

Status of Cryogenics for

Large Cryogenic Gravity Telescope, KAGRA

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and KAGRA Collaboration

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abstract

- KAGRA is a name of project for Large Cryogenic Gravity Telescope, LCGT, having 3 km base line length in Japan, and was accepted by MEXT¹ on FY2010.
- The notable characteristic features of KAGARA are a power-recycled Fabry-Perot-Michelson interferometer using mirrors cooled down to 20 K, and placed underground at Kamioka mine. The characteristic design policy of KAGRA is to reduce thermal noise by cryogenic mirror, and escape from thermal lens effect that may reduce the optical power in Fabry-Perot cavities.
- The fundamental technique of cryogenic mirror was developed by a research with Cryogenics Science Center of KEK.
- A group in Cryogenics Science Center of KEK grapples with KAGRA cryogenic design, and start production of cryostats with very low vibration cryocooler units under MOU exchanged among KEK, ICRR² and NAOJ³.
- ¹⁾ Ministry of Education, Culture, Sport, Science and Technology in Japan
- ²⁾ Institute for Cosmic Ray Research (ICRR) of the University of Tokyo
- ³⁾ National Astronomical Observatory of Japan

Outline

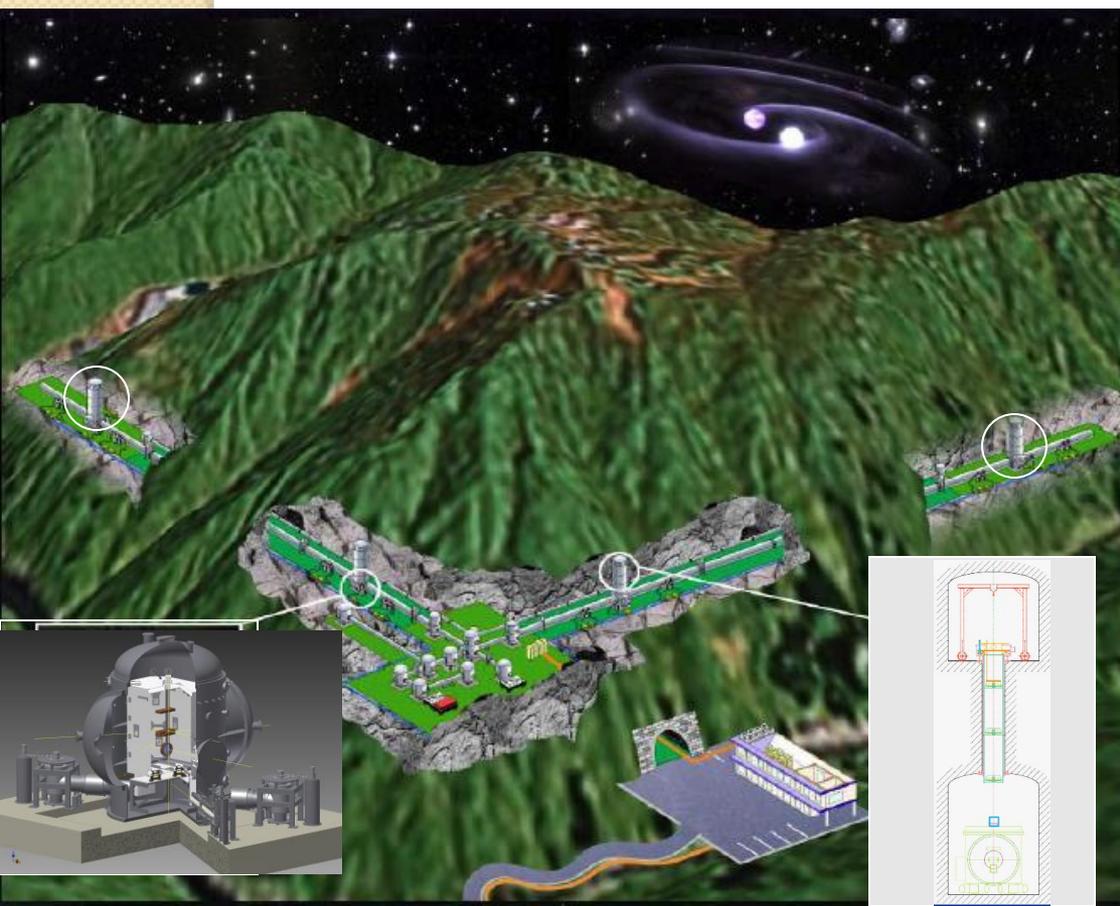
- ✓ *Overview of KAGRA*
- ✓ *Required specifications for the KAGRA Cryogenics*
- ✓ *Cryogenic design*
 - *Components*
 - *Mechanical Analysis*
 - *Thermal Analysis*
 - *Performance of the proto-type cryo-cooler unit*
- ✓ *Schedule*
- ✓ *Summary*

KAGRA Over View of KAGRA

Large-scale Cryogenic Gravitational wave Telescope (abbreviation of the project name)

Objectives

1. Detect gravitational wave for the first time.
2. Begin gravitational wave astronomy.



Peculiarities:

(1) Underground tunnel

Ikenoyama, Kamioka, Gifu

From the surface

Vertical > ~200m

Horizontal > ~400m

(2) Arm length 3km

(3) Cryogenic Mirrors

T=20 K, Sapphire Mass=30 kg

Target: In-spiral of
Neutron Star binary.

Summary of detector parameters

Laser

Nd:YAG laser (1064nm)

Master Laser + Power Amplifier

Power : **180 W**

Main Interferometer

Broad band RSE configuration

Baseline length : 3km

Beam Radius : 3-5cm

Arm cavity Finesse : 1550

Power Recycling Gain : 11

Signal Band Gain : 15

Stored Power : **771kW**

Signal band : **230Hz**

Vacuum system

Beam duct diameter : 80cm

Pressure : **10^{-7} Pa**

Mirror

Sapphire substrate
+ mirror coating

Diameter : 25cm

Thickness : 15cm

Mass : 30 kg

Absorption Loss : 20ppm/cm

Temperature : **20 K**

$Q = 10^8$

Loss of coating : 10^{-4}

Final Suspension

Suspension + heat link
with 4 Sapphire fibers

Suspension length : 30cm

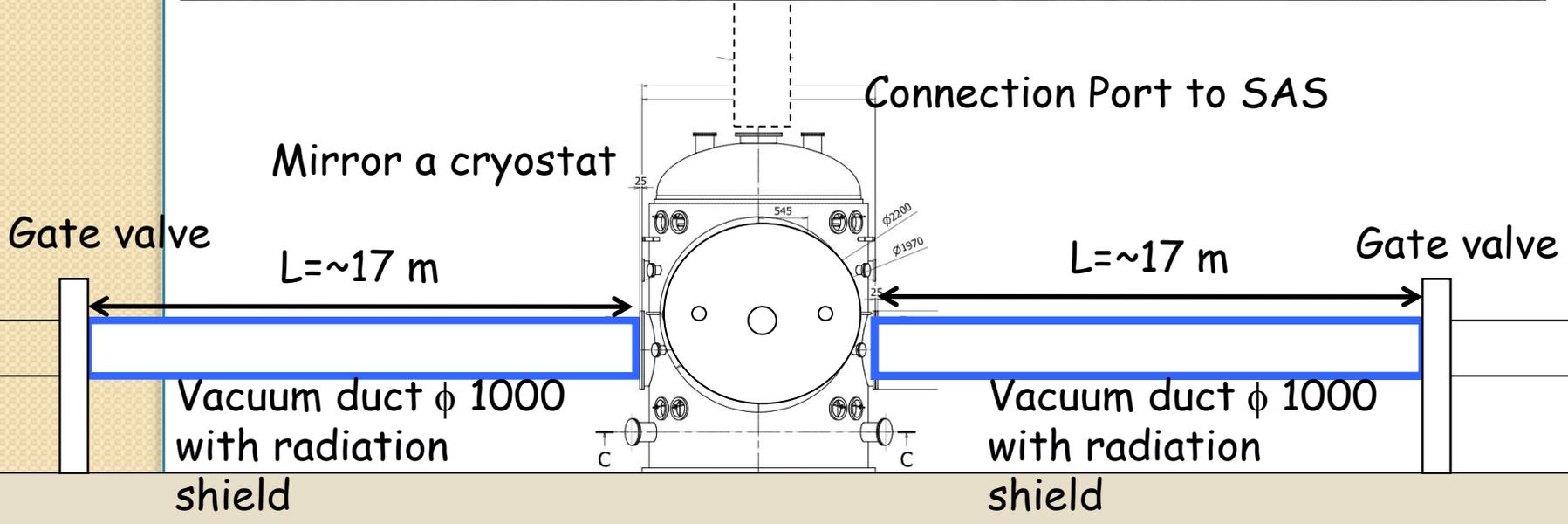
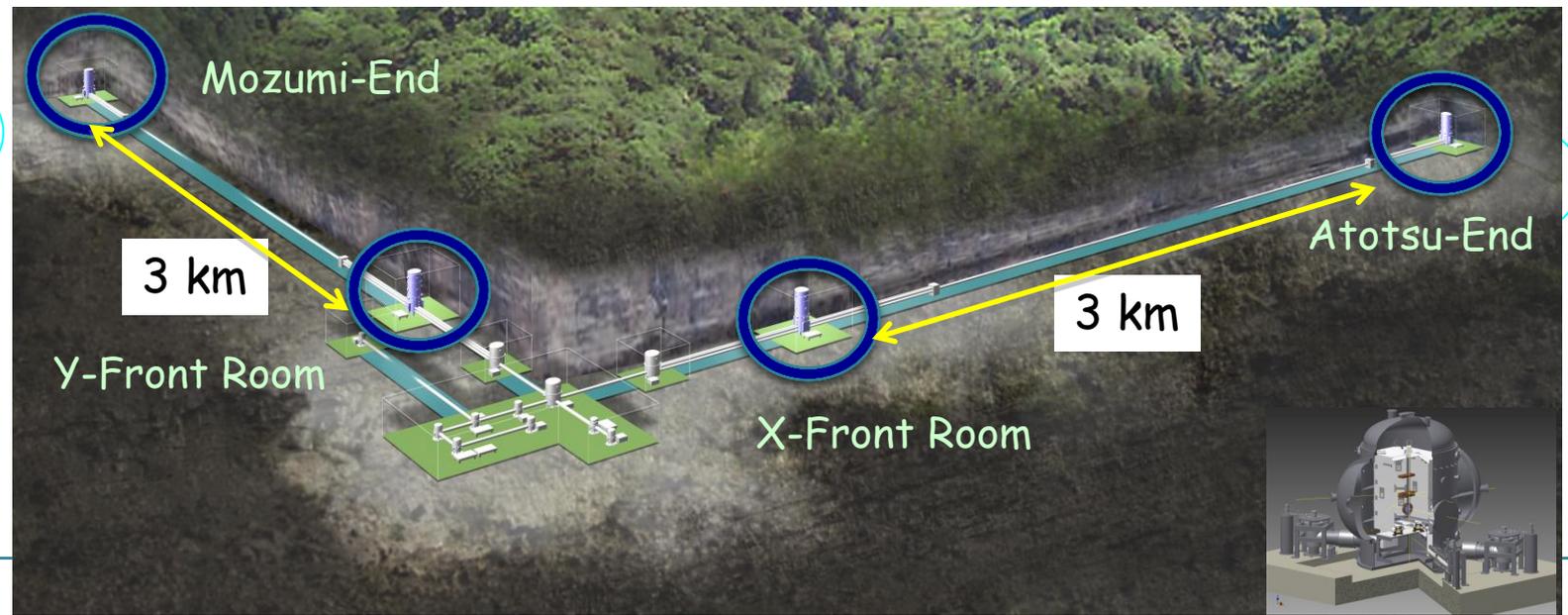
Fiber diameter : 1.6mm

Temperature : **16K**

Q of final suspension : 10^8

by Dr. M. Ando (NAOJ)

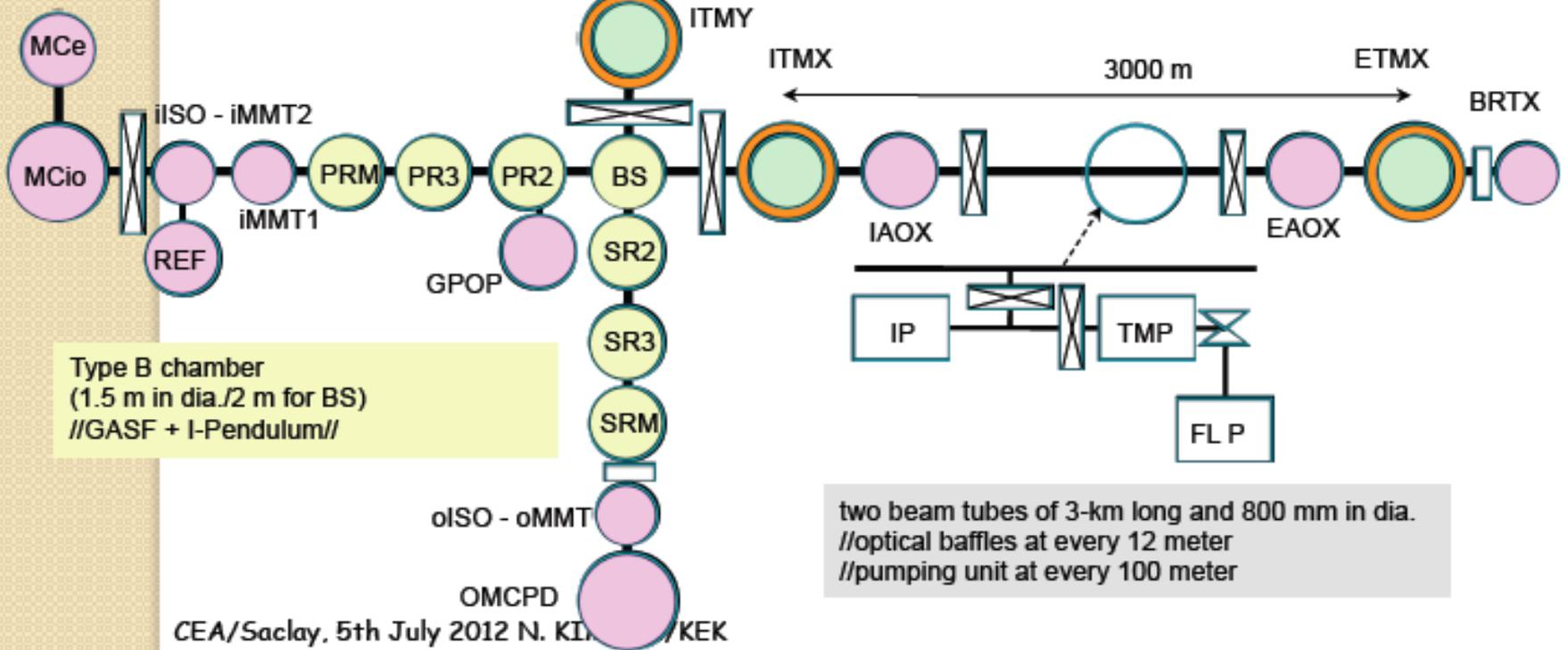
Location of Four Mirror Cryostats with the Cryo-coolers for the KAGRA



KAGR Vacuum System Layout

120525 VAC (YS)

- ETM:** end test mass <= with Cryostat
- ITM:** input test mass <= " "
- BS:** beam splitter
- IAO/EAO:** auxiliary optics of input/end
- MC:** mode cleaner
- PRM:** power recycling mirror
- SRM:** signal recycling mirror
- MMT:** mode matching telescope
- ISO:** isolator
- PD:** photo detector
- BRT:** beam reducing telescope.



Type A double chamber (2.4 and 1.5 m in dia.)
//GASF + I-Pendulum + cryogenic//

Type C chamber
(1, 1.2, 1.5 m in dia./ 2 m for MC)
//stack + D-Pendulum//

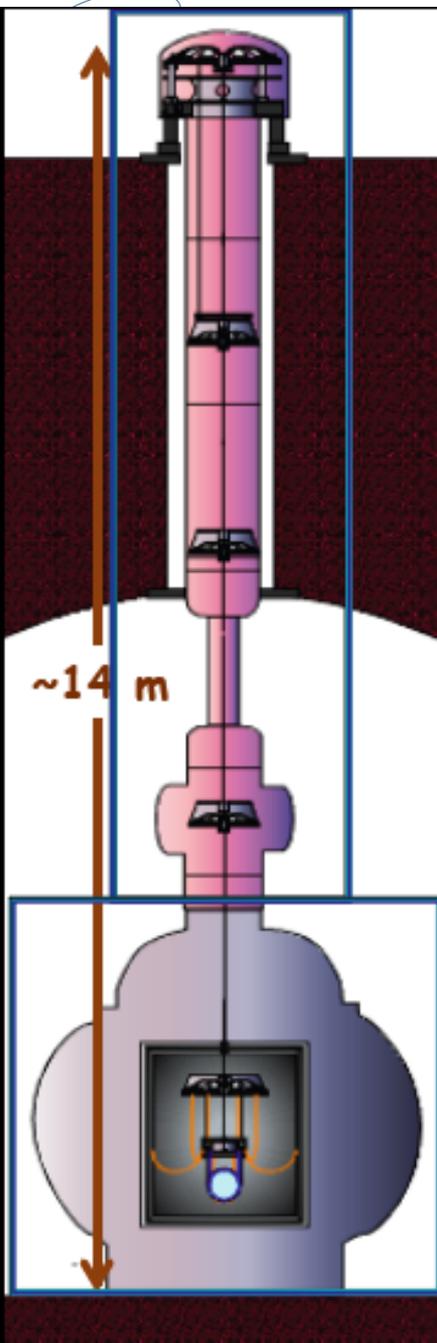
Type B chamber
(1.5 m in dia./2 m for BS)
//GASF + I-Pendulum//

two beam tubes of 3-km long and 800 mm in dia.
//optical baffles at every 12 meter
//pumping unit at every 100 meter

CEA/Saclay, 5th July 2012 N. KIMURA/KEK

Structure of the vacuum tank for KAGRA Test Mass

- The vacuum tank for KAGRA Test Mass has two layer structure having ~14 m height.
- Two layers are connected with each other vacuum pressure level less than $\sim 10^{-7}$ Pa.
- Upper layer of the tank is installed three Seismic Attenuation Systems for KAGRA Test Mass.
- Lower layer of the tank is installed mono crystal sapphire mirror with a cryogenic suspension cooled down to less than 20 K.



Required specification for the KAGRA Cryogenics

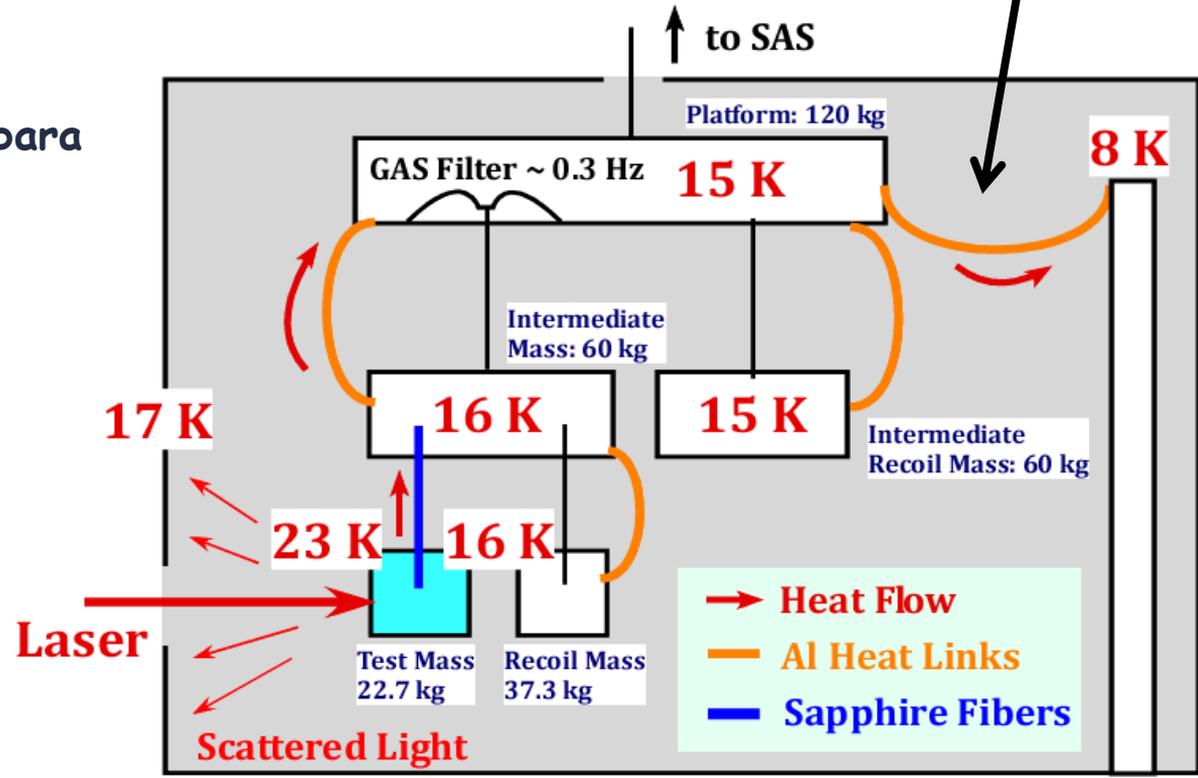
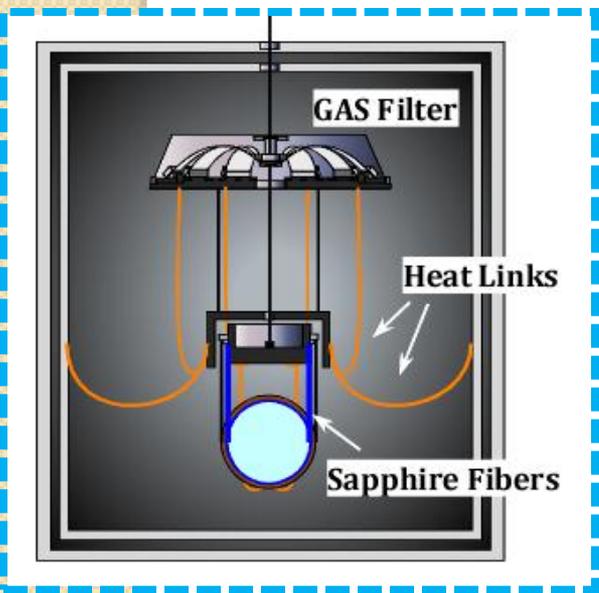
- Temperature of the mirror
(mono crystal sapphire, mass=30 kg) < 20 K.
- Inner radiation shield have to be cooled < 8 K.
- The mirror have to be cooled without introducing excess noise, especially vibration from the cryo-coolers.
- Accessibility and enough space for the installation work around the mirror in the cryostat.
- Satisfy ultra high vacuum specification $< 10^{-7}$ Pa.

Cooling Scheme of the mirror

- Heat transferred via pure aluminum heat links.

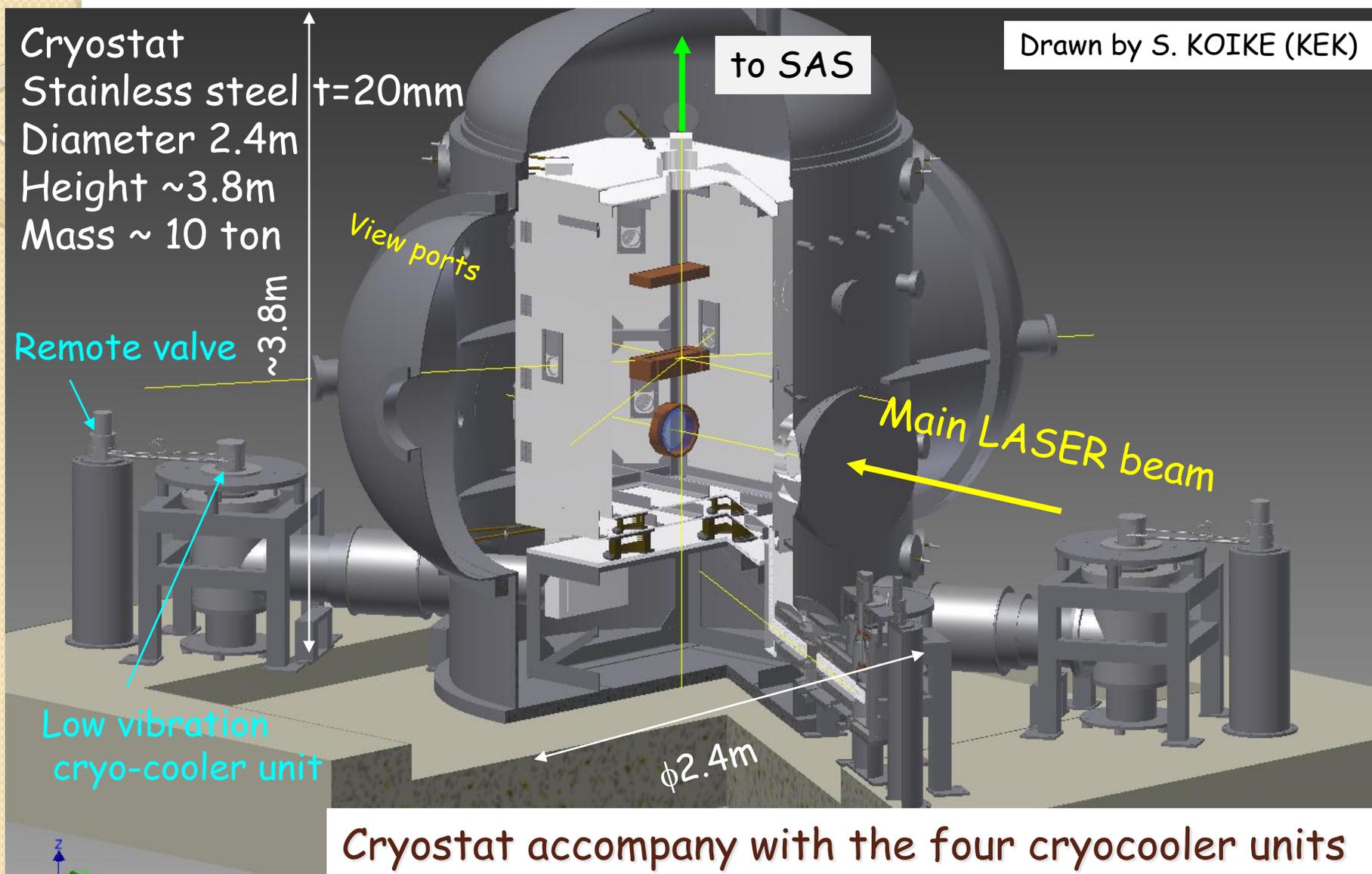
We need $\Phi 1$ mm, L=1 m heat links x 7~8

Thermal simulation
Done by Y. Sakakibara



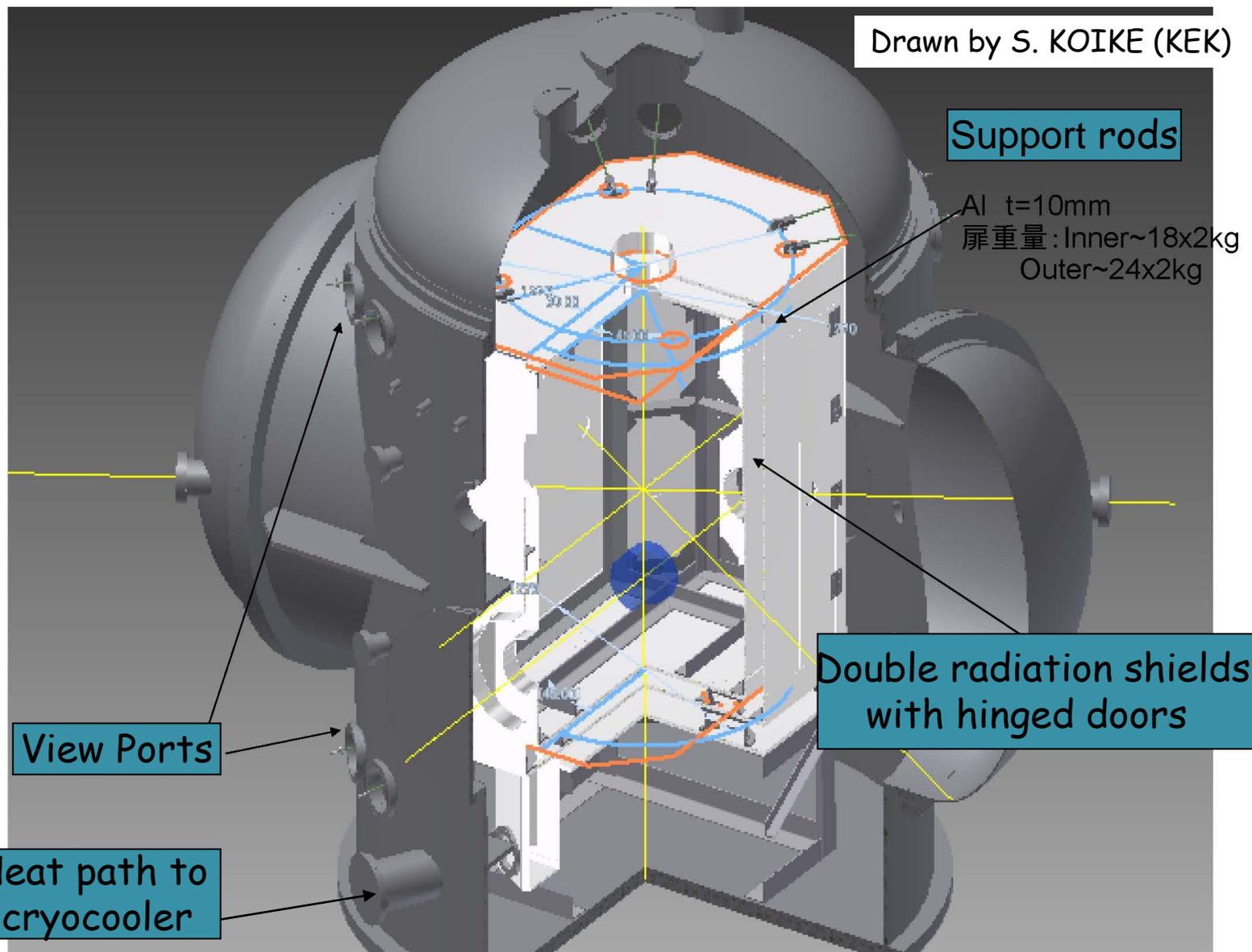
Components of Mirror Cryostat

Drawn by S. KOIKE (KEK)



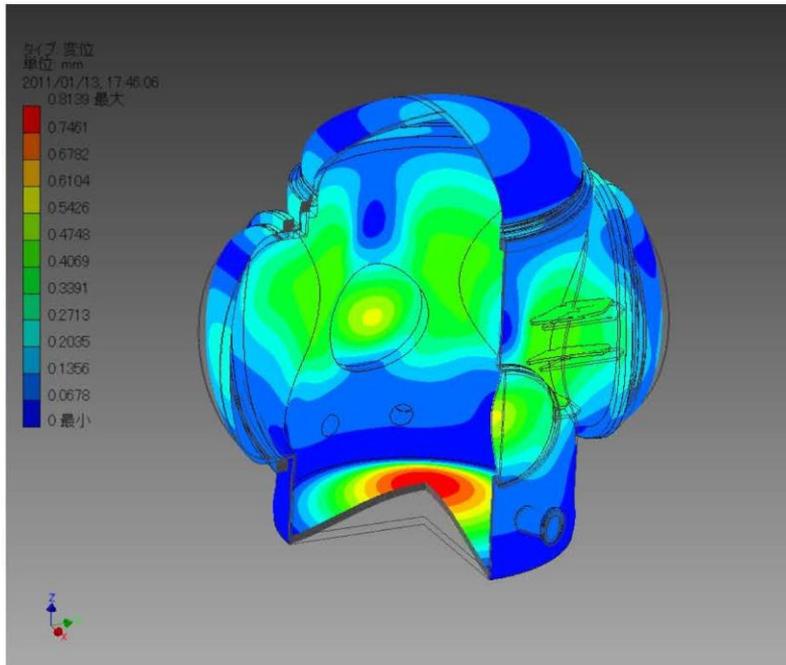
Cryostat accompany with the four cryocooler units

The interior of the cryostat

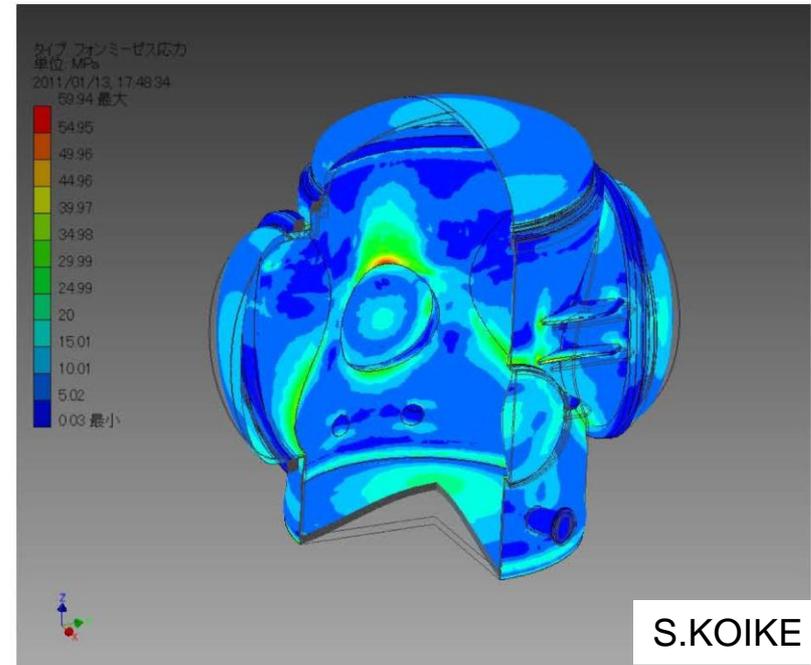


Example of static deformation analysis

Deformation under the atmospheric pressure and the gravity



Maximum deformation : 0.8 [mm]



Maximum stress : 59 [Mpa]

S.KOIKE

- Main vacuum duct and the duct to SAS are not connected.
- periphery of the bottom are fixed on the floor

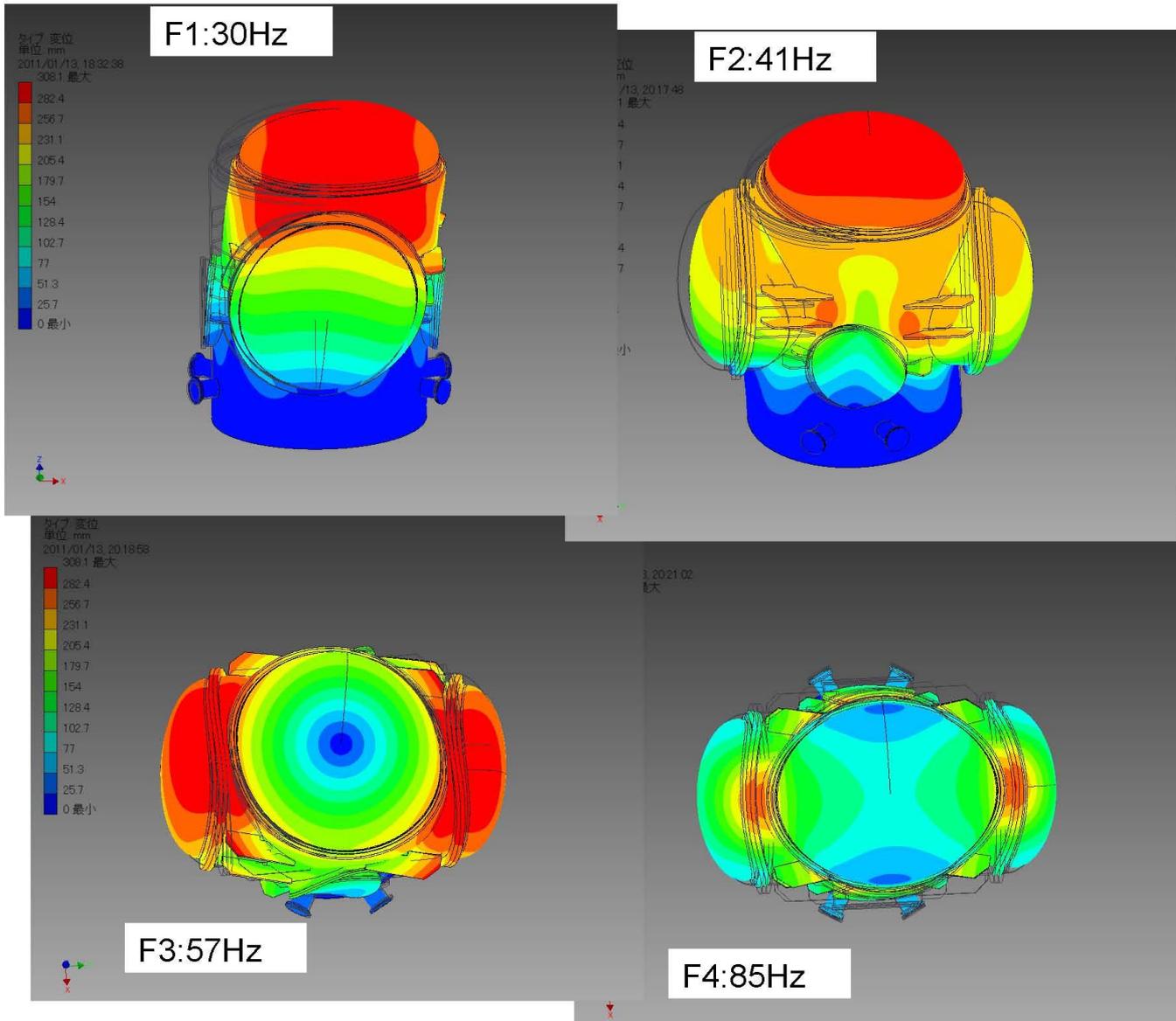
* Interface to SAS is not fixed at the moment.

Modal analysis

S. Koike

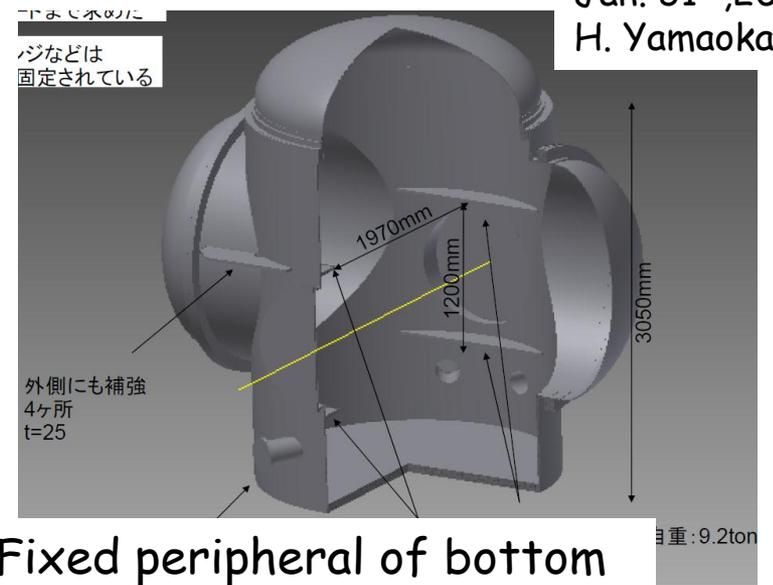
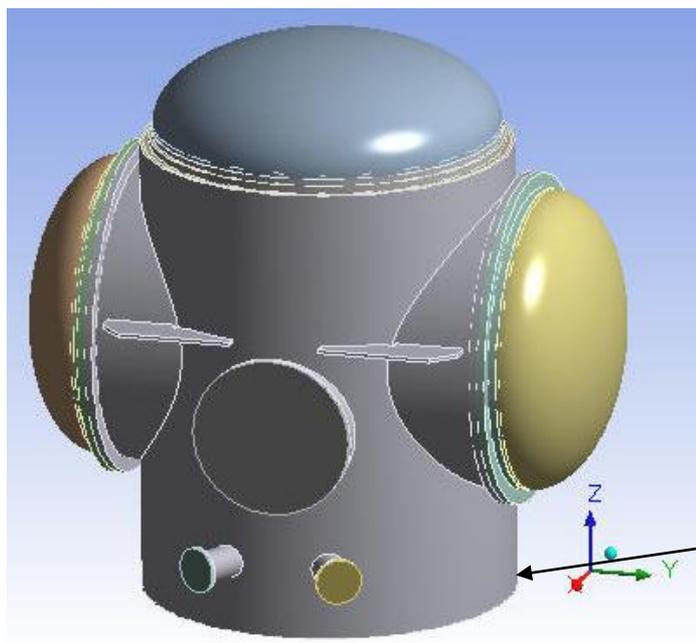
Resonance Frequency

- F1 29.86 Hz
- F2 41.27 Hz
- F3 57.22 Hz
- F4 85.01 Hz
- F5 89.68 Hz
- F6 93.33 Hz
- F7 111.81 Hz
- F8 120.70 Hz

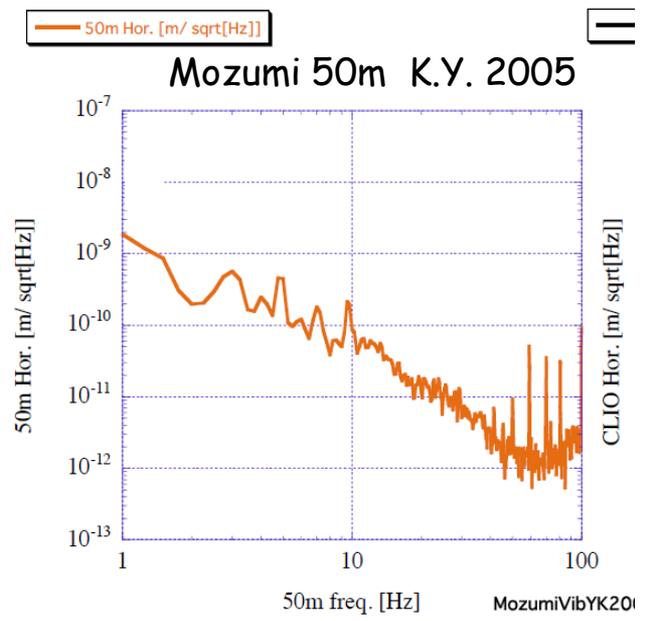


KAGRA Response to ground motion

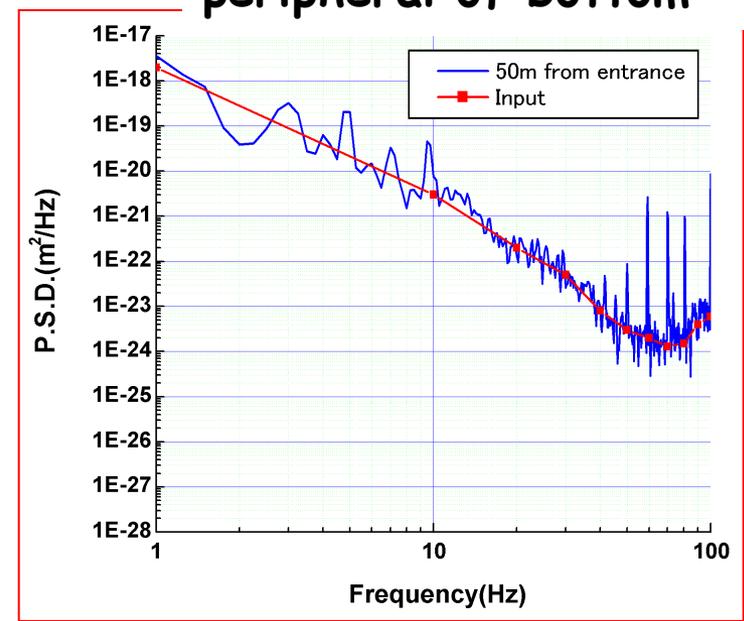
Jan. 31st, 2011
H. Yamaoka



Fixed peripheral of bottom on the ground

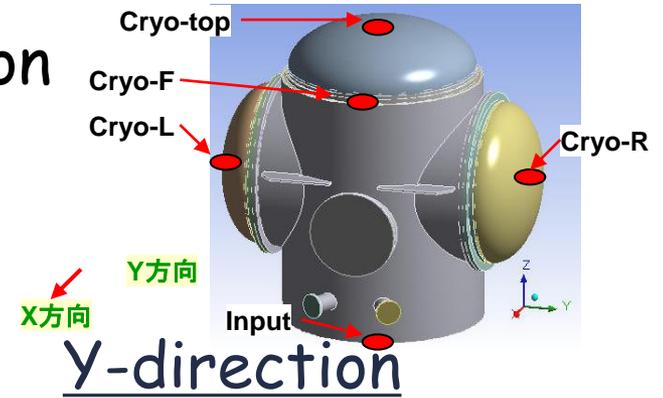


Input ground motion to peripheral of bottom

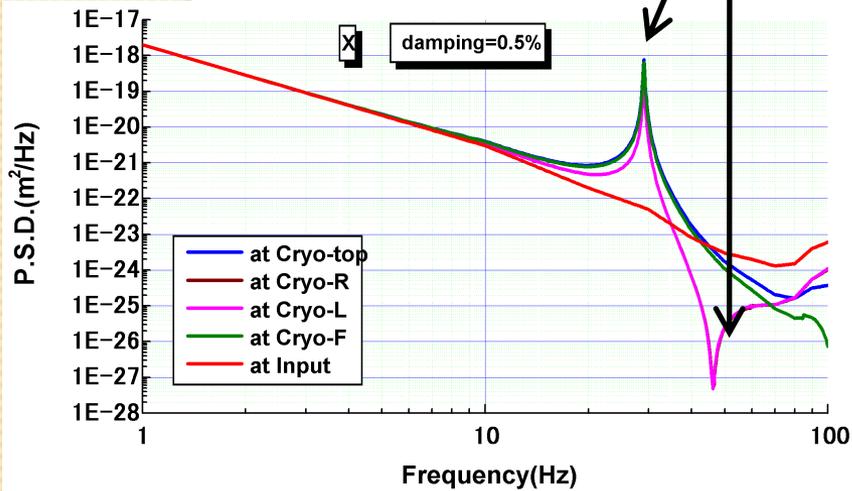


Analyzing of Response to ground motion

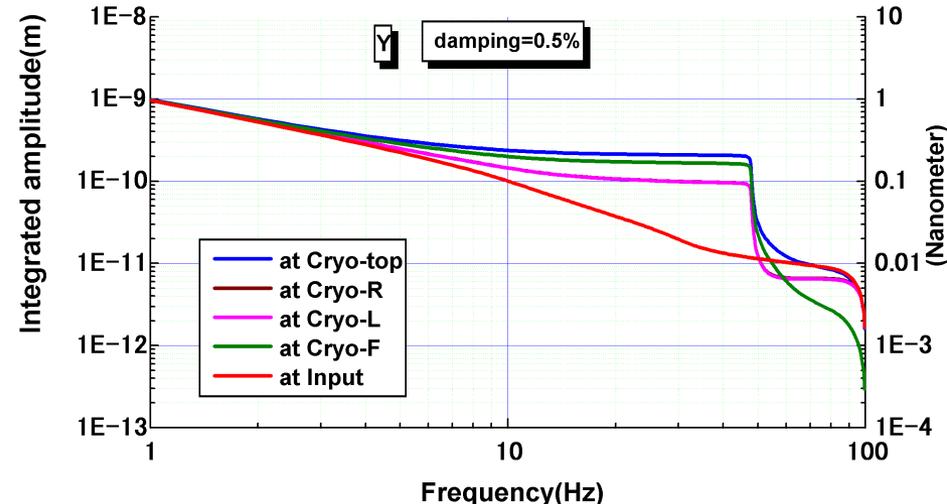
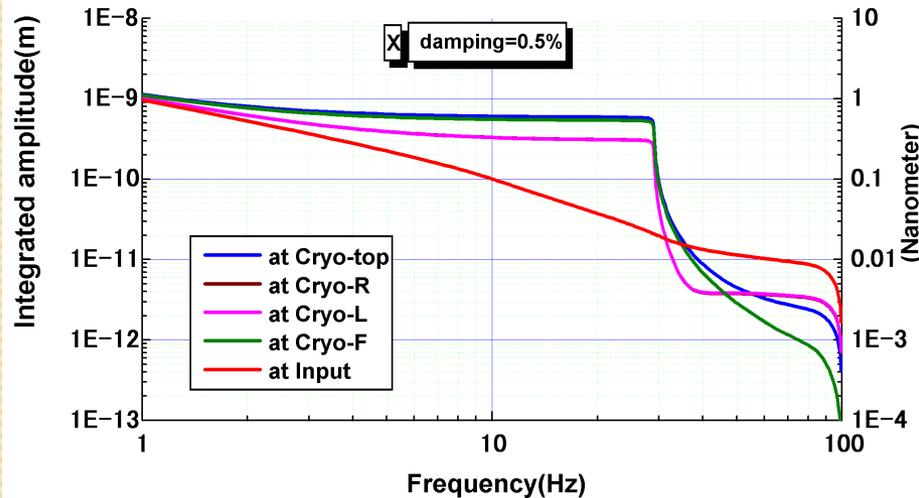
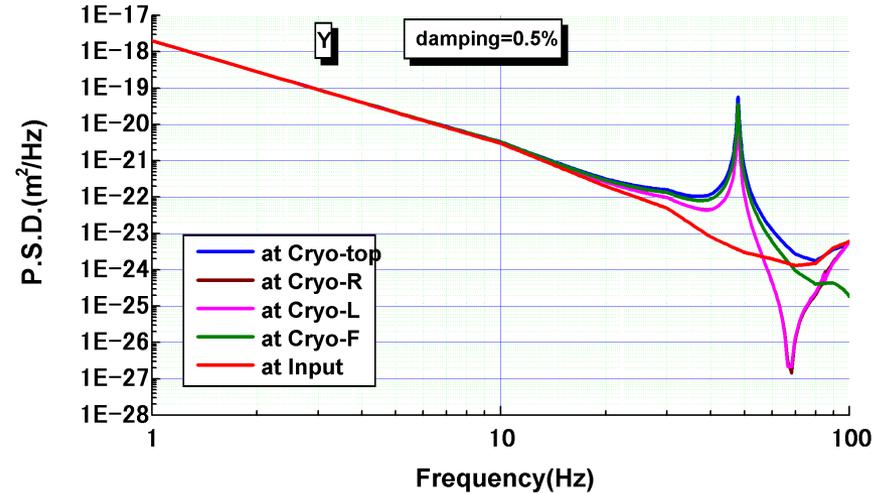
resonant frequency



X-direction



Y-direction



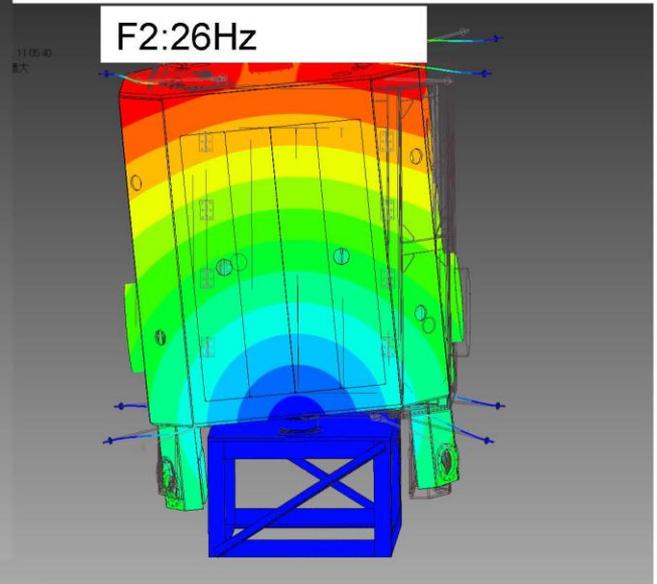
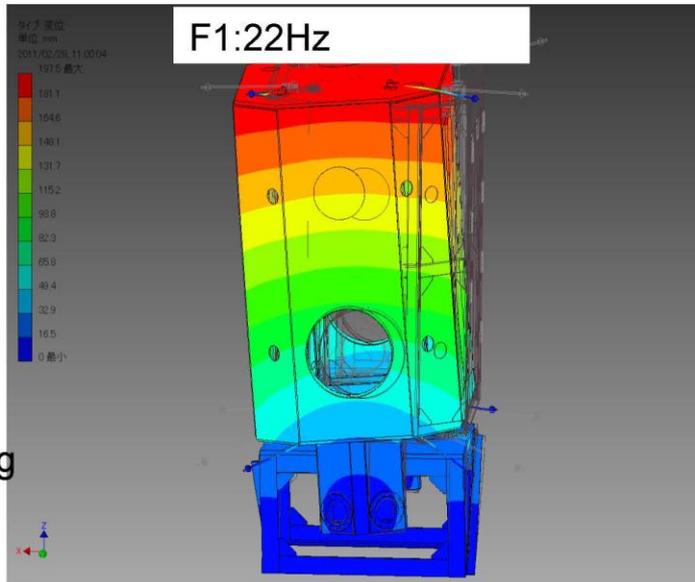
Modal analysis of outer shield

S.KOIKE

Mode frequency

- F1 22.31 Hz
- F2 25.98 Hz
- F3 39.47 Hz
- F4 41.79 Hz
- F5 46.22 Hz
- F6 57.38 Hz
- F7 59.04 Hz
- F8 76.29 Hz

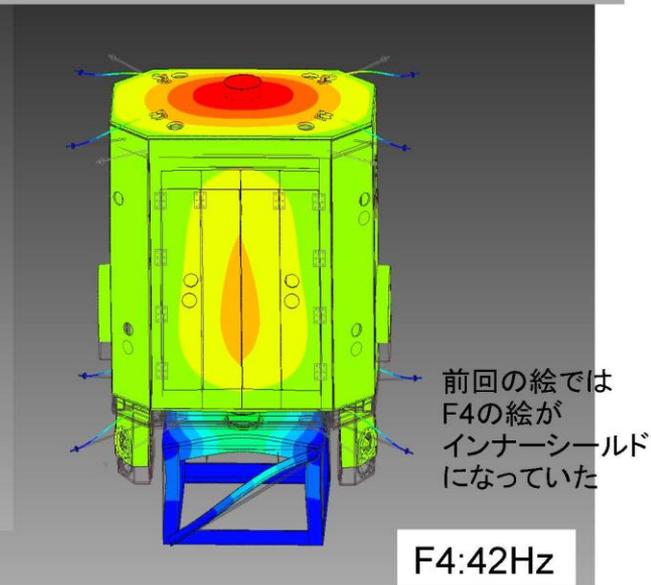
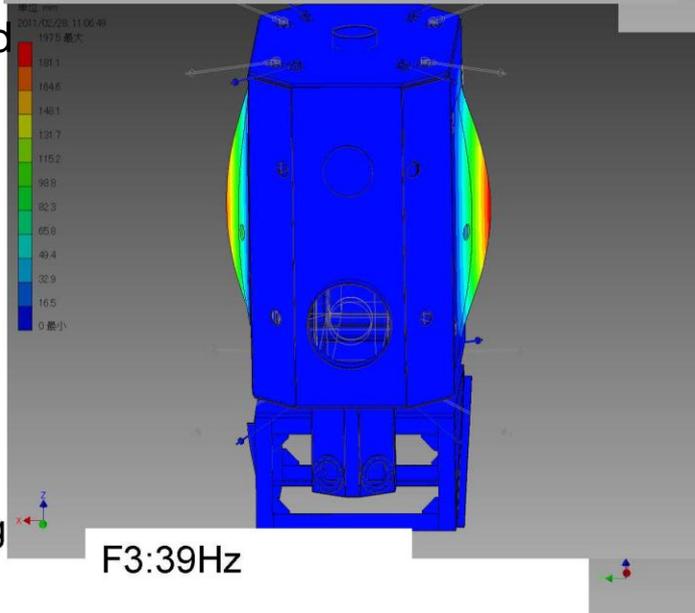
Mass=893.429 kg



Remove support rod Mode Frequency

- F1 7.86 Hz
- F2 16.80 Hz
- F3 39.18 Hz
- F4 41.78 Hz
- F5 43.01 Hz
- F6 44.96 Hz
- F7 57.11 Hz
- F8 58.41 Hz

Mass=889.352 kg



The Newest Estimated Heat load of the cryostat

1st Cold stage

| | |
|-------------------------|--------------------|
| • Outer Shield | (W) |
| ◦ Duct Shields | 8.2 |
| ◦ Eleven View Ports | 7.8 |
| ◦ Radiation From 300 K | 40.7 |
| ◦ Support post and Rods | 4.8 |
| ◦ Electrical wires | 3×10^{-4} |
| ◦ Cryo-cooler units | 15×4 |

| | |
|-------|-----------------|
| Total | <u>61.5 (W)</u> |
| /unit | <u>30.3 (W)</u> |

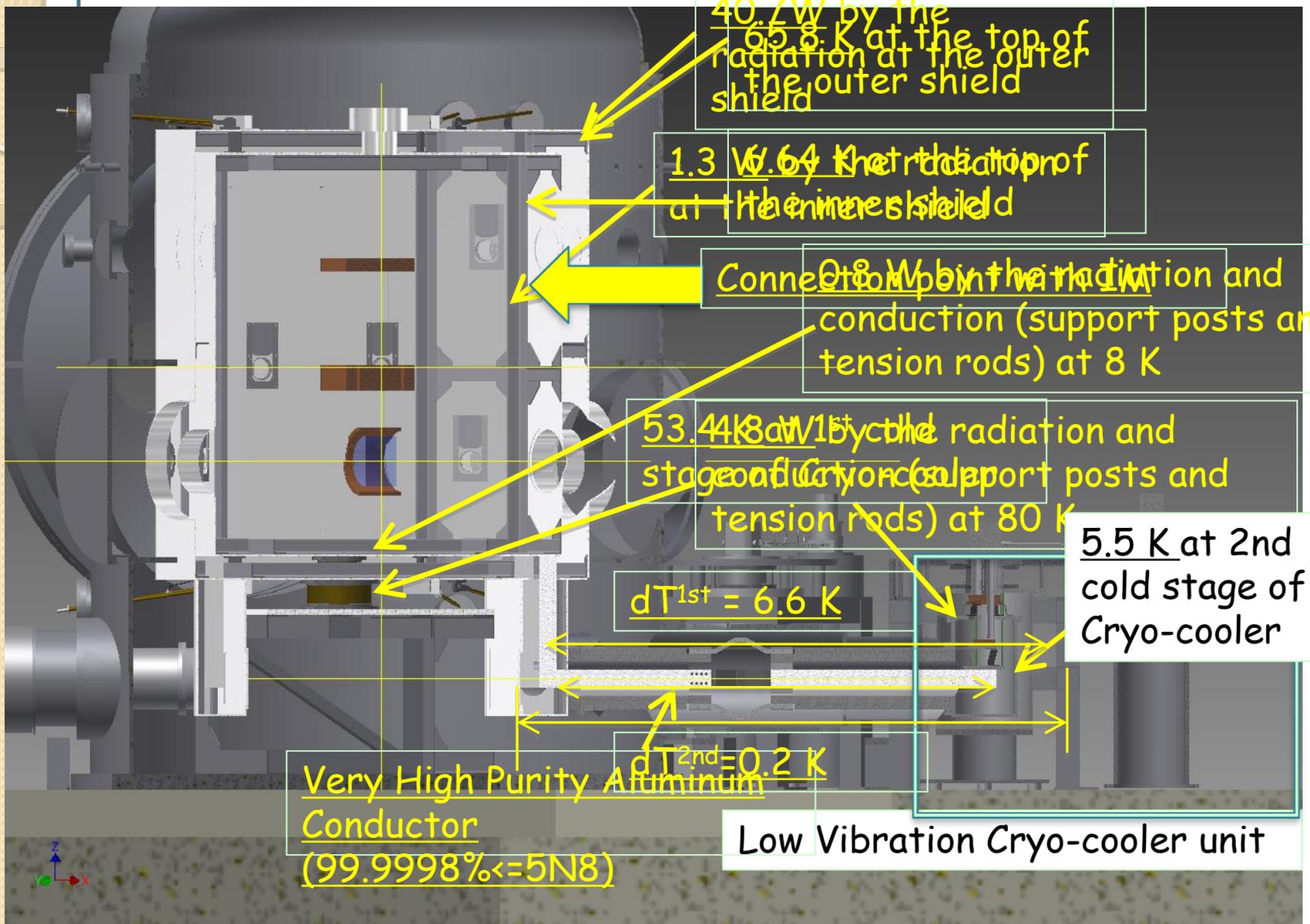
2nd stages of two cryo-cooler units will be connected with the inner shield.

Left 2nd stages of two cryo-cooler units will be connected with the mirror via cryogenic suspensions.

2nd Cold stage

| | |
|-------------------------|-------------------------|
| • Inner Shield | (W) |
| ◦ Radiation From 80 K | 1.3 |
| ◦ Support post and Rods | 0.8 |
| ◦ Electrical wires | 3×10^{-4} |
| ◦ Scattering Light | 8 |
| | (400kW \times 20 ppm) |
| ◦ Cryo-cooler units | 0.5×2 |
| Total at Inner Shield | <u>11.1</u> |
| W/unit | <u>5.6</u> |
| • Mirror | (W) |
| ◦ <u>Duct Shields</u> | ~ 0.02 |
| | (Beam and SAS) |
| ◦ Eleven View Ports | 0.8 |
| ◦ Mirror Deposition? | 0.9 |
| ◦ Cryo-cooler units | 0.5×2 |
| Total at the mirror | <u>2.7</u> |
| W/unit | <u>1.3</u> |

Estimated Thermal Budget



40.7W by the radiation at the outer shield
65.8 K at the top of the outer shield

1.3 W by the radiation at the inner shield
6.64 K at the top of the inner shield

0.8 W by the radiation and conduction (support posts and tension rods) at 8 K

53.44 W by the radiation and stage conduction (support posts and tension rods) at 80 K

5.5 K at 2nd cold stage of Cryo-cooler

$dT^{1st} = 6.6 K$

$dT^{2nd} = 0.2 K$

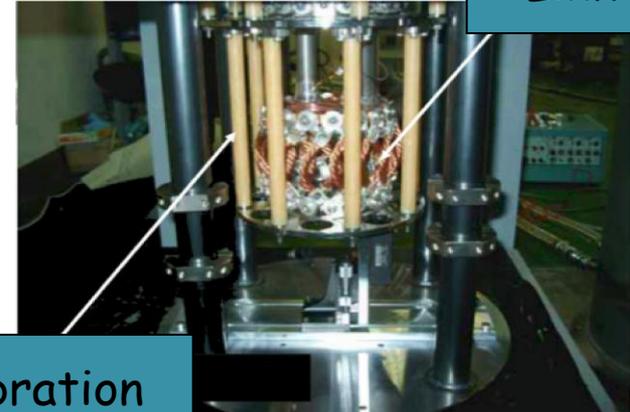
Very High Purity Aluminum Conductor (99.9998% $\leq 5N8$)

Low Vibration Cryo-cooler unit

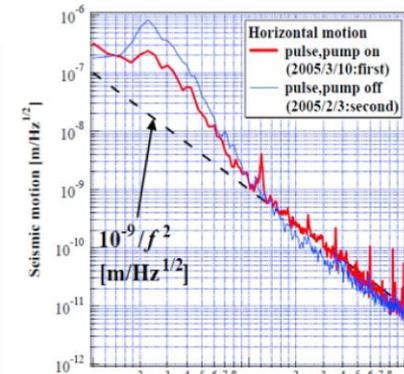
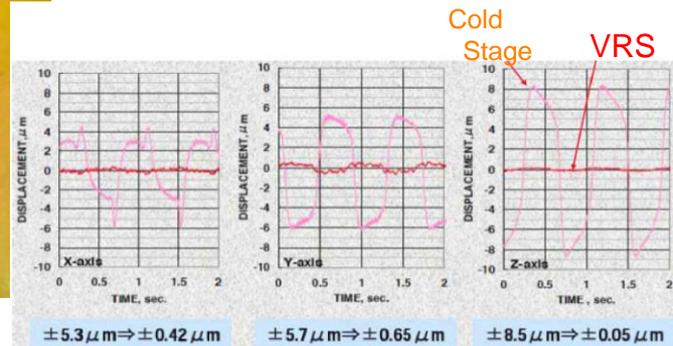


KAGRA Cooling Option: Conductive cooling by cryo-coolers with low vibration stage

Our decision: Use CLIO type Cryo-cooler with low vibration mount for KAGRA



Vibration Reduction Stage



CLIO is prototype for KAGRA constructed at Kamioka mine.

Achieved very vibration level < few nm!

Advantage and Disadvantage of CLIO type cryocooler unit

Discontinued Items

- Ready to use Cryo-Cooler equipped special cold stage, such as CLIO type
- Aluminum FRP tube as anti-vibration support rods
- High pure aluminum thin wire less than $\phi 0.12$ mm for heat link.

Substitutes for the Items

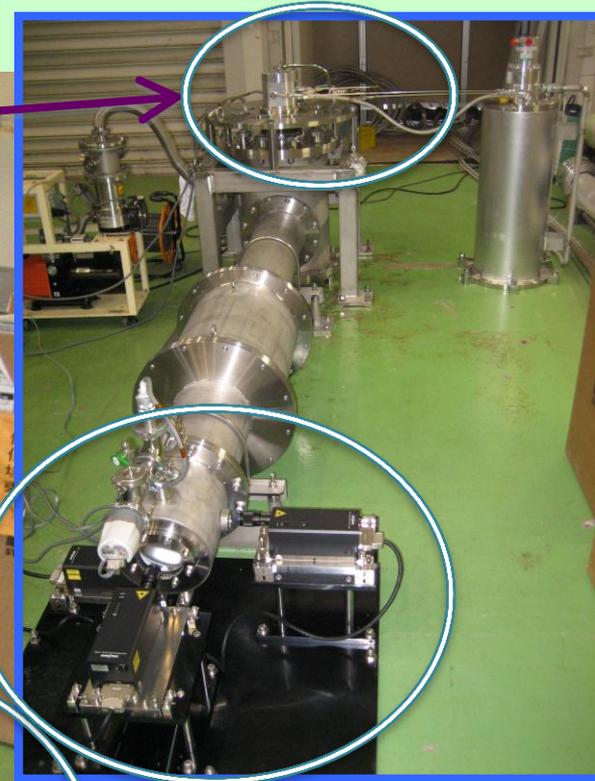
- Attach new design of cold stage flanges to mass-produced 1W/4K PTC
- Replace to Carbon FRP tube as anti-vibration support rods (stiffness $A_{FRP} > CFRP > GFRP$)
- Start R&D work with new company for development of high pure aluminum thin wire less than $\phi 0.12$ mm.

Proto-type cryocooler unit under the performance test

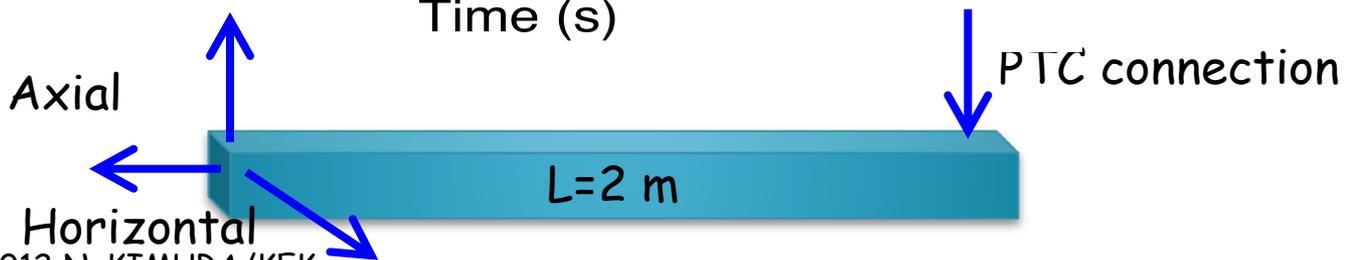
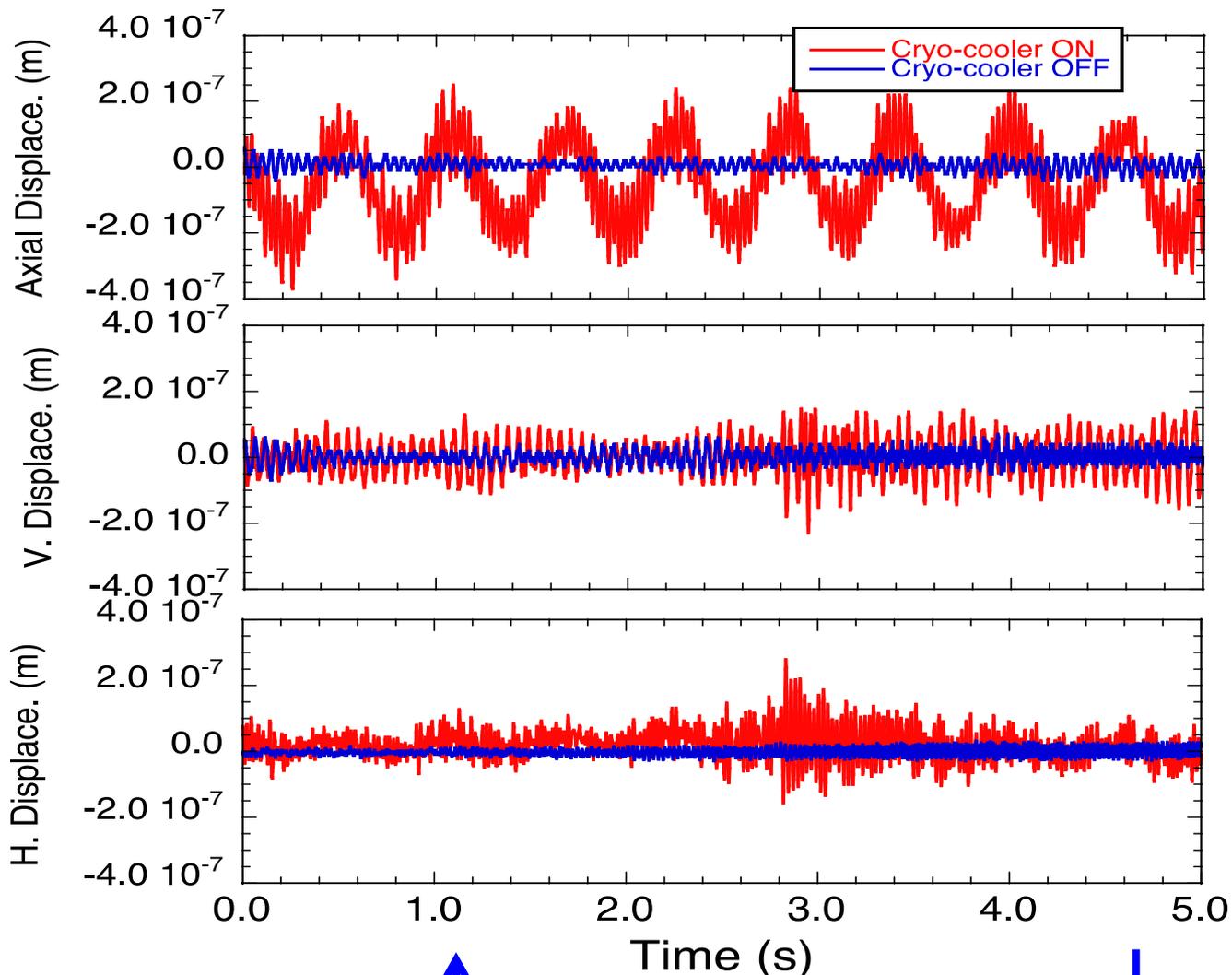
Pulse tube type cryo-cooler with anti-vibration stage

Vacuum duct for very high pure aluminum thermal conductor and radiation shield

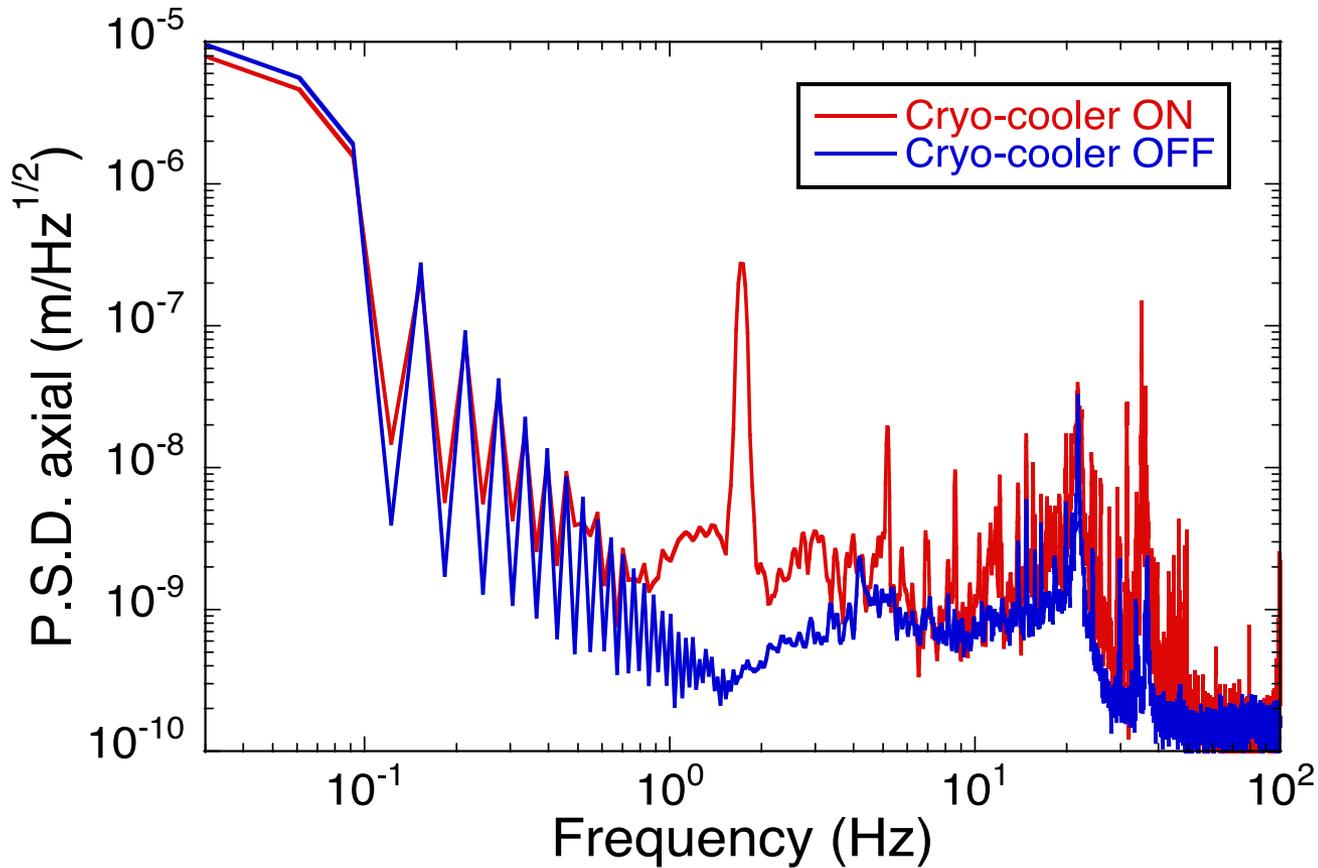
Tri-axial laser displacement meter



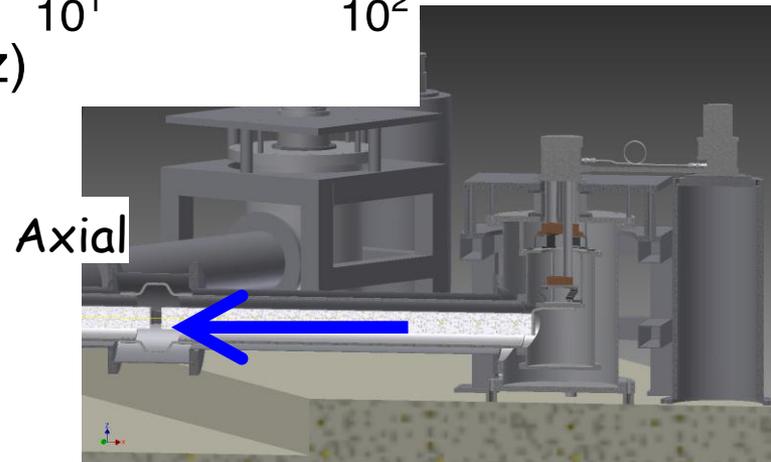
Vibration Level at edge of AL thermal conductor



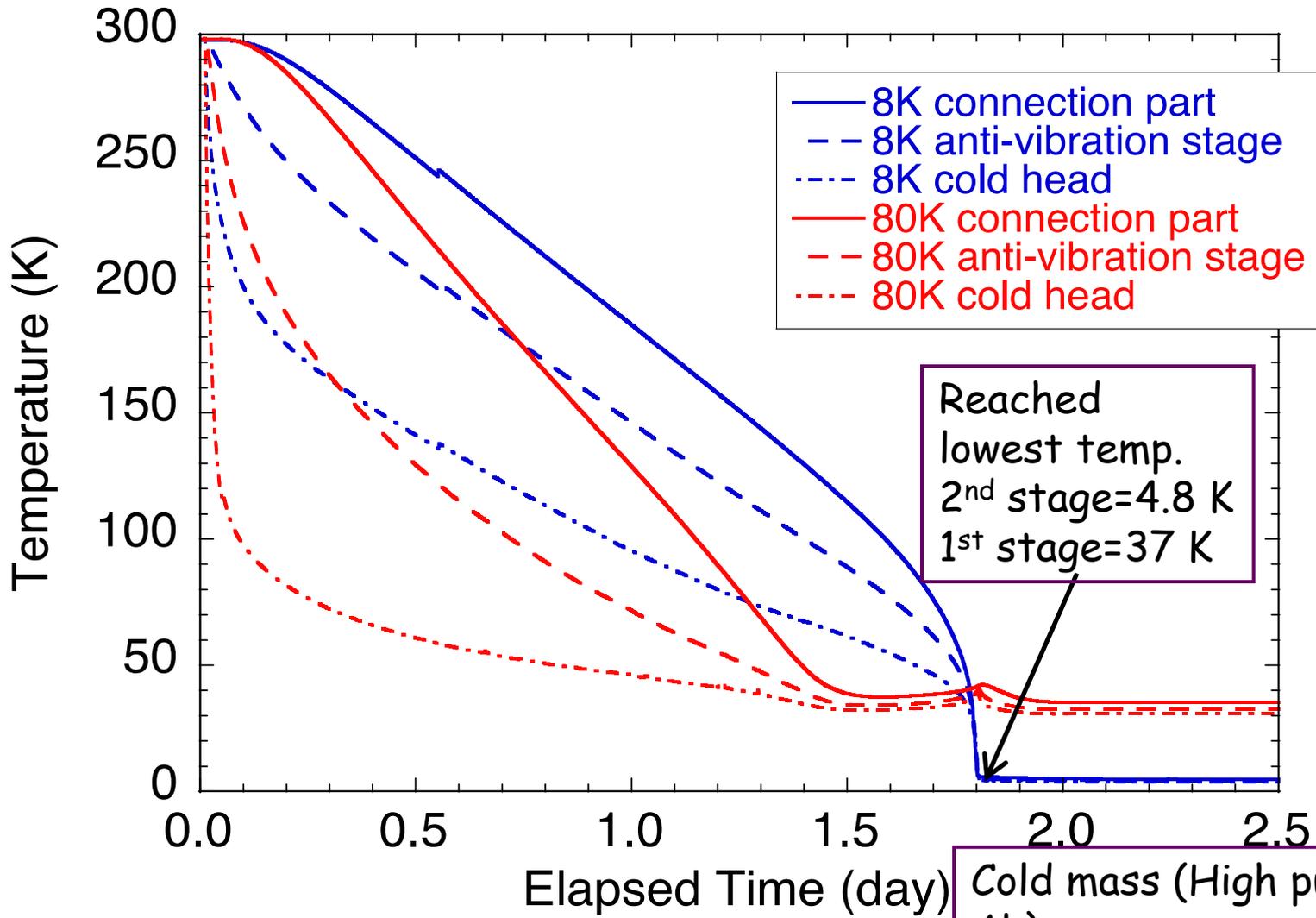
F.F.T. analysis (Ex. Axial direction)



Results of displacement at connection point
 Axial < 200 nm
 Vertical < 50 nm
 Horizontal < 10 nm

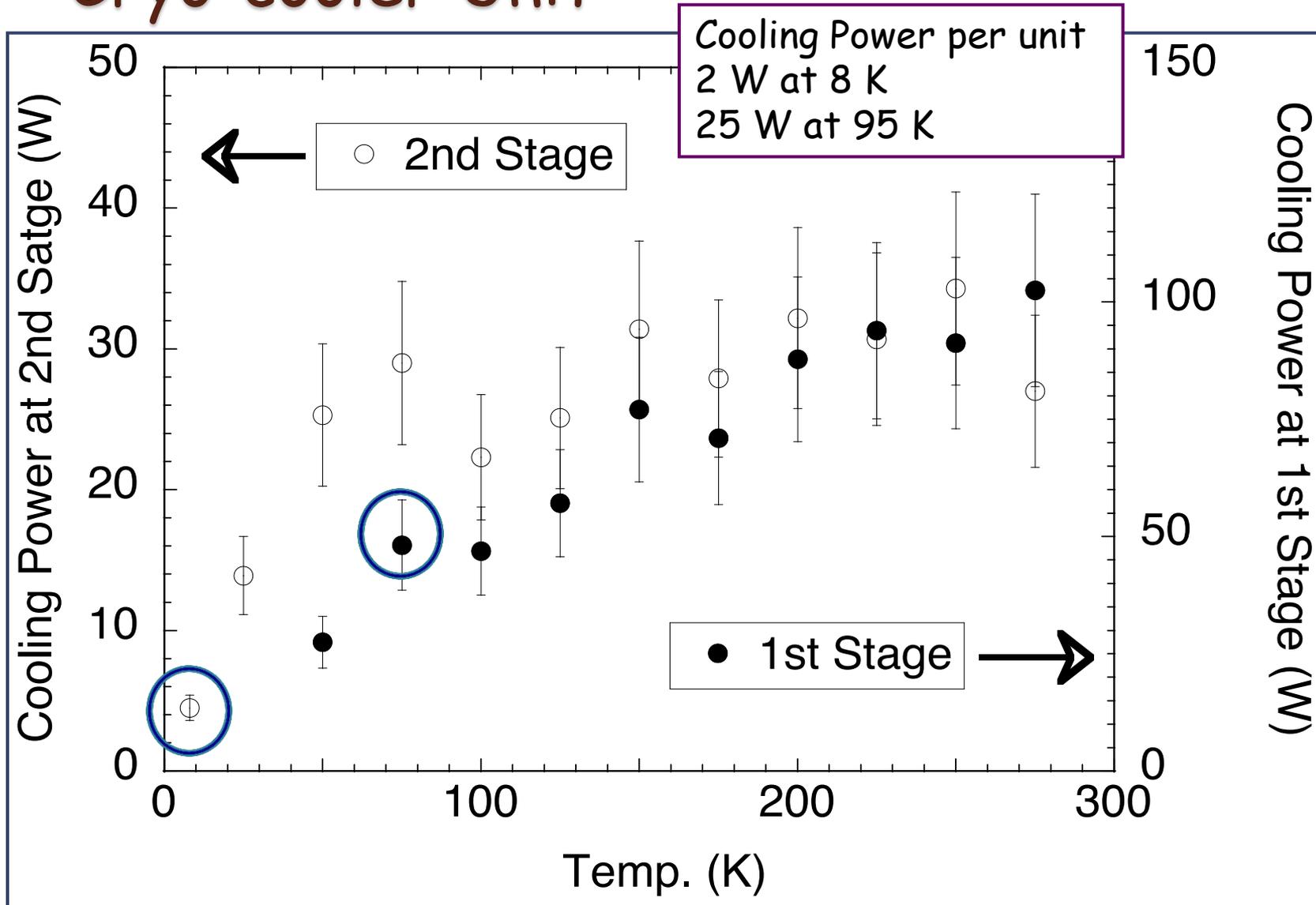


Cooling curve of proto-type cryo-cooler unit

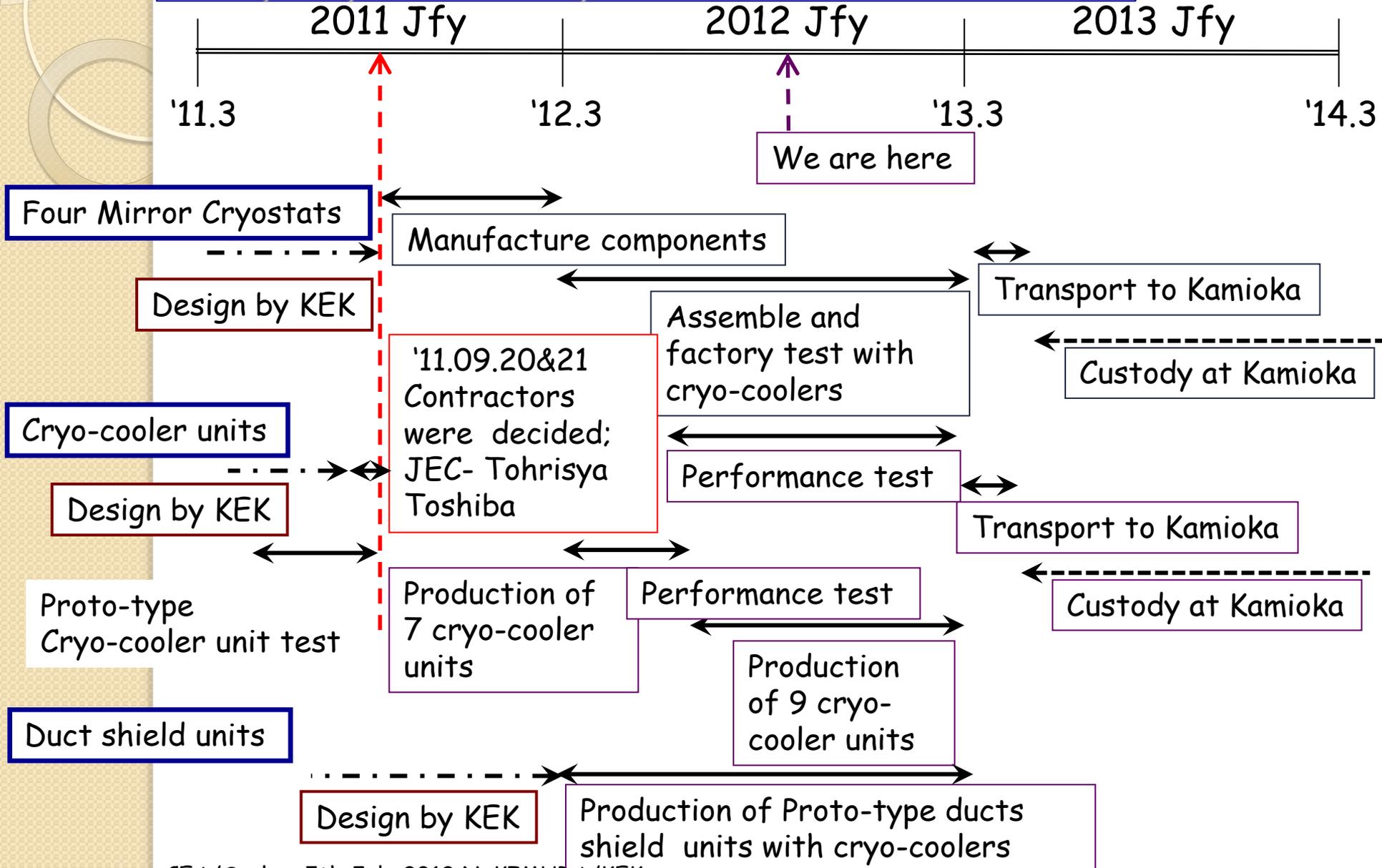


Cold mass (High pure AL)
2nd stage= 25 kg

Cooling Performance of Proto-type Cryo-cooler Unit



Production plan of KAGRA mirror cryostats and peripheral components



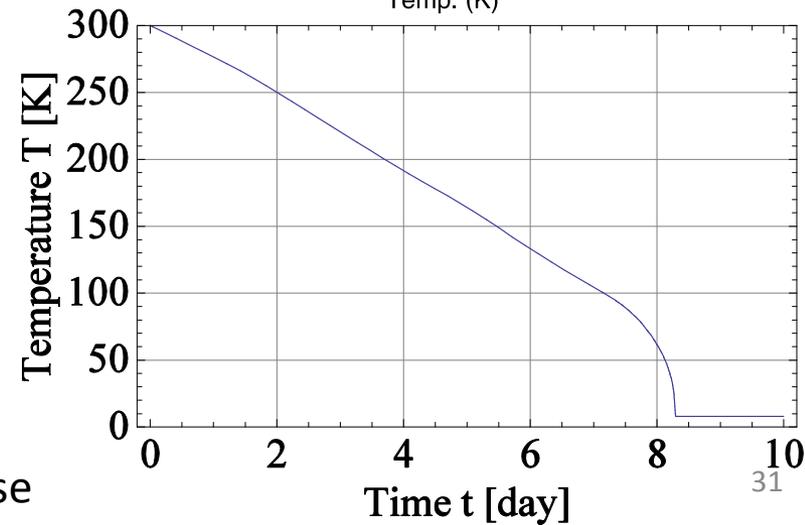
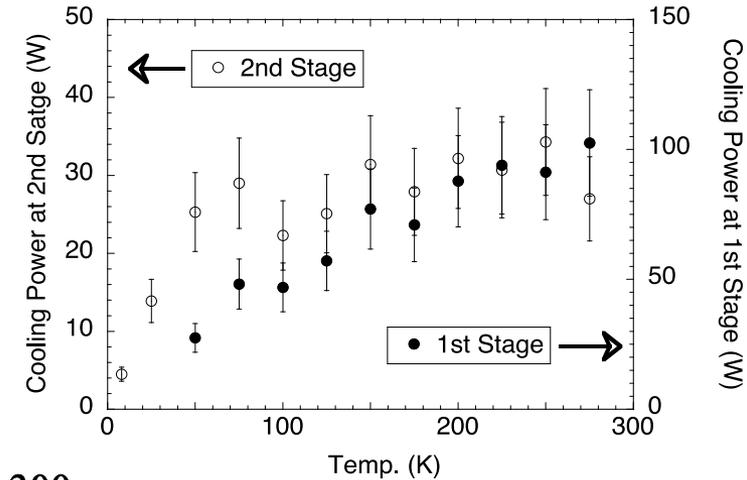
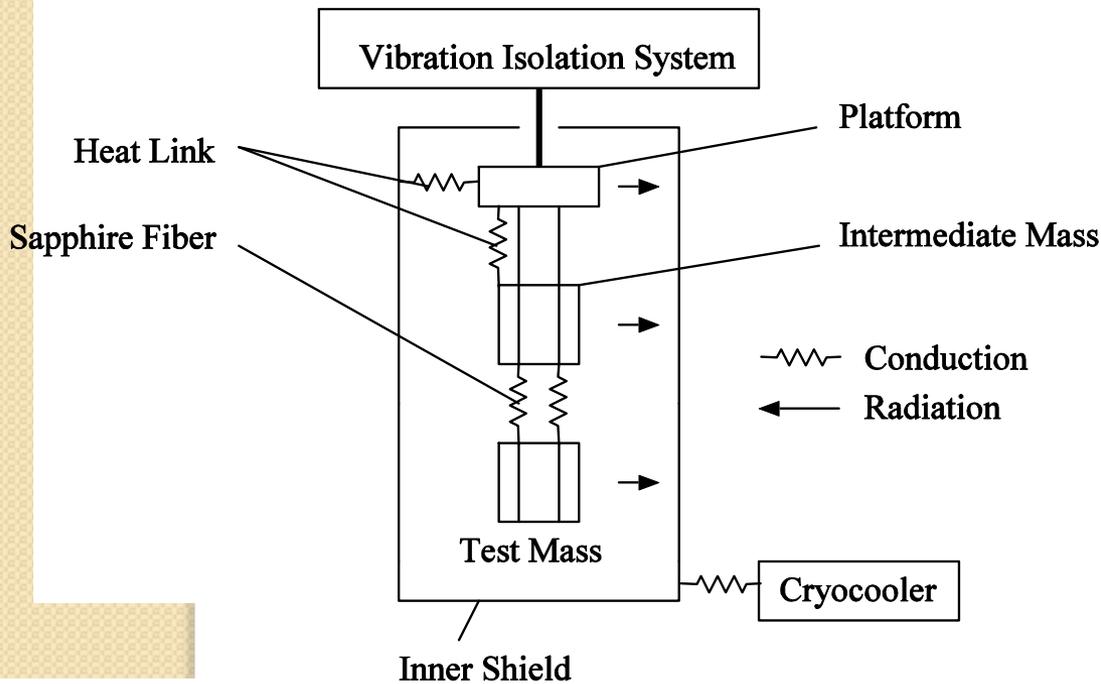
- The design of the cryostat and cryo-cooler for KAGRA were finished.
- The production of the components for the cryostat have started in this September 2011.
- The performance of the cryo-cooler unit with anti-vibration stage have almost confirmed, but need some modification to clear the specification.
- Performance of the first cryostat will be demonstrated on the mid of 2012 Jfy.
- Total performance of the first cryo-cooler will be confirmed on the mid of this August.

Back UP

KAGRA Estimation cooling characteristics

Y.SAKAKIBARA

- Model is constructed to estimate initial cooling time
- Heat is transferred by conduction in sapphire fibers and heat links and radiation
- Inner shield of 410 kg is connected to the 2nd stages of 4 cryocoolers
 - Cooling power is derived from test result of proto-type cryo-cooler



Inner Shield
(Al)
 T_{sh}, M_{sh}

$$\frac{dT_{sh}}{dt} = - \frac{4Q_{cryo}(T_{sh})}{M_{sh} C_{Al}(T_{sh})}$$

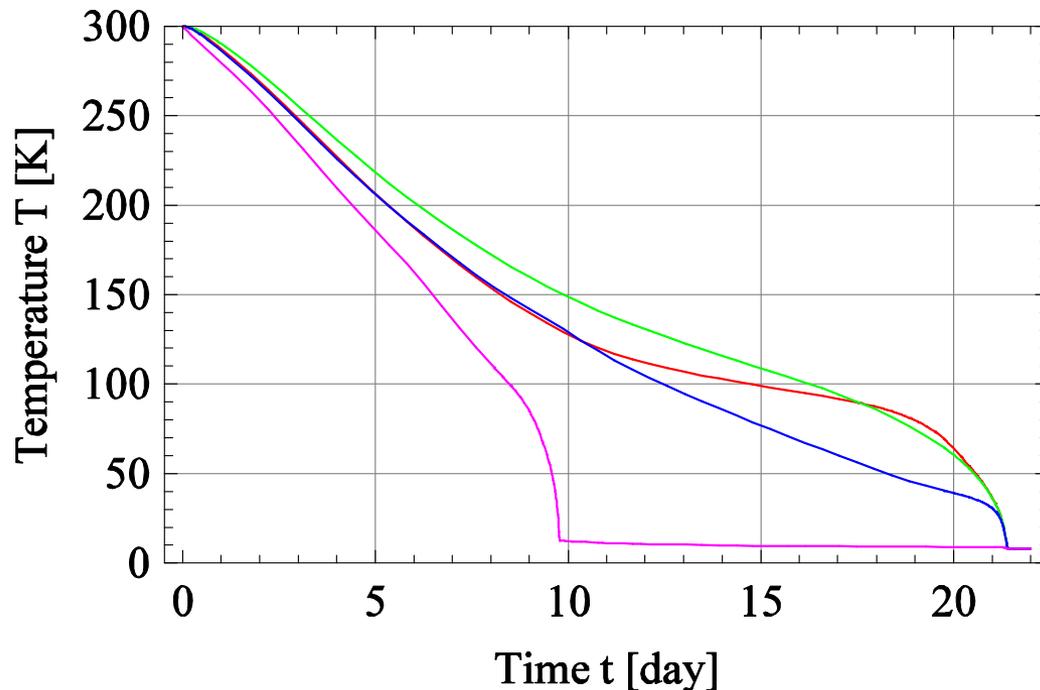
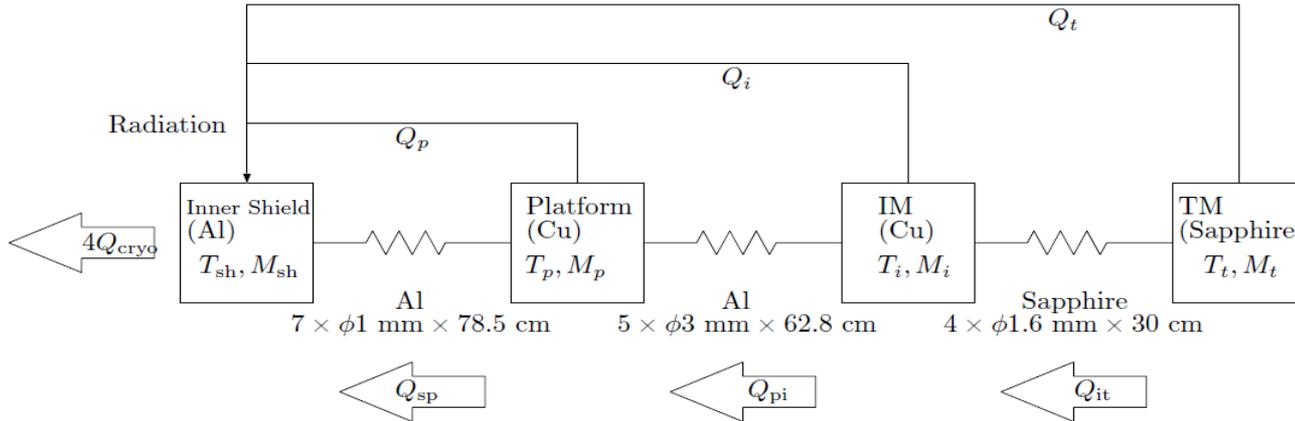
Temperature T [K]

Time t [day]

Suspension from isolation system is excluded in this case

Effect on Diamond Like Carbon coating

Y.SAKAKIBARA



- Increased radiation by platform, intermediate mass, and inside of inner shield coated with DLC (Diamond Like Carbon)
- Absorptivity of DLC at 10 μm is 0.41 (cf. emissivity of Cu and Al is 0.03)
 - We assume that it equals emissivity

| | |
|---|--------------|
| — | TM |
| — | IM |
| — | Platform |
| — | Inner Shield |

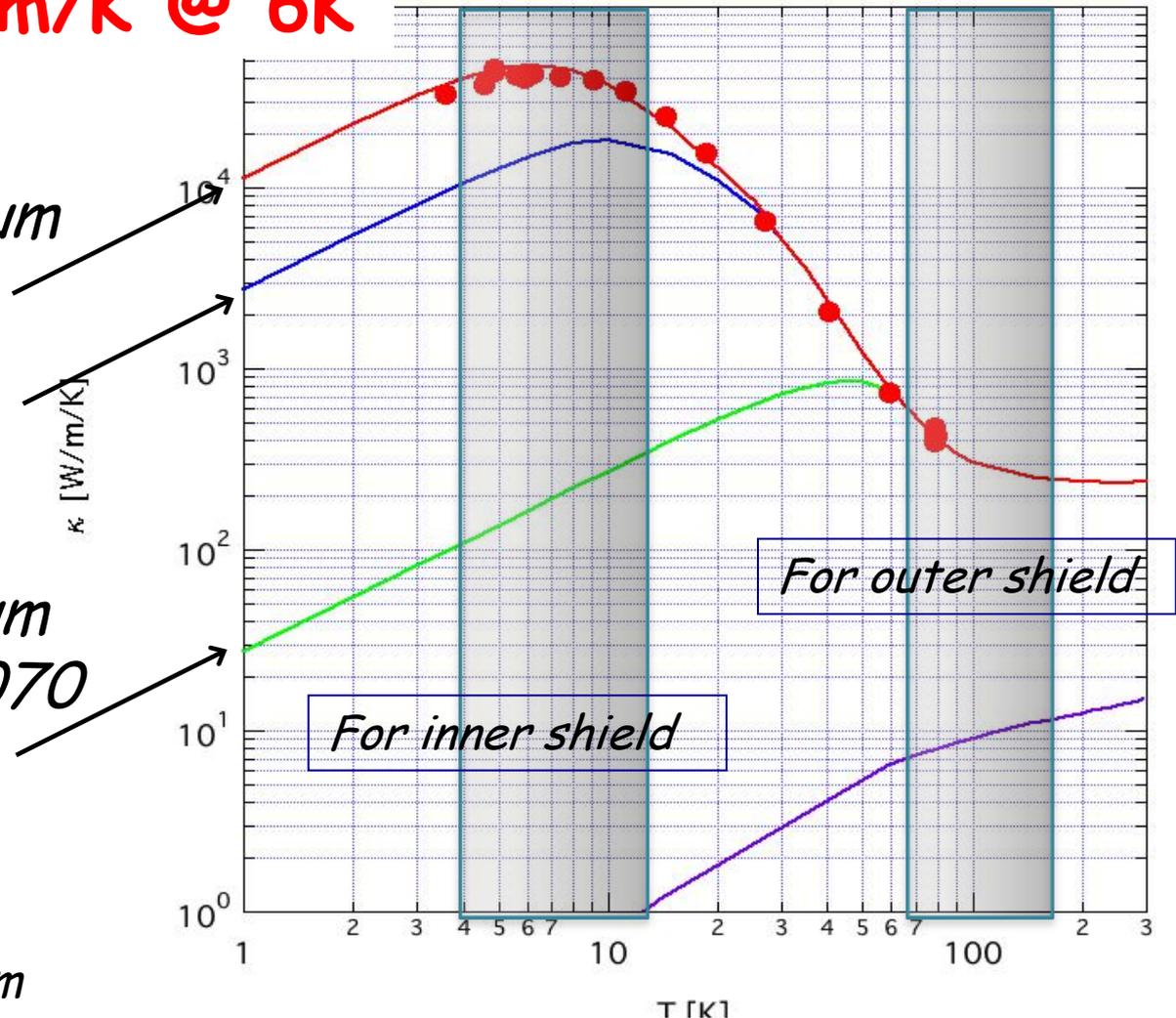
Example of Thermal Conductivity of 6N-class Very High Pure Aluminum*

40,000 W/m/K @ 6K

6N Aluminum

5N up Al
RRR=3000

2N Aluminum
~Type A-1070



Cost:

5N8 > 2N Aluminum

We must put the right material in the right position.

