



Global Solar Wind Model with Physicsbased Alfvén Wave Reflection

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Outline

M BATS-R-US

- **M** Alfvén wave turbulence driven corona and inner heliosphere model
- **M** March 7, 2011 Coronal Mass Ejection (CME): 1T versus 2T
- **M** Improved lower corona turbulence model with physics-based wave reflection
- **M** Summary



The BATS-R-US Multiphysics Code

Time-stepping Local explicit (CFL control) for steady state Global explicit Part steady explicit Explicit/implicit Point-implicit Semi-implicit Fully implicit

Conservation laws Hydrodynamics, MHD Ideal & non-ideal Hall Anisotropic pressure Semi-relativistic **Multi-species** Multi-fluid Ideal & non-ideal EOS

Numerics

Conservative finite-volume discretization 2nd (TVD), 4th (PPM) & 5th (MP) spatial order schemes Rusanov/HLLE/AW/Roe/HLLD

Splitting the magnetic field into B₀ + B₁ Divergence B control

CT, 8-wave, projection, parabolic-hyperbolic cleaning

Block Adaptive-Tree Solar-wind Roe-type Upwind Scheme

AMR Library (BATL)

Self-similar blocks Cartesian grid Curvilinear grid (can be stretched) Supports 1, 2 and 3D block-adaptive grids Allows AMR in a subset of the dimensions

Source terms

Gravity Heat conduction Ion-neutral friction Ionization Recombination Charge exchange Wave energy dissipation Radiative heating/cooling

Auxiliary equations

Wave energy transport Radiation transfer (multigroup diffusion) Material interface (level set) Parallel ray-tracing Tabular equation of state



Alfvén Wave Solar Model (AWSoM)

Inner boundary at T=50,000K (upper chromosphere)

- Density at inner boundary n=2×10¹⁷ m⁻³
- The Alfvén wave Poynting flux at the inner boundary is proportional to the surface magnetic field:

 $S_A = V_A w = C B$

where w is the Alfvén wave energy density at the inner boundary $C = (0.5 \div 1.5) \times 10^6 \text{ Jm}^{-2} \text{ s}^{-1} \text{ T}^{-1}$

Imbalanced turbulence on open field lines

≯w_

W

Radiative cooling

Wт

′W⊥

Heat conduction

Heat conduction

Balanced turbulence

at top of closed field lines

Radiative cooling

Wave dissipation $\varepsilon_{\pm} = \frac{w_{\pm}}{L_{\perp}\sqrt{\rho}}\sqrt{\max\left(w_{\mp}; C_{refl}^2 w_{\pm}\right)} \qquad L_{\perp}\sqrt{B} = const$ Open and bottom of closed field lines $\varepsilon_{\pm} \propto C_{refl}\sqrt{\frac{B}{\rho}} w_{\pm}\sqrt{w_{\pm}}$ Top of closed field lines $\varepsilon_{\pm} \propto \sqrt{\frac{B}{\rho}} w_{\pm}\sqrt{w_{\mp}}$ Here L_⊥ is the perpendicular correlation length of Alfvénic turbulence C_{refl} is a uniform reflection coefficient for wave mixing (0.01÷0.1)



Model Equations

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$$\begin{split} &\frac{\partial\rho}{\partial t} + \nabla\cdot(\rho\mathbf{u}) = 0 & \text{wave pressure} \\ &\frac{\partial\rho\mathbf{u}}{\partial t} + \nabla\cdot\left(\rho\mathbf{u}\mathbf{u} + p_p + p_e + \frac{B^2}{2\mu_0} - \frac{\mathbf{B}\mathbf{B}}{\mu_0} + \frac{w_+ + w_-}{2}\right) = -\rho\frac{GM_{\odot}}{r^2}\mathbf{e}_r \\ &\frac{\partial}{\partial t}\left(\frac{p_p}{\gamma-1} + \frac{\rho u^2}{2} + \frac{B^2}{2\mu_0}\right) + \nabla\cdot\left[\left(\frac{\rho u^2}{2} + \frac{\gamma p_p}{\gamma-1} + \frac{B^2}{\mu_0}\right)\mathbf{u} - \frac{\mathbf{B}(\mathbf{u}\cdot\mathbf{B})}{\mu_0}\right] \\ &= -(\mathbf{u}\cdot\nabla)p_e + \frac{n_pk_B}{\tau_{pe}}(T_e - T_p) + (1-\alpha)(\Gamma_+w_+ + \Gamma_-w_-) - \rho\mathbf{u}\cdot\mathbf{r}\frac{GM_{\odot}}{r^3} \\ &\text{wave energy} \\ &\frac{\partial}{\partial t}\left(\frac{p_e}{\gamma-1}\right) + \nabla\cdot\left(\frac{p_e}{\gamma-1}\mathbf{u}\right) + p_e\nabla\cdot\mathbf{u} \\ &= -\nabla\cdot\mathbf{q}_e + \frac{n_pk_B}{\tau_{pe}}(T_p - T_e) - n_pn_e\Lambda(T_e) + \alpha(\Gamma_+w_+ + \Gamma_-w_-) \\ &\text{heat} \\ &\text{collisional} \\ &\text{coupling} \\ &\text{wave energy} \\ &\text{dissipation} \\ \hline \frac{\partial w_{\pm}}{\partial t} + \nabla\cdot(\mathbf{u}w_{\pm}\pm\mathbf{b}V_Aw_{\pm}) + \frac{1}{2}w_{\pm}\nabla\cdot\mathbf{u} = -\Gamma_{\pm}w_{\pm} \\ &\text{wave energy} \\ &\text{wave energy} \\ &\text{dissipation} \\ \hline \end{array} \right) \\ &\Gamma_{\pm} = \frac{1}{L_{\perp}}\sqrt{\frac{\max\left(w_{\mp}, C_{refl}^2w_{\pm}\right)}{\rho}} \end{split}$$



M Synoptic magnetogram of Carrington rotation 2107 from *SDO/*HMI. The saturation value of the magnetic field is set to be 200 G in order to show the active regions more clearly.



Computational Grids



Solution for CR2107 (Feb-Mar 2011)

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In-situ validation

Validation with WIND



Validation with STEREO B





M M3.7 Flare occurred on March 7 (extended decay phase ~8 hrs).
M Followed by a very fast CME (~2200 km/s), SEP event, and radio bursts.



CME Initiation by Flux Rope Eruption



Analytical flux rope model first developed by *Titov & Demoulin (1999).*



 $I = 2.0 \times 10^{12} A$ R = 60 Mm r= 9 Mm Total Mass = $10^{16} g$ Total Free Energy = 7.2 x $10^{33} ergs$

V_r = 1000 km/s isosurface colored by proton temperature





- M The shock heating should only go to the protons due to the different sound speeds of electrons and protons (proton: ~100 km/s; electron: ~5000 km/s)
- In 1T the electron heat conduction also applies to protons. What are the consequences for the thermodynamics near the CME shock ?



M In the 1T model, a strong heat precursor is in front of the CME, which is caused by the electron heat conduction applied to the proton temperature jump at the shock.

M In the 2T model, the strength of the heat precursor is much smaller than 1T case. At the shock the protons are heated to ~85 MK.





Ppace Weather Modeling

M For 1T CME, the compression ratio is always larger than 4 (hypersonic limit), with the maximum value reaches >10. (caused by unphysical heat conduction behind the shock that cools down the plasma efficiently and allows the density to increase.)

M For 2T CME, the compression ratio is around 4 during the whole evolution.

2T model is needed to produce correct properties of the CME-driven shocks.



M Typical double front morphology (Voulidas & Ontiveros, 2009) in which faint front is caused by shock and bright front is coronal plasma piled up at the top of the erupting flux rope



Adaptive Mesh Refinement



Proton temperature gradient criterion is reasonably good for shock refinement.



- M Active regions are not as pronounced in the EUV images synthesized from simulations as in the observed images. What is missing in the lower corona model is enhanced wave reflected near active regions.
- **M** We apply the following steps (see also e.g. Chandran et al., 2011, Li and Habbal, 2012):
 - The nonlinear cascade is driven by partial reflection of outward propagating waves due to the gradients of the largescale solar wind parameters
 - Amplitude of reflected inward propagating wave is much smaller than the outward propagating wave
 - Inward wave cascades sufficiently fast compared with their wave periods



Line-of-Sight Integrated Images Stereo A, March 7 2011

Observation New model (TVD) New model (MP5)

171 Å (1.0 MK)

195 Å (1.4 MK)





Line-of-Sight Integrated Images Stereo A, March 7 2011

Observation Old model (MP5) New model (MP5)





Line-of-Sight Integrated Images Stereo B, March 7 2011



171 Å (1.0 MK)

195 Å (1.4 MK)





Summary



M Previous two-temperature, Alfvén wave turbulence driven solar coronal and inner heliosphere model

- Inner boundary is in the upper chromosphere, outer boundary beyond Earth's orbit
- Solution Very small number of free parameters (L_{\perp} , C_{refl})
- **M** Validation with SOHO, STEREO, SDO, ACE and WIND
- **M** 2T CME simulations show proton shock heating
- M 1T simulations show unrealistic heat precursor and compression ratios
- M New improved solar lower corona model
 - Physics-based wave reflection
 - Simulated STEREO EUVI images start to resemble observations.
 - High order schemes help to resolve the details in these images.