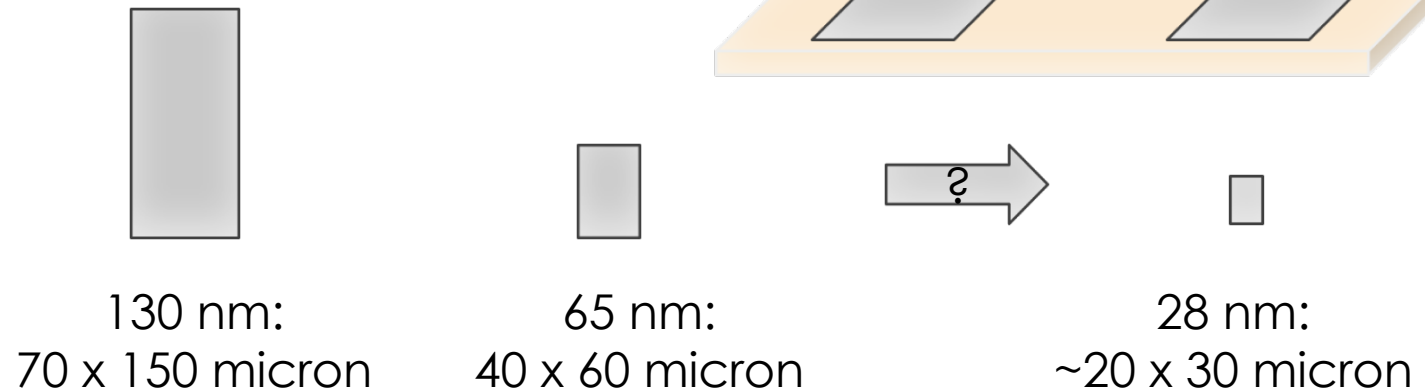
Very important point: in hybrid technology (sensor bump-bonded to the ASIC),
the area available for each read-out channel is identical to the pixel area

**Assuming a goal of ~ 5 mm spatial resolution,
 the RSD pitch can be 150-200 μm**

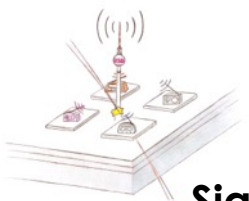
- At least a factor of 10-20 more space than using binary readout
- Can concentrate the power available for that area into a single channel
- The needed circuits for timing might actually fit



Example:
 TDC evolution



RSD Read-out scheme - II



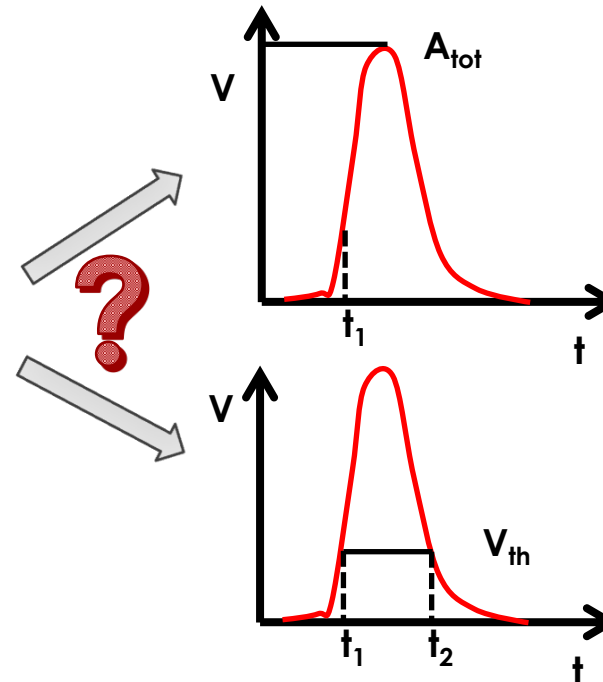
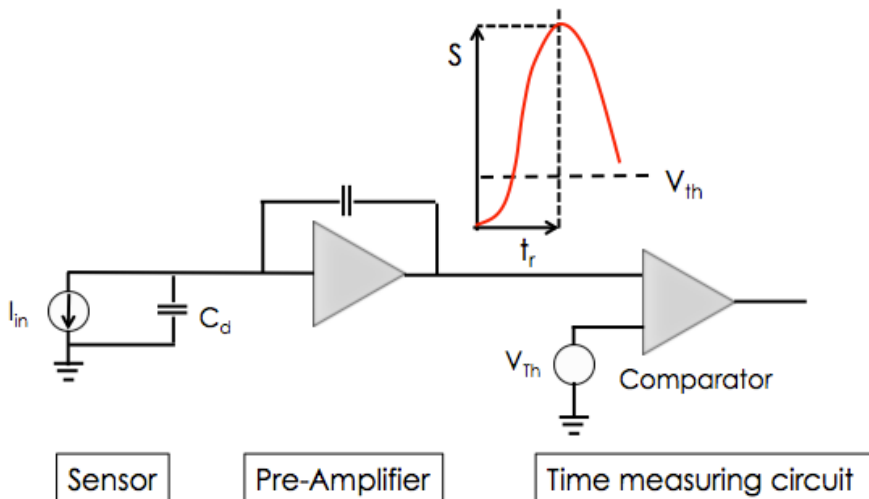
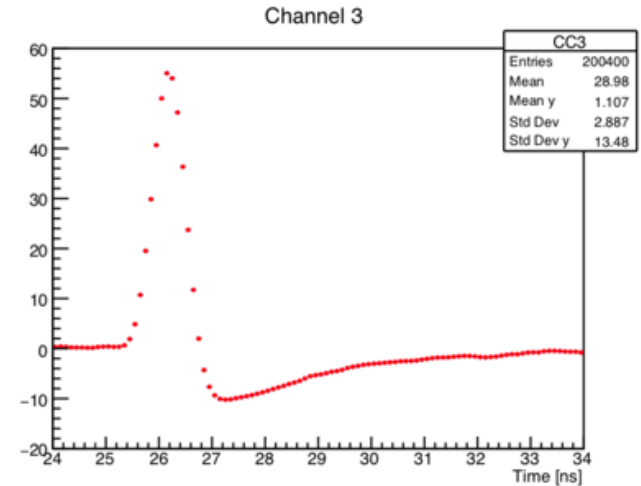
Signal characteristics:

- Short and fast, very similar to standard UFSD
- Bipolar (do not integrate)

Read-out characteristics:

- Record signal amplitude with good precision
- Timing capabilities: keep the jitter below the Landau floor
 $BW \sim 500 \text{ MHz}, Q_{in} \sim 5 - 10 fC$

➔ A Leading edge discriminator with linear Time-over-Threshold information or/and a DAC for amplitude measurement



Time of Arrival and Amplitude:

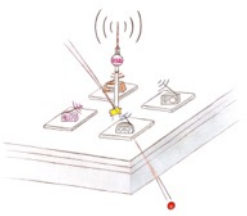
$$t_1, A_{tot}$$

TDC for t_1 ,
ADC for A_{tot}

Time over Threshold:

$$ToT = t_2 - t_1$$

Need TDC for t_1, t_2



RSD intrinsic time resolution



The AC readout scheme does not change the basic timing properties of UFSD:

$$\sigma_t^2 = \left(\frac{\text{Noise}}{dV/dt}\right)^2 + (\Delta\text{ionization})^2$$

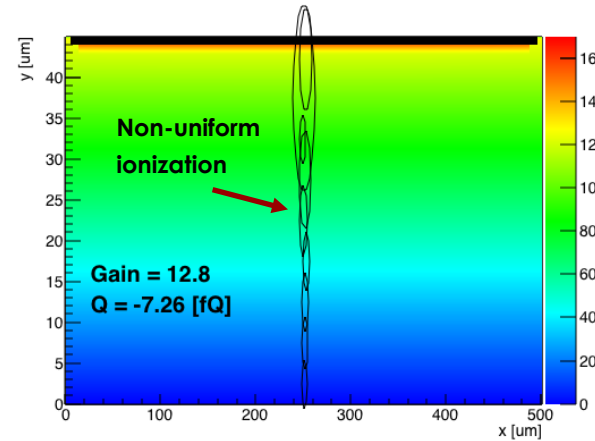
“Jitter” term

Here enters everything that is “Noise” and the steepness of the signal

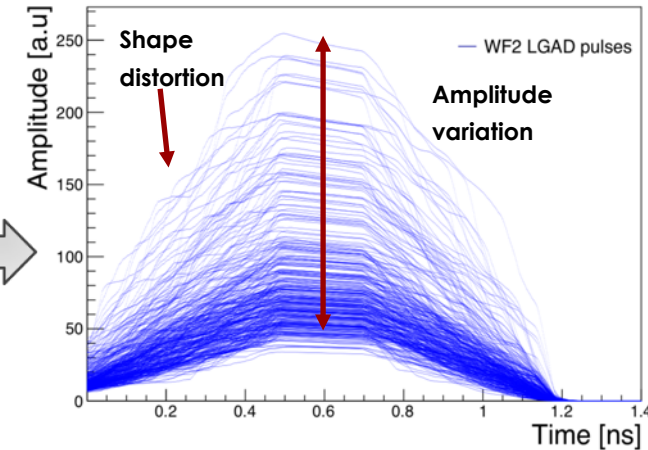
Non uniform ionization:

1) **Amplitude variation:**
variation in the total charge

2) **Shape distortion:**
Signal Shape distortion → Minimum time resolution



Simulation of signals in 50-um RSD



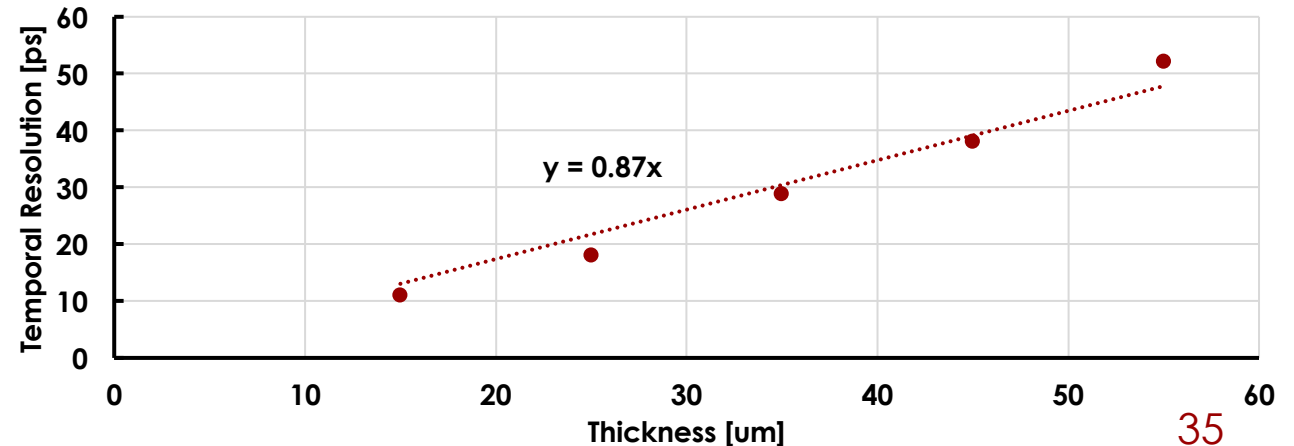
RSD minimum temporal resolution improves for thinner sensors:

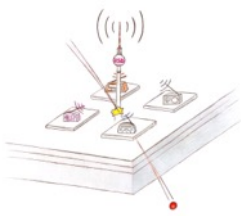
40 ps @ 45 um → 20 ps @ 25 um

However, the total charge is less (10fC → 5 fC) and the electronics might not be able to exploit this improvement

WF2 Simulation

Minimum temporal resolution vs sensor thickness using CDF = 50%





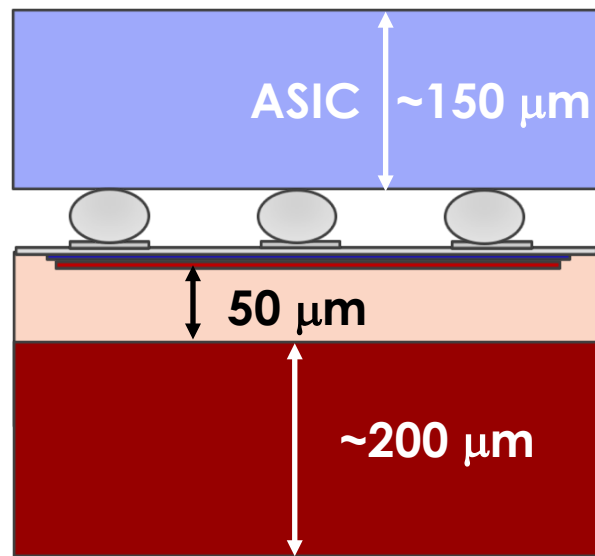
RSD material budget and time resolution



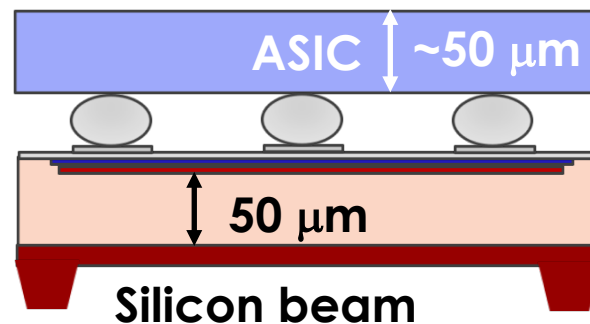
The active thickness of RSD sensor is rather small $\sim 50 \mu\text{m}$.

In the present prototypes, the active part is attached to a thick “handle wafer”

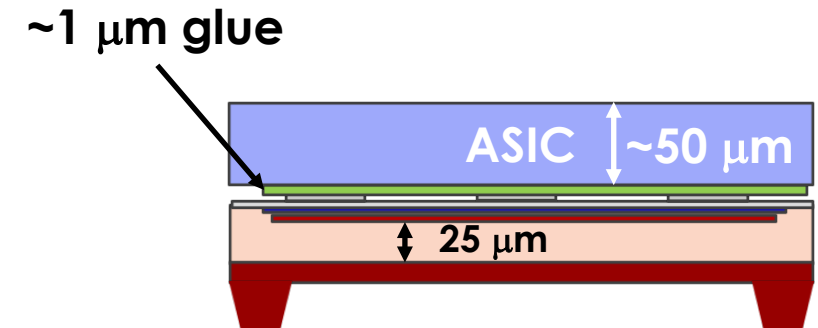
There is a clear path leading to $< 100 \mu\text{m}$ material:



Present design: no material budget optimization

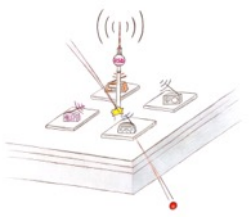


- Thinned handle wafer: $500 \mu\text{m} \rightarrow 10\text{-}20 \mu\text{m}$



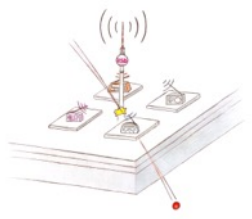
- Thinned handle wafer: $500 \mu\text{m} \rightarrow 10\text{-}20 \mu\text{m}$
- Thinned active area: $50 \mu\text{m} \rightarrow 25 \mu\text{m}$
 $50 \text{ ps} \rightarrow 25 \text{ ps}$

Summary of RSD characteristics



In AC-LGAD/RSD signal sharing happens on the surface, in the n+ layer, and not during the e/h drift, opening the possibility of having very small σ_{MS} and σ_x

1. The AC-LGAD/RSD design combines internal signal sharing with internal gain
2. RSDs have:
 - Very good position resolution due to internal sharing ($< 5 \mu\text{m}$)
 - Very good temporal resolution due to internal gain ($\sim 20\text{-}30 \text{ ps}$)
 - 100% fill factor due to the continuous n+ implant
3. RSDs can be made very thin ($\sim 30 \mu\text{m}$)
4. The pixel size can be kept large: $200 \times 200 \mu\text{m}^2$ achieves $5 \mu\text{m}$ position resolution



Future directions



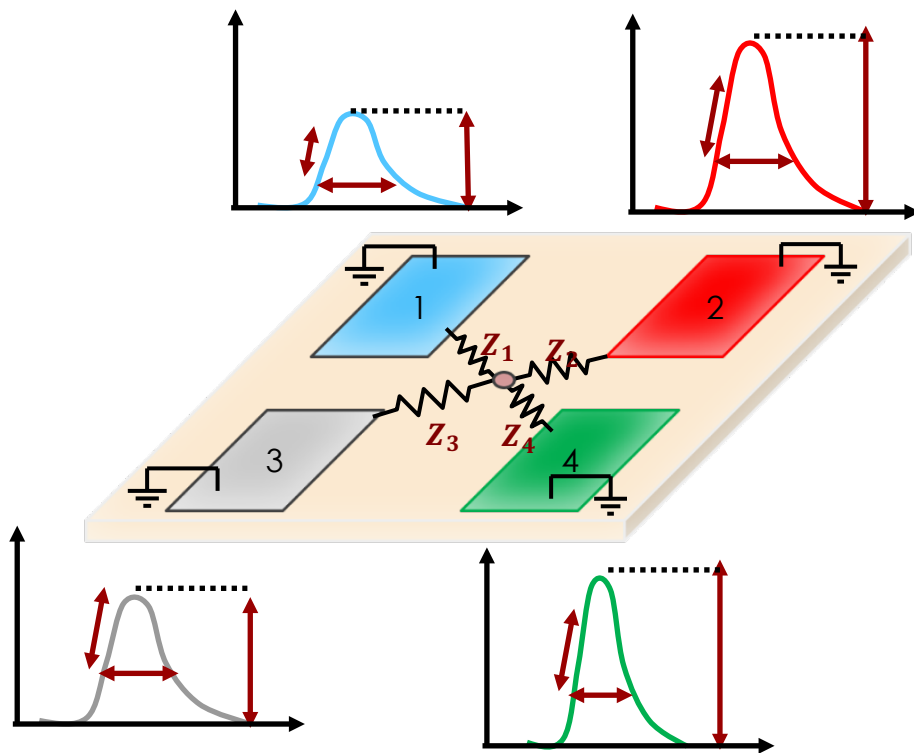
- **Reconstruction algorithm:** use of machine learning
- **Position resolution:** design optimization
- **RSD strip detector:** design optimization
- **Far out designs:** where the wild things are
- **RSD field of applications**

Machine Learning applied to RSD

All details in: F. Siviero, 36th RD50 “Position reconstruction using machine learning algorithms applied to Resistive Silicon Detectors (RSD)”



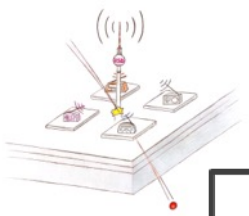
Each of the signals in an RSD event carries a lot of information (**amplitude, derivative, width**) that can be exploited to perform very accurate x-y-t reconstruction.



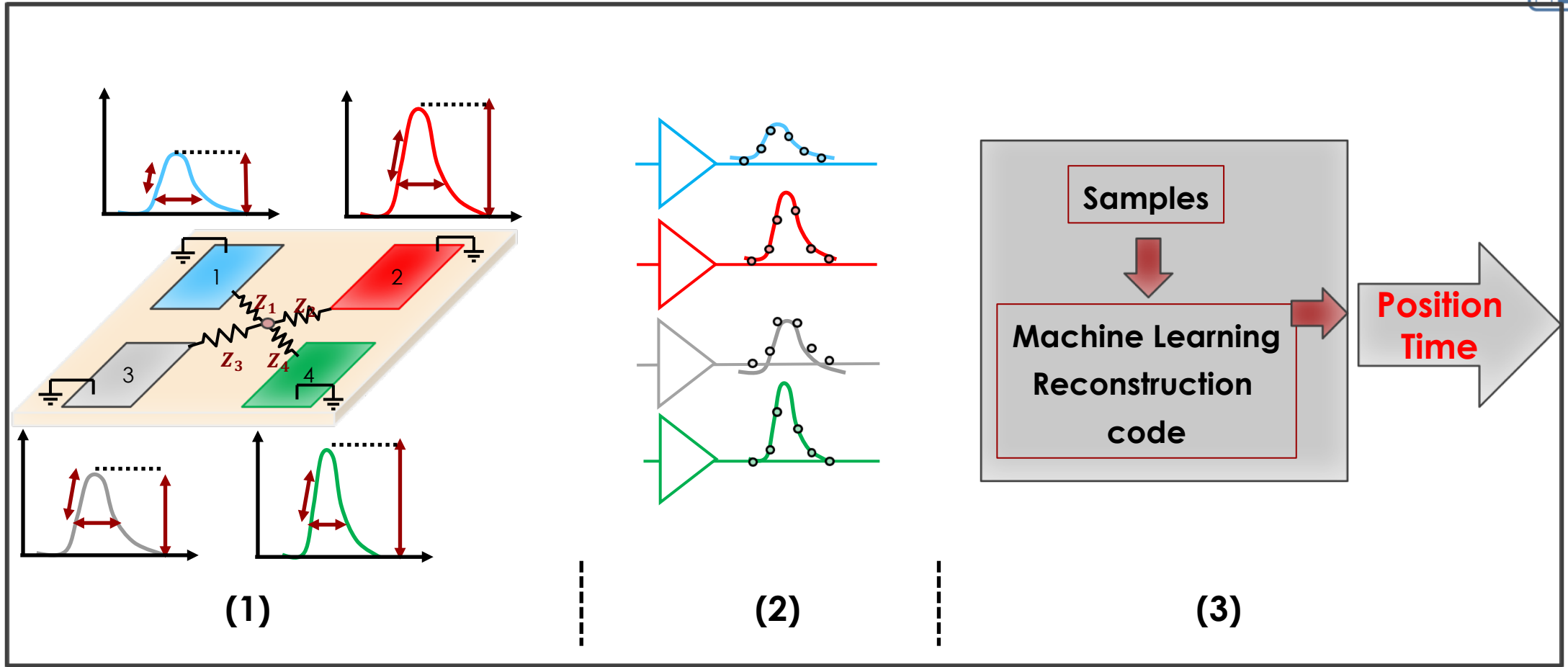
Analytic sharing laws are not able to capture all this information

Need to use

- Multiple sampling front-end
- Machine learning algorithm trained with real data, no need to have a “sharing law”



The "1 μm" project

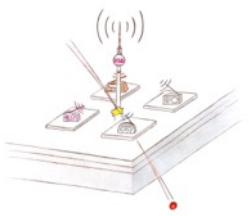


RSD sensor

Multiple sampling
frontend

Simplest design:
Time-over-threshold

Multi-inputs regression task
Trained using laser and
beam test data



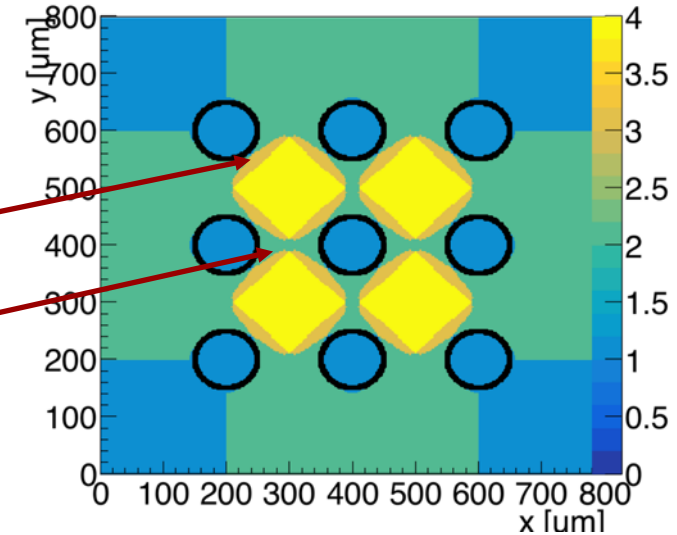
Position resolution: the geometry problem



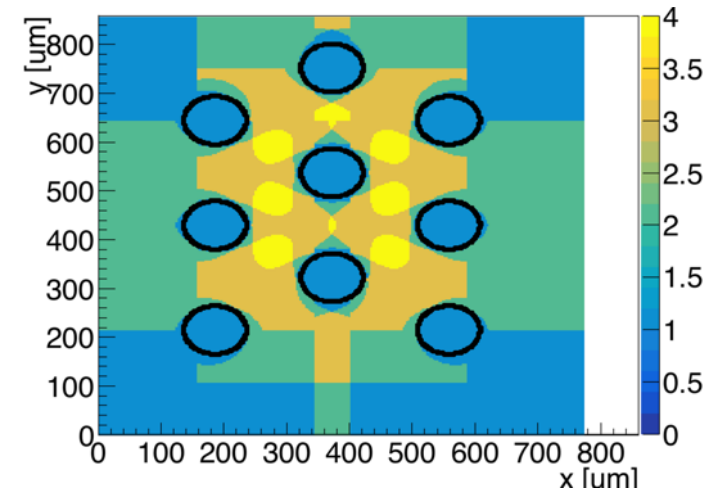
In a squared pixel geometry, **4 pads are necessary to obtain optimal resolution**

- **When only 3 pads are used**, the reconstructed position is “pulled away” from the missing pad
- **When 2 pads are used**, the hit position cannot be determined

100 – 200 Number of pads used in reconstruction
Amplitude = 120 mV, min amplitude = 15 mV



100 – 200 Number of pads used in reconstruction
Amplitude = 120 mV, min amplitude = 15 mV



Solution:

- ➔ Use triangular geometry, with equidistant pads
- ➔ In triangular geometry, **3 pads are necessary to obtain optimal resolution**
- ➔ **No region with 2 pads**

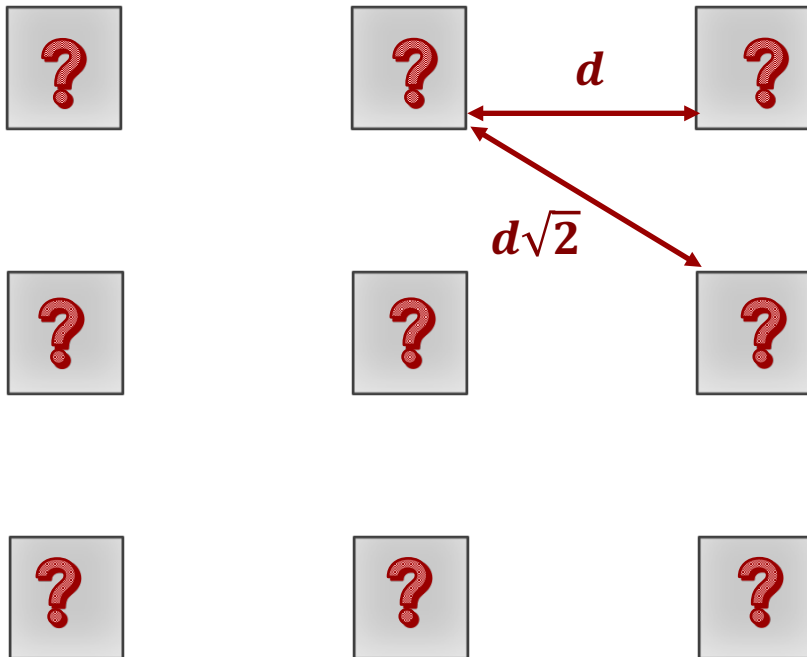
Position resolution: the metal problem



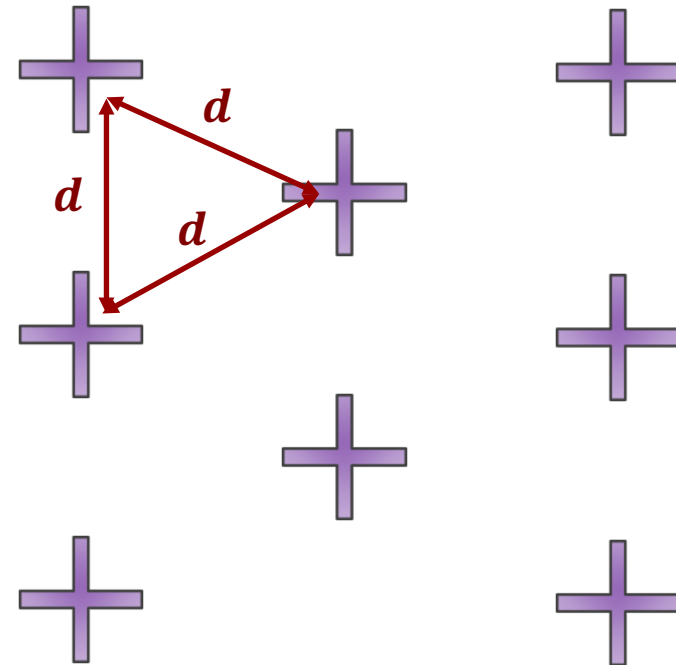
Lessons learnt:

- Very good position resolution ($\sim 3\text{-}5\ \mu\text{m}$) even with large pixels ($\sim 100\text{--}200\ \mu\text{m}$) can be achieved exploiting charge sharing
- The traditional “squared geometry” leads to a position-dependent space resolution
- Large metal pads prevent good hit localization
- **Uniform read-out is obtained when the distance between neighboring pad is the same**
- **The metal pads should be redesigned, using less metal**

Present design



Better design



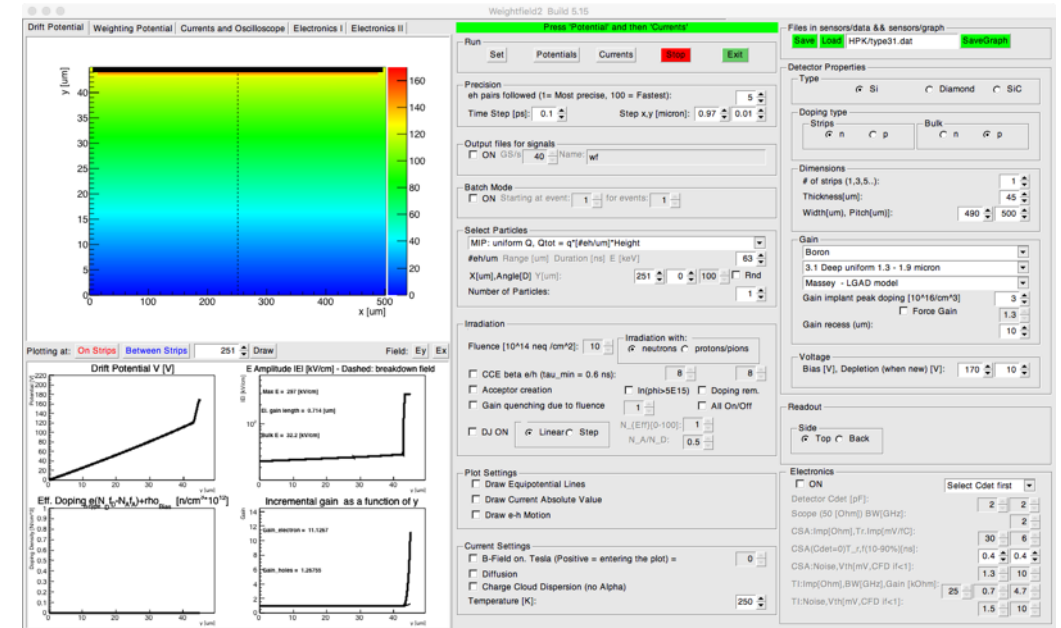


RSD Simulator: WF2_{RSD}



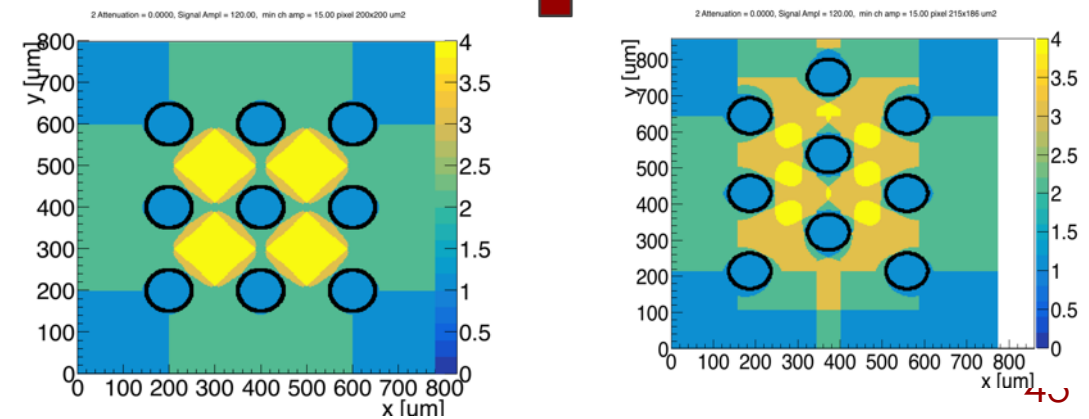
In the development of Ultra Fast Silicon Detectors we have written and extensively used a simulator, Weightfield2.

- <http://personalpages.to.infn.it/~cartigli/Weightfield2/Main.html>
- WF2 emulates the current signals produced in a UFSD.
- It includes non-uniform ionization, radiation damage, B field, temperature
- It requires Root build from source, it is for Linux and Mac.
- It will not replace TCAD, but it helps in understanding the sensors response



We has expanded WF2 to include RSD, incorporating the RSD main formula and the signal sharing among pads placed with any array geometry.

WF2_{RSD} emulates the charge sharing among pads and provide the current signals from each pad.

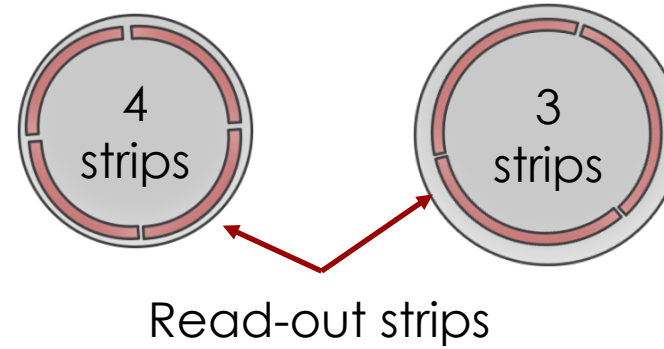




Where the wild things are



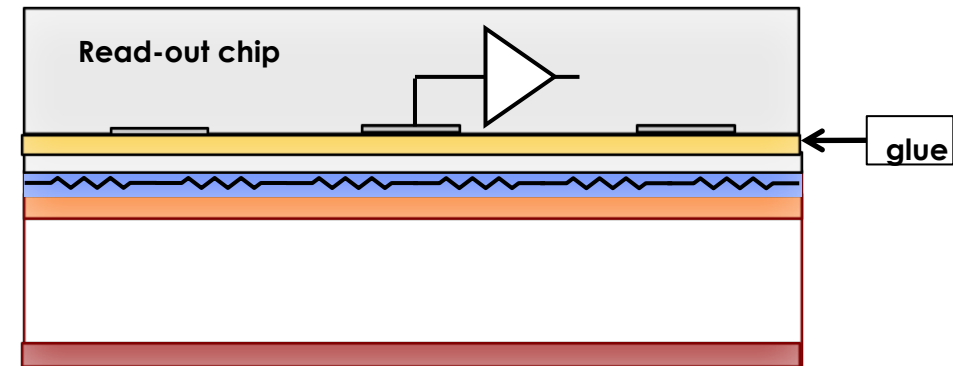
A circular RSD with 3 or 4 electrodes should be very accurate providing with a few channels excellent position ($\sim 5 \mu\text{m}$) and time ($\sim 35 \text{ ps}$) resolution. Looks promising for beam test apparatuses



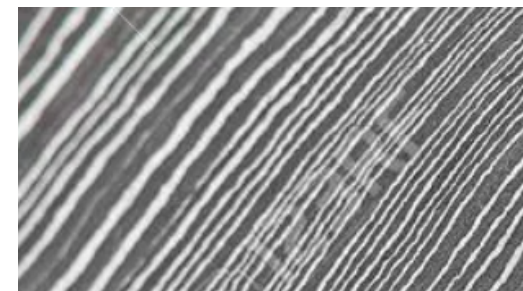
Universal RSD: no metal pad, glued to the ASIC.

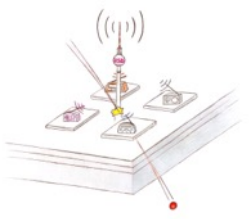
In RSD the signal is large, 5-10 fC, so it can be seen across a thin layer of glue.

The metal pads are provided by the read-out chip, no need to deposit metal pad on the RSD side.



Any metal pattern: as there is no implant underneath, the AC metal can be shaped into any pattern





It takes a village



Very special thanks to the UFSD group, for enduring endless weeks of measurements in the lab and many many meetings

R. Arcidiacono^{ab}, G-F Dalla Betta^{ae}, G. Borghi^{fa}, M. Boscardin^{fa}, M. Costa^{ac}, F. Fausti^{ac}, F. Ficorella^{fa}, M. Ferrero^{ab}, M. Mandurrino^a, J. Olave^a, L. Pancheri^{ae}, F. Siviero^a, V. Sola^a, M. Tornago^{ac}, G. Paternoster^f, H. Sadrozinski^d, A. Seiden^d, M. Centis Vignali^{fa}

^a INFN, ^b Università del Piemonte Orientale, ^c Università di Torino,

^d University of California, Santa Cruz, ^e Università di Trento, ^f FBK

Fermilab beam test team: A. Apreysan, R. Heller, K. Di Petrillo, S. Los.

Thank you for your attention



RSD are a novel n-in-p silicon device that evolves the LGAD design to obtain signal amplification with 100% fill factor and very strong signal sharing among pads

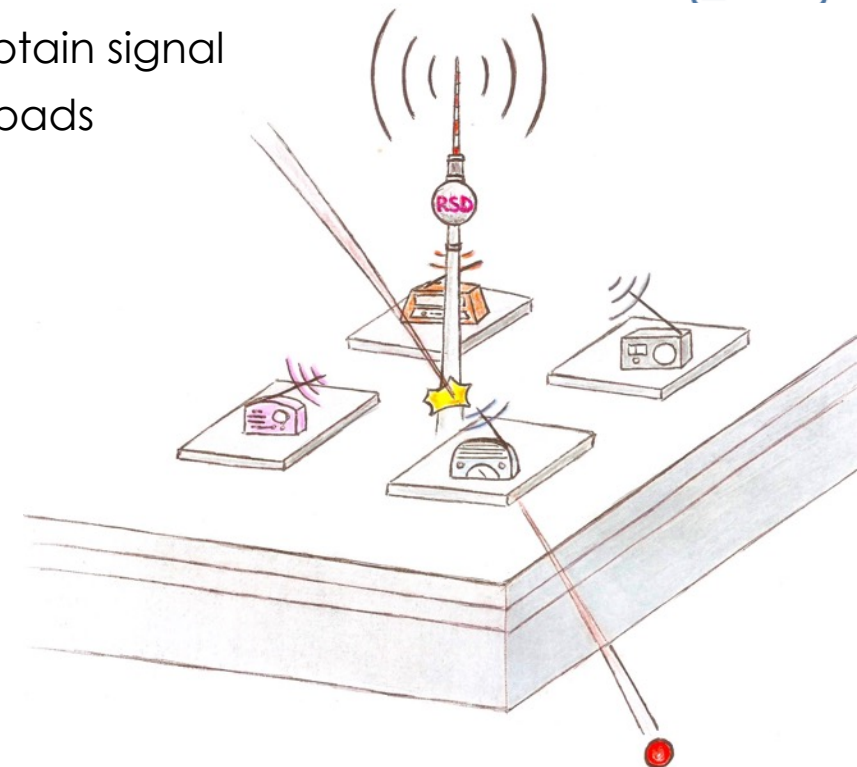
The RSD design maintains the excellent temporal resolution of UFSD sensors, $\sigma_t \sim 40$ ps for 50 μm thick sensors at gain ~ 15 .

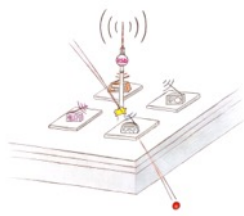
RSD exploits the resistive n+ layer to achieve charge sharing among pads. The spatial resolution is about 5% of the inter-pad distance:

Geometry	50 - 100	100-200	150 - 300	200-500
σ_x [μm]	4	5.5	5.9	15

The multiple signals germane to RSD are well suited for reconstruction algorithms based on machine learning. We expect that this technique will provide the ultimate spatial and temporal resolution

The extended signal sharing in RSD is a drawback in environment with high density of tracks and high irradiation. Most likely RSD and FCC-hh don't go together



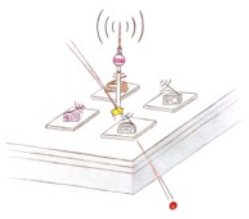


Acknowledgement



We kindly acknowledge the following funding agencies, collaborations:

- INFN - Gruppo V, UFSD and RSD projects
- INFN – FBK agreement on sensor production (convenzione INFN-FBK)
- Horizon 2020, grant UFSD669529
- U.S. Department of Energy grant number DE-SC0010107
- Dipartimenti di Eccellenza, Univ. of Torino (ex L. 232/2016, art. 1, cc. 314, 337)
- Ministero della Ricerca, Italia , PRIN 2017, progetto 2017L2XKTJ – 4DinSiDe
- Ministero della Ricerca, Italia, FARE, R165xr8frt_fare



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https://indico.cern.ch/event/351695/contributions/828366/attachments/695875/955507/TREDI_Cartiglia.pdf, N. Cartiglia, A. Seiden, H. Sadrozinski, *US Patent 9613993*

[2] M. Mandurrino *et al.*, "Demonstration of 200-, 100-, and 50- micron Pitch Resistive AC-Coupled Silicon Detectors (RSD) With 100% Fill-Factor for 4D Particle Tracking," in *IEEE Electron Device Letters*, vol. 40, no. 11, pp. 1780-1783, Nov. 2019.

[3] M. Mandurrino *et al.* "Analysis and numerical design of Resistive AC-Coupled Silicon Detectors (RSD) for 4D particle tracking" <https://doi.org/10.1016/j.nima.2020.163479>

[4] H. Sadrozinski, HSTD11, "[Time resolution of Ultra-Fast Silicon Detectors](#)",

<https://indico.cern.ch/event/577879/contributions/2740418/attachments/1575077/2487327/HSTD1--HFWS1.pdf>

[5] G. Giacomini, W. Chen, G. D'Amen, A. Tricoli, Fabrication and performance of AC-coupled LGADs, *JINST* 14 (09) (2019)

[6] M. Tornago *et al.*, "Resistive AC-Coupled Silicon Detectors principles of operation and first results from a combined laser - beam test analysis", <https://arxiv.org/abs/2007.09528>

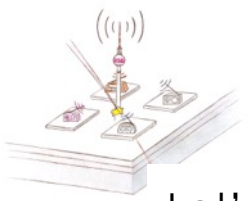
[7] F. Siviero *et al.*, "Application of machine learning algorithms to the position reconstruction of Resistive Silicon Detectors", paper in preparation

[8] A. Apresyan, "Measurements of an AC-LGAD strip sensor with a 120 GeV proton beam", <https://arxiv.org/abs/2006.01999>



Extra topics

Calculation of signal sharing



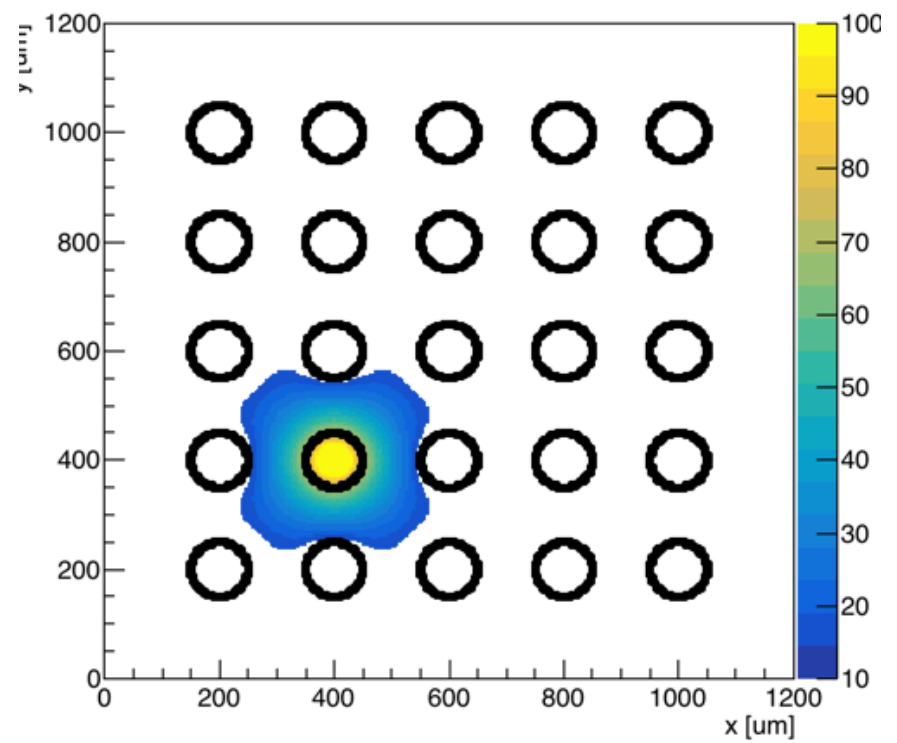
Let's use the RSD main formula to explore the following geometry (analytic calculation):

- Pixel matrix (round metal for simplicity) with metal – pitch = 100 – 200 micron
- Signal amplitude = 100 mV
- Min amplitude = 15 mV

Blue = 1 active pad: when the hit is on the pad, the signal does not spread much

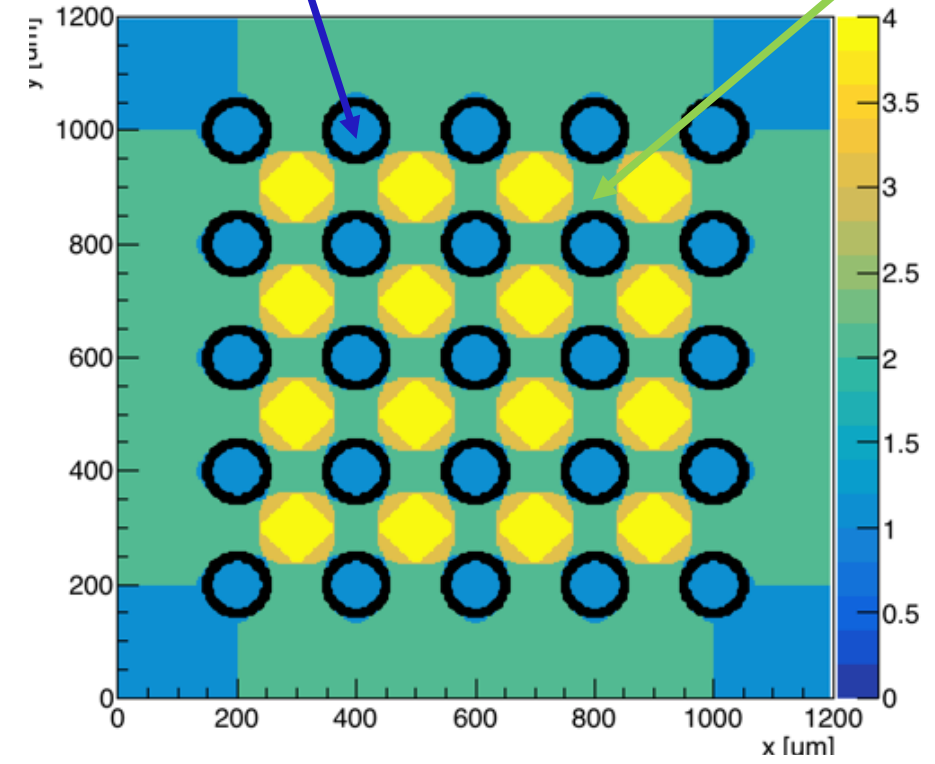
Green = 2 active pads: in between 2 pads

Signal seen by a pad as a function of distance



Good localized signal

Number of pads (1,2,3, or 4) with signal > 15 mV



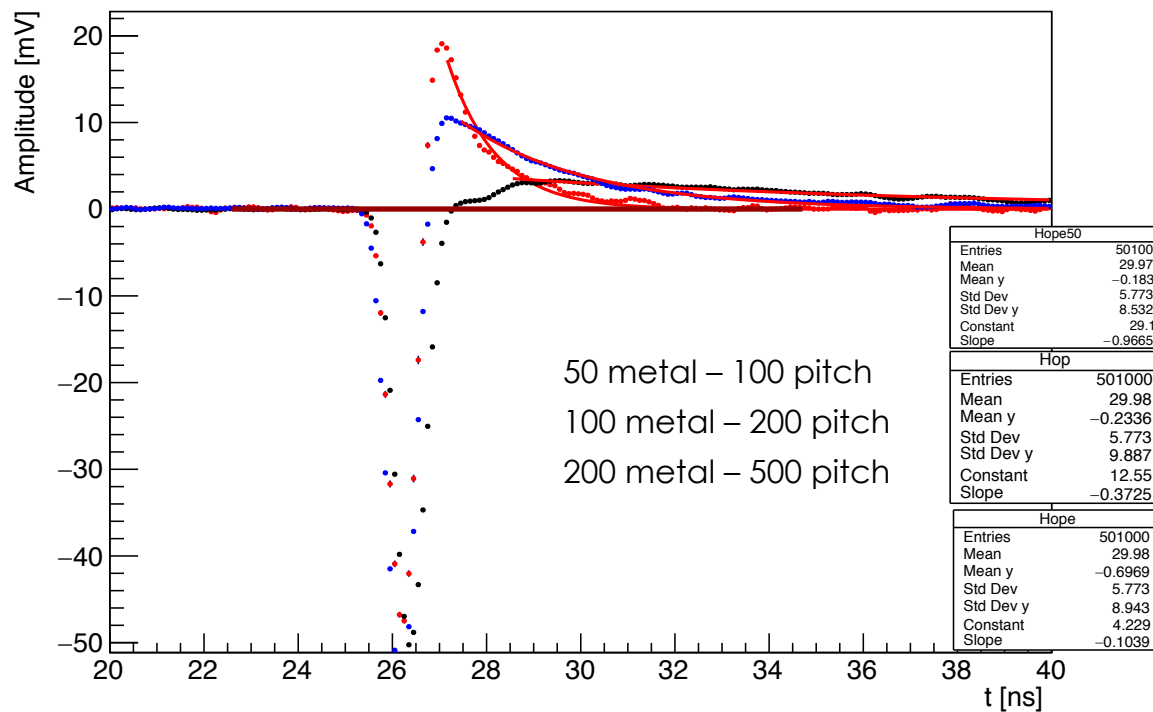
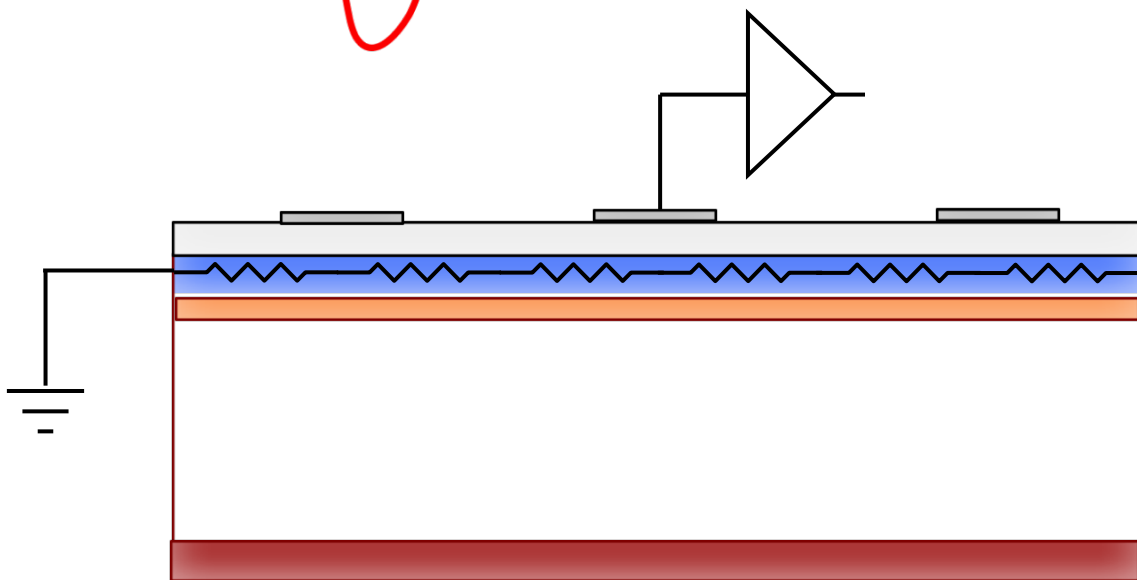
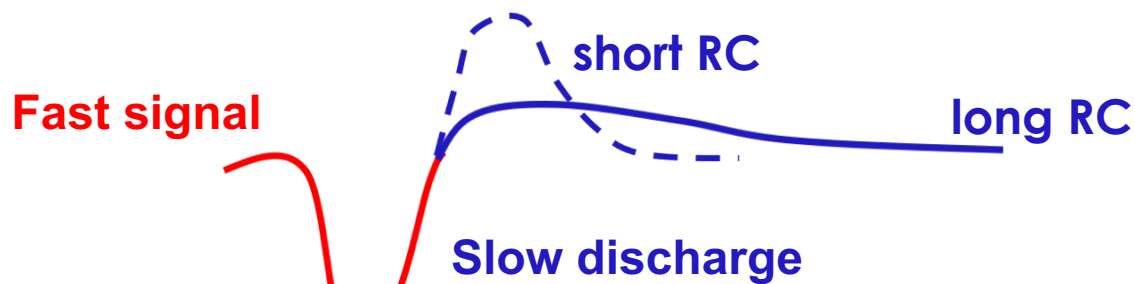
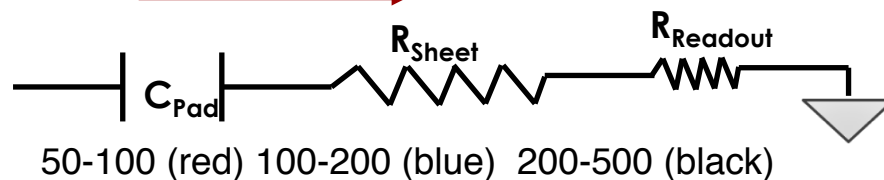
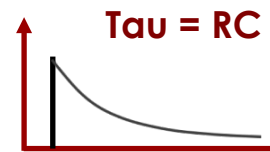
Not very uniform readout pattern

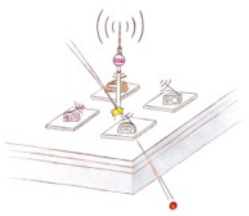
Signal discharge



The signal discharges, according to the read-out RC.

Small RC have larger and shorter positive lobes (need to discharge the same charge in a shorter time)





RSD strip detectors



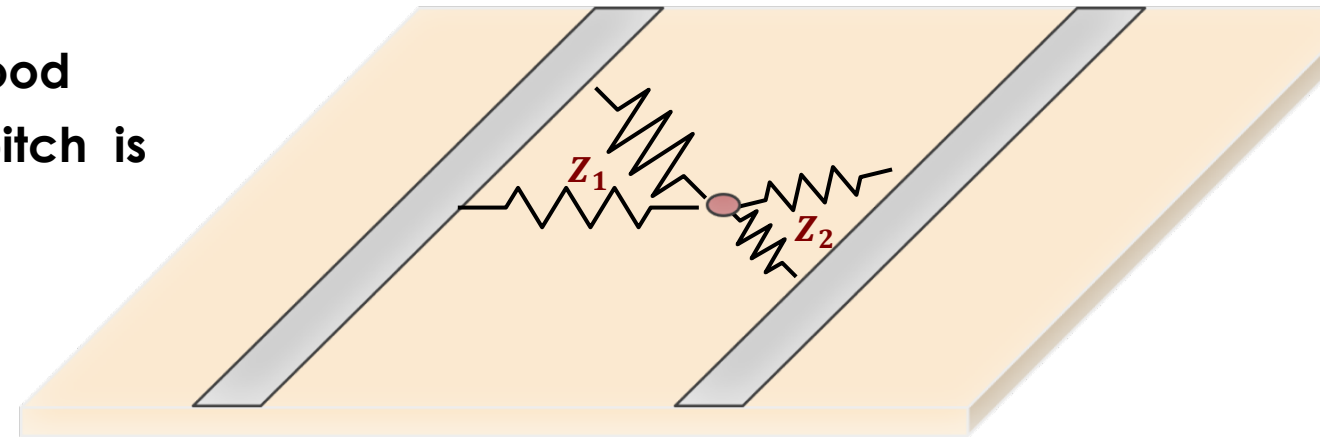
The FBK RSD1 sensor production included 2 type of strip designs.

We tested them with the TCT laser and they work fine.

This first design did no exploit completely the charge sharing capability

In the next productions, several strip pitch and metal width will be explored, using thin metal strips ($\sim 20\text{-}30\text{ }\mu\text{m}$) at increasing distance (50, 100, 200, 500 μm).

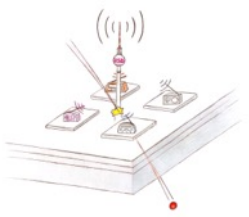
Given the very favorable geometry, very good position resolution ($\sim 5 - 10\text{ }\mu\text{m}$) with large pitch is expected



RSD strips should have small metal and large intergapd

Results on AC-LGAD strips manufactured by BNL was shown here: K. Di Petrillo,

https://indico.cern.ch/event/918298/contributions/3880513/attachments/2050888/3437589/2020.06.04.kdp.ACstrips_RD50.pdf



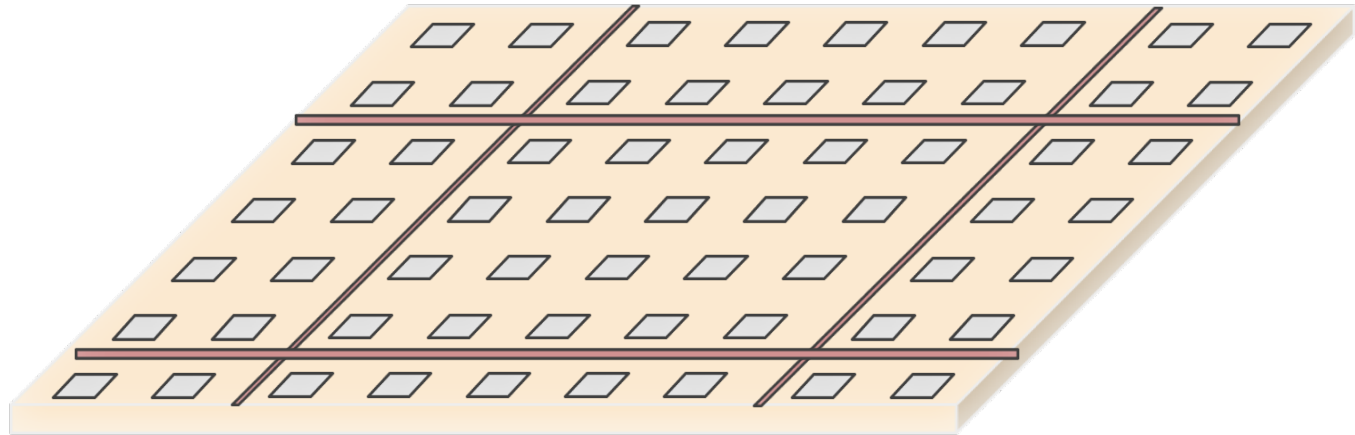
RSD large sensors



Pixellated RSD sensor have a single n-in-p diode.

This can be a problem in large detectors (in 6" wafers they can be $\sim 10 \times 10 \text{ cm}^2$)

Possible solution: insert a macro grid of ground contacts connected to the guard ring.



This grid isolates the macro area from each other, making the detector look like a sequence of smaller units

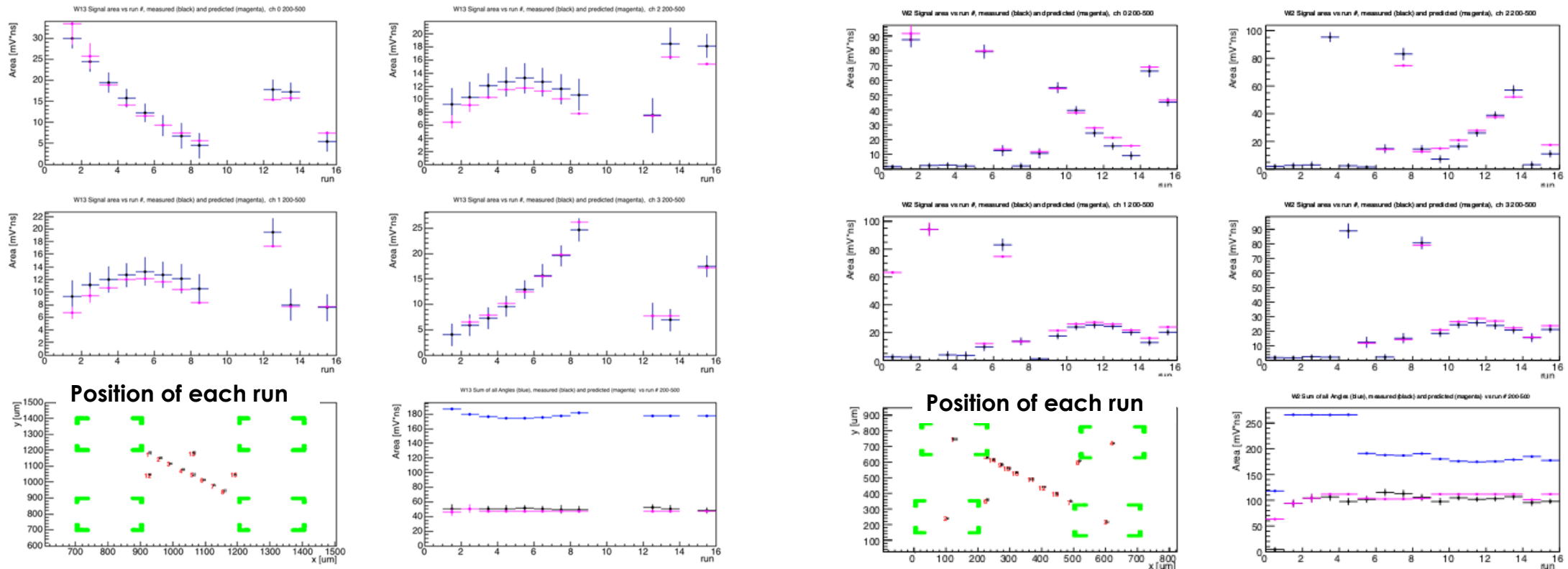
The RSD main formula vs n+ resistivity



The RSD main formula does not depend on the n+ resistivity since **it predicts the relative split** of signals among the pads.

$$S_i(\alpha_i, r_i) = \frac{\alpha_i}{\sum_1^n \frac{\alpha_i}{\ln(r_i)}}$$

Signal split among pads as a function of run number (black = measured, magenta = predicted)



RSD1 W13: low resistivity n+ implant

RSD1 W2: high resistivity n+ implant

The effect of n+ resistivity



What are the effects of n+ resistivity on the signal?

The signal is formed on the n+ layer, and it is coupled to the AC metal pad.

If the n+ is too conductive, it will not couple the charges to the AC metal pad

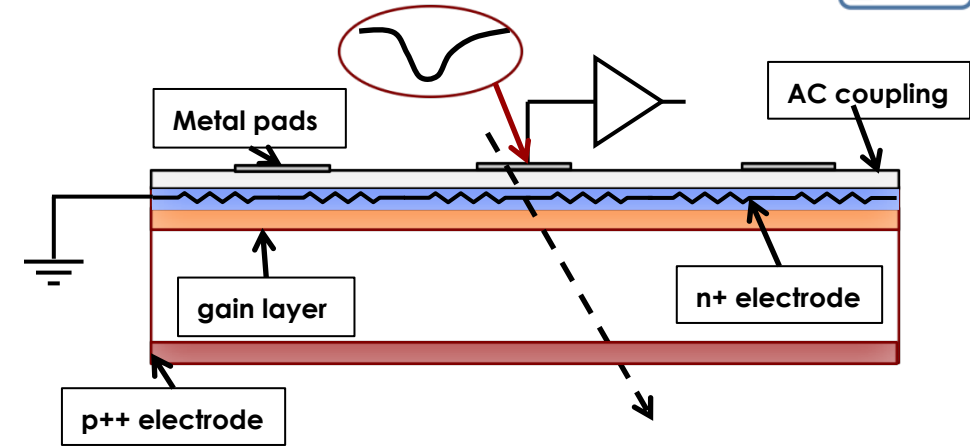
→ the AC amplitude decreases with increasing n+ doping.

In the limit of very conductive n+, there is no AC signal.

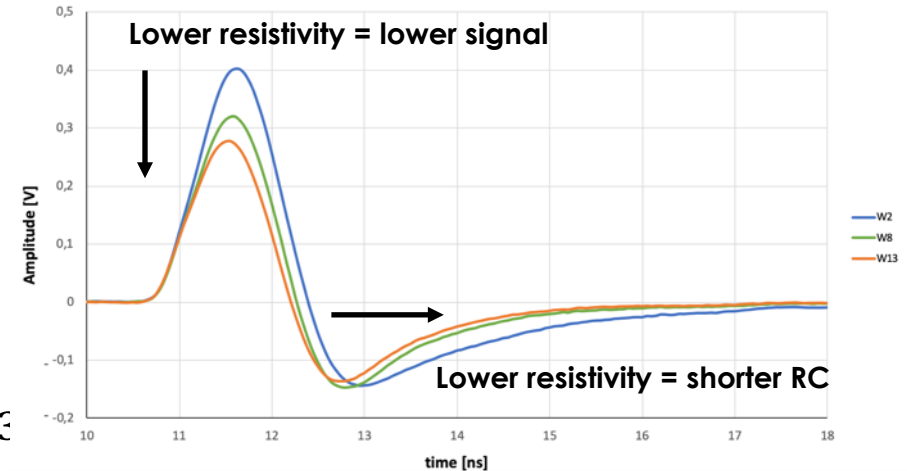
→ Additional effects, studied on RSD1 wafers (W13, W2) with $\frac{Doping\ W13}{Doping\ W2} \sim \frac{1}{3}$

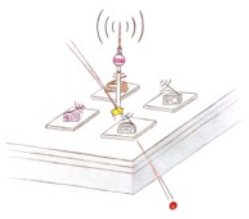
- RC discharge time is shorter at lower resistivity, ($\frac{\tau_{W13}}{\tau_{W2}} \sim 0.5$)

- The β [ns / $\frac{\ln(r)}{\alpha}$] coefficient, the delay, decreases at lower resistivity ($\frac{\beta_{W13}}{\beta_{W2}} \sim 0.8$)



Signals RSD 70-100 different n+ dose



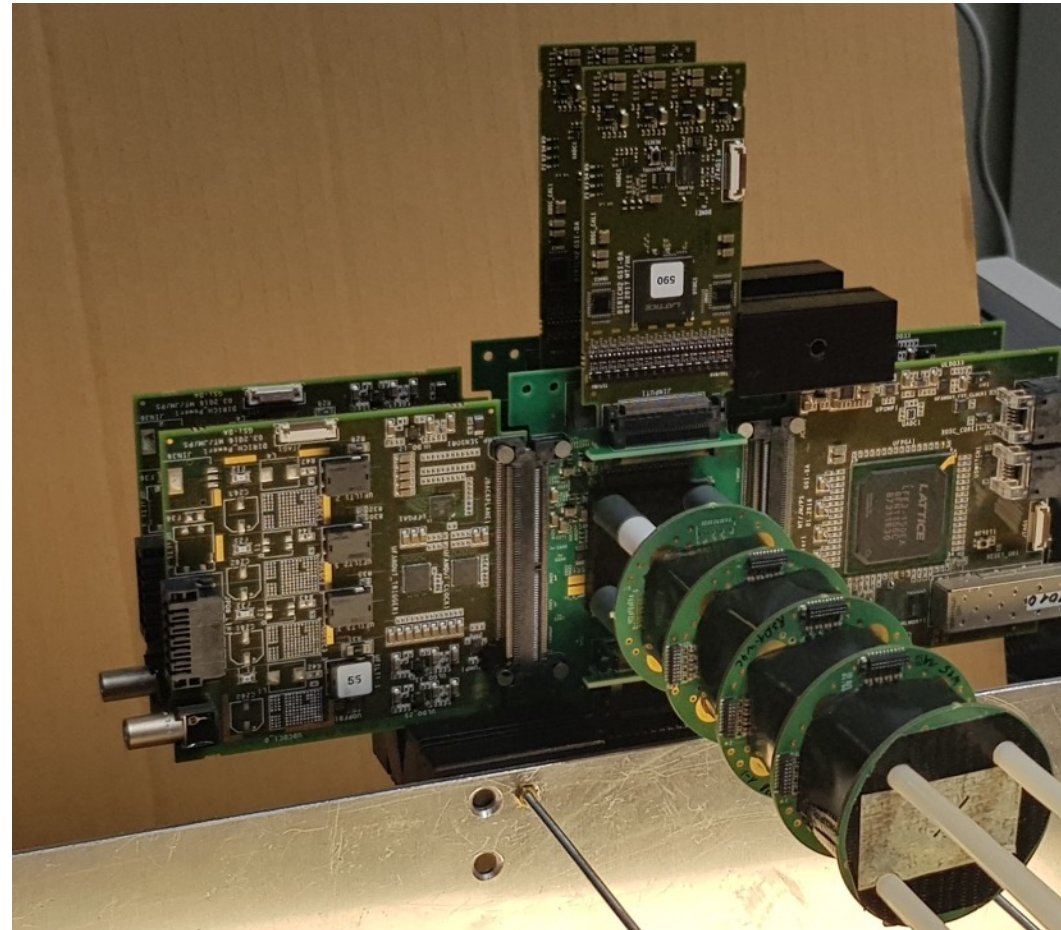


RSD use in HADES



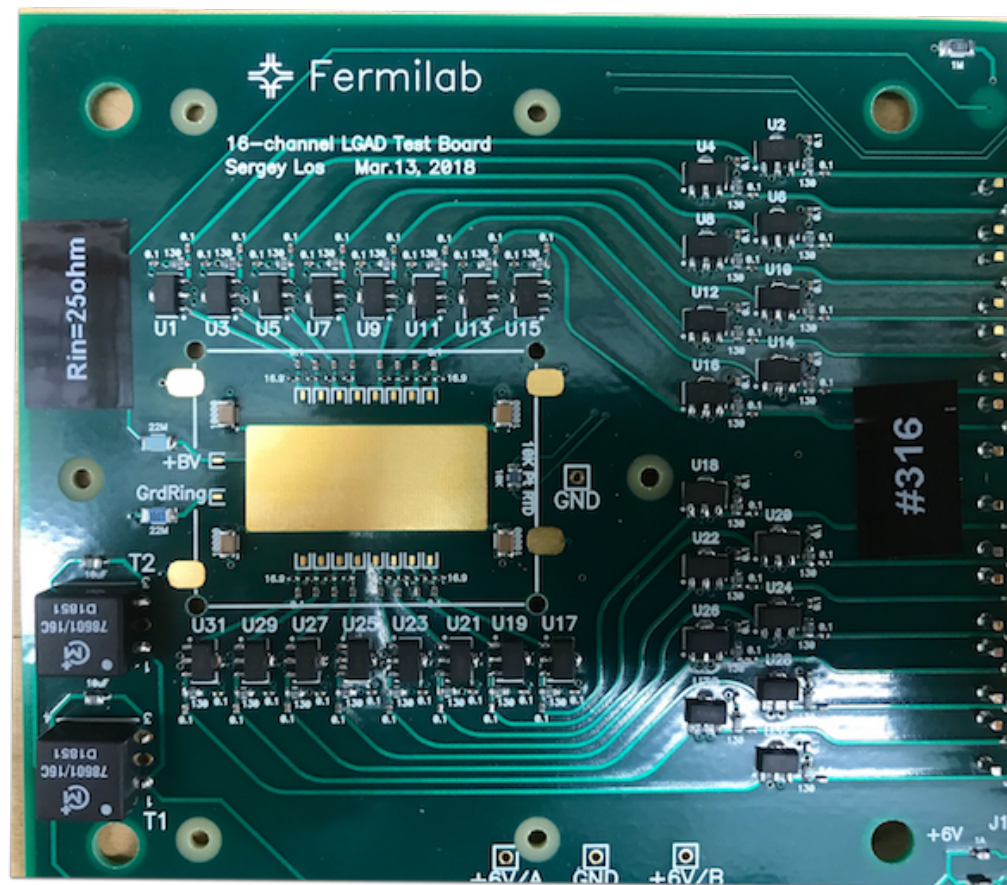
The HADES collaboration (GSI) has completed a beam test with a combination of UFSD and RSD strips.

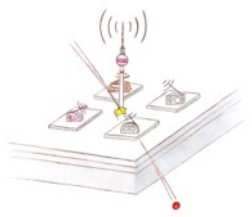
2.5 GeV/c protons, 1.2 MHz/ strip, results in the near future





FNAL 16-ch board





RSD radiation resistance

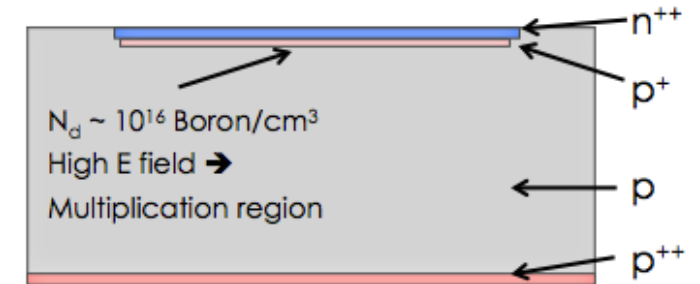


The effect of irradiation on RSD is similar to that of the other LGAD-based devices:

- Decrease of charge collection efficiency due to trapping
- Doping creation/removal
- Increased leakage current, shot noise

Most important fact: irradiation de-activate the gain layer

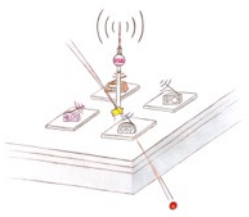
→ the electric field decreases, and the multiplication stops.



RSD has been irradiated, albeit not yet tested after irradiation.

Possible outcome: RSD will behave as the other LGAD-based devices, working well up to fluences of about $\sim 1E15 n_{eq}/cm^2$

Unknown: effect of enhanced oxide charges due to radiation to the AC coupling mechanism



Position reconstruction method: the recipe

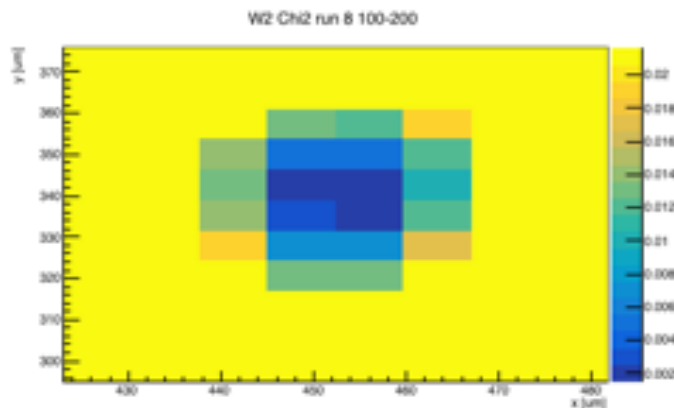


Recipe:

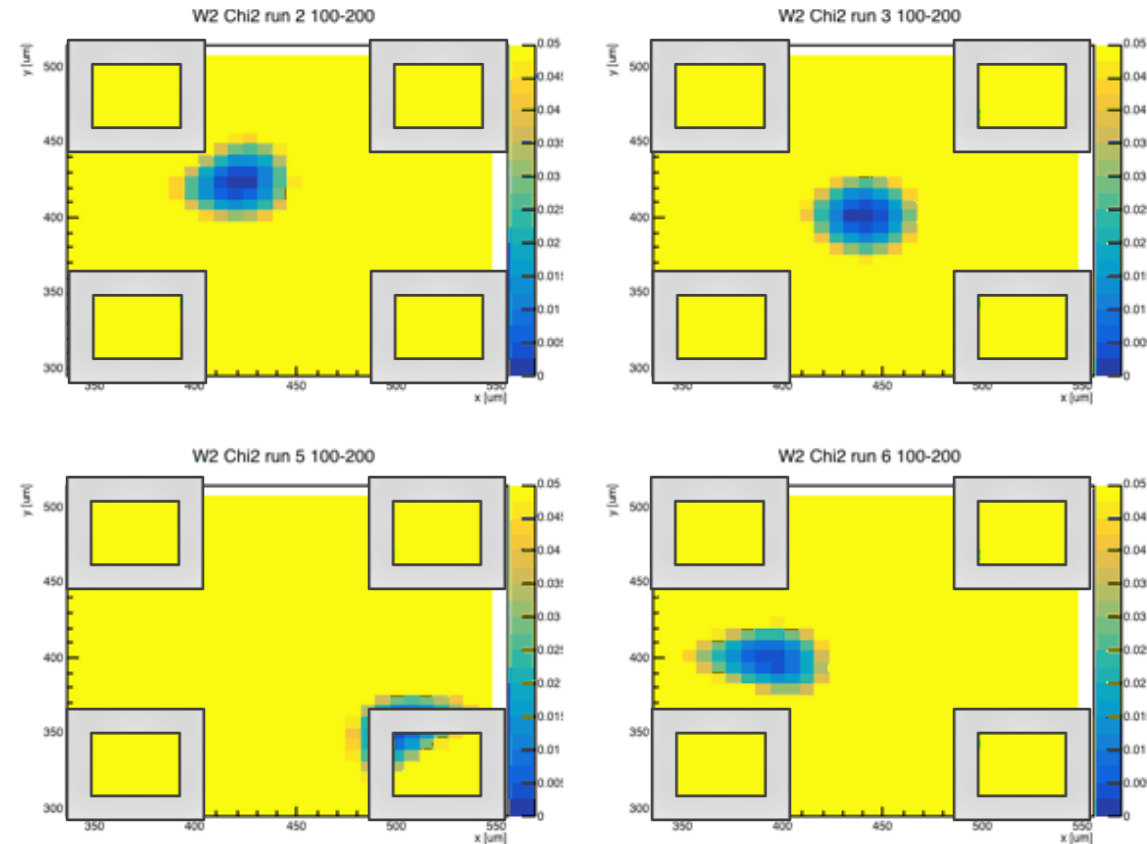
- For each position, using the RSD main formula, calculate S_i^{Calc}
- Find which x-y bin minimize the quantity:

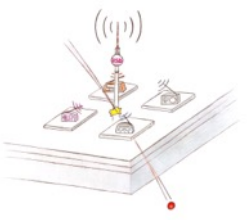
$$\chi^2 = \sum_1^4 \frac{[S_i^{Meas} - S_i^{Calc}]^2}{\sigma}$$

- Perform a local interpolation around the minimum.



χ^2 values for 4 different laser shots
(sensor geometry: 100-metal 200-pitch)
The reconstructed position is the bin with the minimum χ^2 value





Laser study: time resolution



The **hit time** is obtained combining the timing information from each pad, after correcting for delay

Geometry:

Temporal precision:

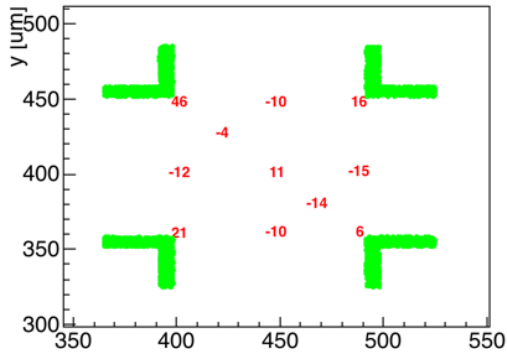
100 Metal, 200 pitch

28 ps

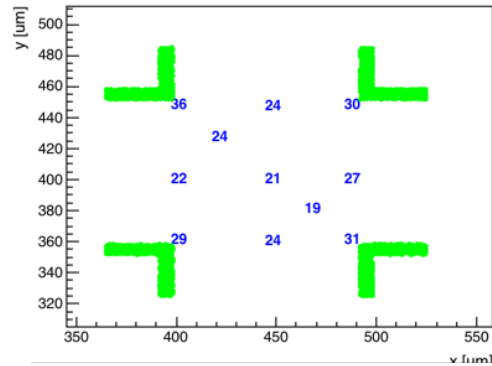
200 Metal, 500 pitch

35 ps

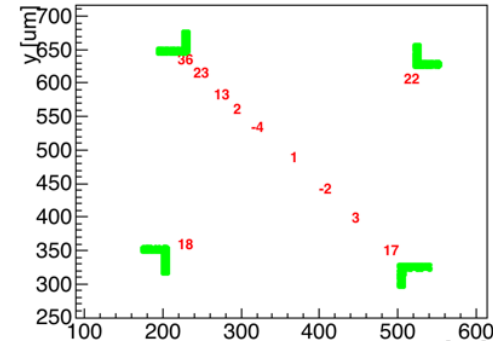
Offset at each point



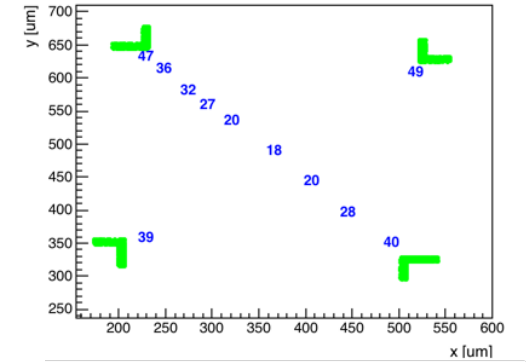
Resolution at each point



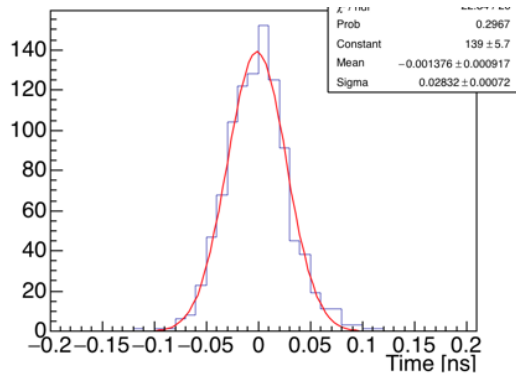
Offset at each point



Resolution at each point

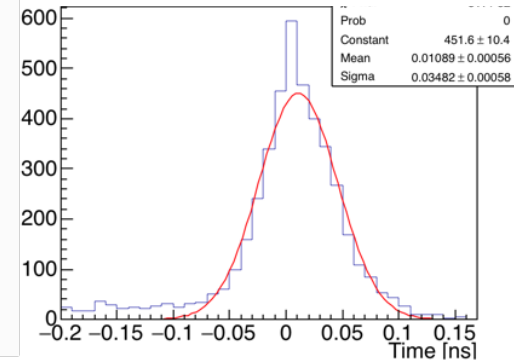


Total resolution



RSD maintain the “usual” excellent temporal resolution of standard UFSD

Total resolution





Fermilab beam test results

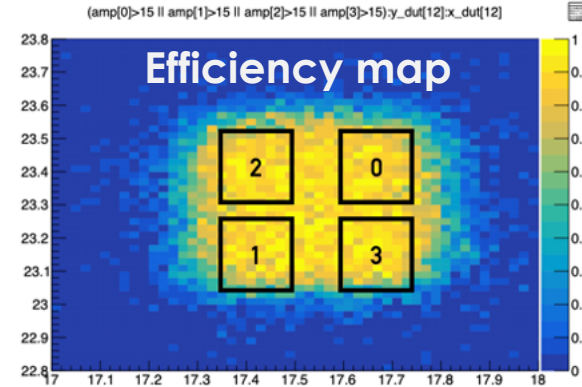


All details in: M. Tornago, 36th RD50 "Latest results on RSD spatial and timing resolution <https://indi.to/2cGQy>

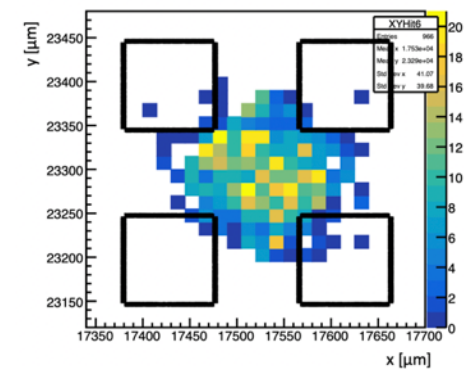
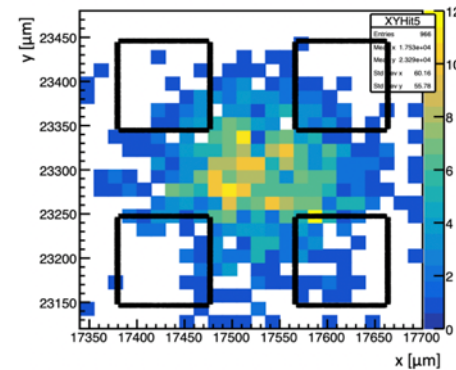
Data taken with RSD 3x3 100-200 and 190-200 geometries

Lesson learnt:

- RSD are ~ 100% efficient
- The RSD x-y hit reconstruction worked very well
- The time resolution is $\sigma_{t\ 100-200} = 44\ ps$, $\sigma_{t\ 190-200} = 42\ ps$ similar to UFSD results, limited by non-uniform ionization
- The metal size (100 vs 190 μm) does not influence the time resolution

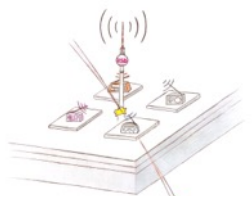


	single pad	3 pad	4 pad
100-200 laser	45 ps	Improves as $1/\sqrt{n}$ →	
100-200 test beam	50 ps	44 ps	-
190-200 test beam	35 ps	42 ps	-



x-y tracker reconstruction x-y RSD reconstruction

**Small improvement combining pads in beam test:
resolution limited by the effects of non-uniform ionization that are fully correlated**



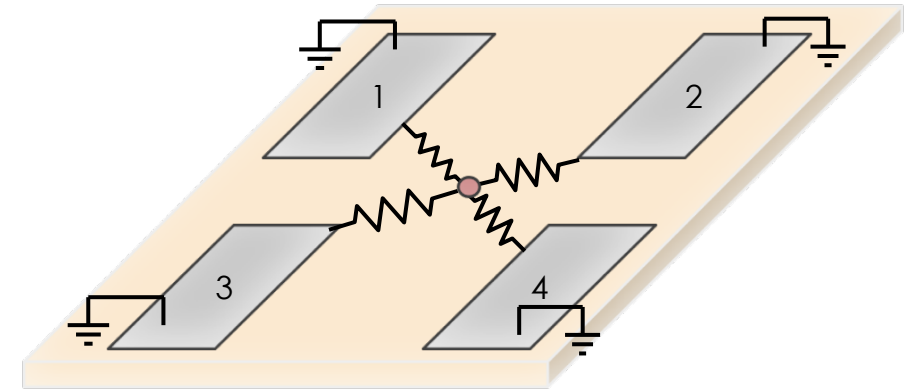
Laser study: signal delay



There is one more interesting point.

Let's compute the time of the event as the average time seen by the 4 pads:

$$RSD_{Time} = \frac{1}{4} \sum_1^4 t_i^{True} = \frac{1}{4} \sum_1^4 t_i^{Meas} - \beta \frac{1}{4} \sum_1^4 \frac{\ln(r_i)}{\alpha_i}$$



The sum of the resistivity, $\sum_1^4 \frac{\ln(r_i)}{\alpha_i}$, is actually a constant (it is equivalent of the signal amplitude) for every point of the sensor, **so it does not contribute to the time resolution**, it is just an offset → **no need to know accurately the delay**

$$\sigma_{tot}^2 = \sigma_{Trigger}^2 + \sigma_{RSD}^2 = \sigma_{Trigger}^2 + \frac{1}{4} \sqrt{\sum_1^4 \sigma_{t_i^{Meas}}^2}$$

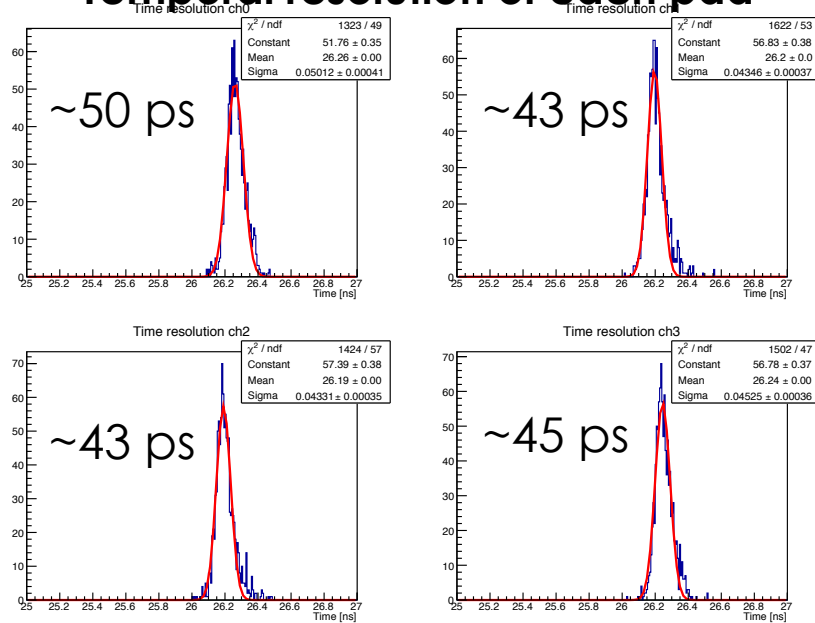


Laser study: time resolution



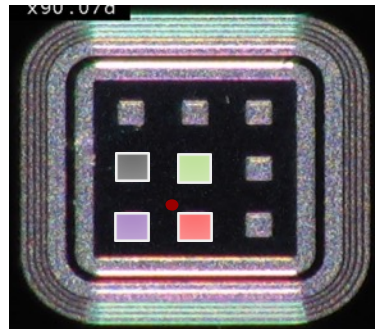
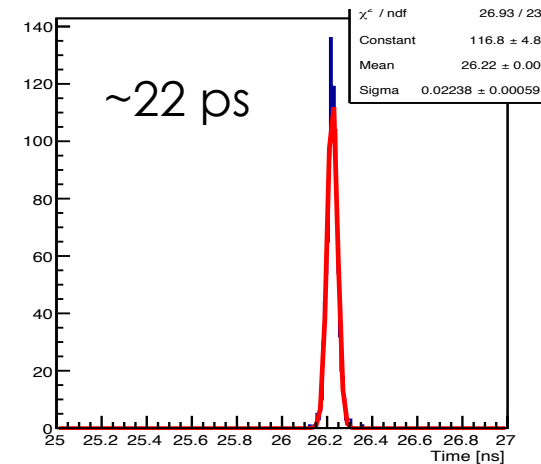
The **hit time** is obtained combining the timing information from each pad, after correcting for delay

Temporal resolution of each pad



~45ps/√4

4-pads combined temporal resolution



RSD show excellent temporal resolution and the combination of

multiple signals yields to $\sim \frac{1}{\sqrt{n}}$ improvements