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# Cryogenics, a science for magnets

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# Outline

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- Superconducting magnet cooling
  - Heat transfer in superconducting magnet
  - Magnet types and Cooling methods
- State of the art
  - Accelerator magnets
  - Detector magnets
  - Magnets for the other scientific communities
- Propositions
  - Design limits and future needs
  - Cryogenics R&D at Dapnia
  - Propositions of R&D actions

# Heat transfer in SC magnets (1/2)

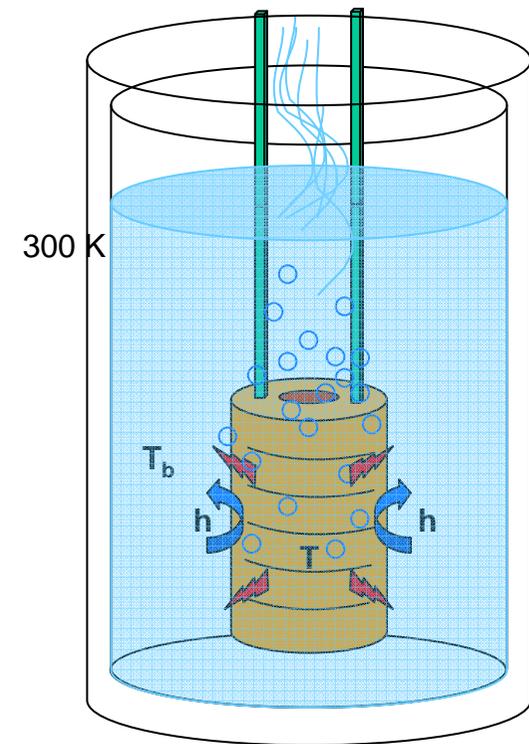
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- To insure stability ( $T_{\text{magnet}} < T_{\text{critical}}$ ) and protection ( $T_{\text{max}}$ ) of the magnet
  - Against permanent thermal losses ( $Q_p$ )
    - Thermal radiation (300 K to  $T_{\text{magnet}}$ )
    - Conduction through current leads, structural elements and support
    - Internal volume dissipation such as "Beam losses" and "AC losses"
  - Against transient perturbations ( $Q_t$ )
    - Local Super/Normal transition
    - Magnet Quench
  - With cooling power ( $Q_R$ )
    - $Q_R = h \cdot (T - T_b) \cdot p / A$  with cryogenic fluids
    - $Q_R = \text{Cryocooler power}$
  - Thermodynamic properties of magnet components
    - Heat capacity  $C$ , Thermal conductivity  $k$  ⓘ
  - Cooling power ( $Q_R$ )
    - Thermodynamic properties of cryogen
    - Cryocooler performance

$$C \frac{\partial T}{\partial t} = \nabla \cdot (k \vec{\nabla} T) + Q_p + Q_t - Q_R$$



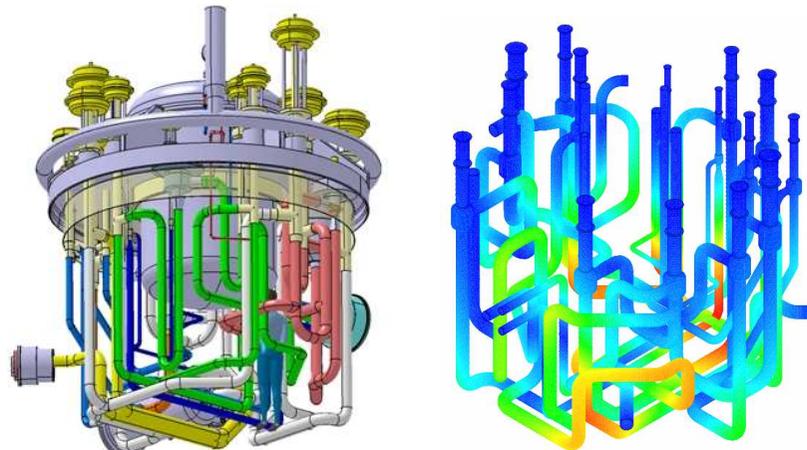
# Heat transfer in SC magnets (2/2)

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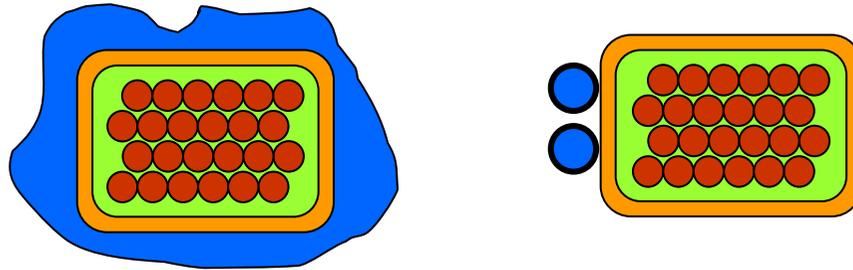
- In operation with fixed  $H(T)$  and  $J(A/m^2)$ 
  - Superconductor used impose  $T_b$ ,  $C$  et  $k$
  - Thermal losses :  $Q_p$  et  $Q_t$  (W)
  - Design impose geometry :  $A$  ( $m^2$ ), wetted perimeter,  $p$  (m)
  - **Only one free parameter for cryogenics engineer** :  $h$  pour  $T < T_c$
- $h$ , surface heat transfer coefficient depend on
  - Cryogen, Cooling methods (flow, static, boiling), magnet geometry (confinement), material components of the magnet
- Cryogenics for magnet design is also
  - Vacuum technology, Fluids Cryo-distribution and cryoplant
  - **Team work** with magnet designers, mechanical engineer, vacuum engineer...



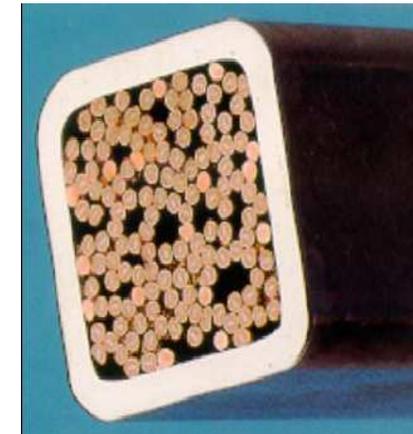
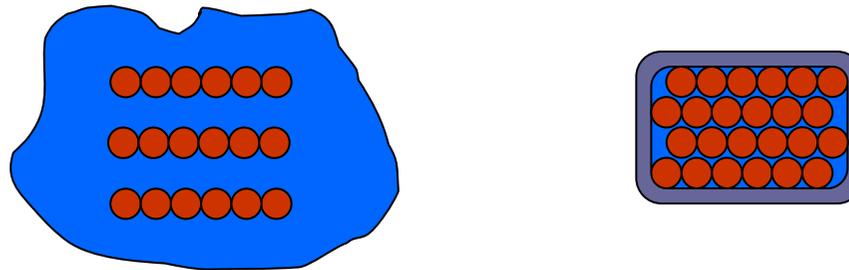
Maximum horizontal displacements  
(red parts): 5.7 mm  
SIS for ITER

# Magnet Types / Cooling method

- "Dry magnet" : No contact between the cryogen and the conductor
  - Conduction in the magnet : bath or Cryocooler
  - External flow of cryogen to the coil (CMS, ATLAS, ...)



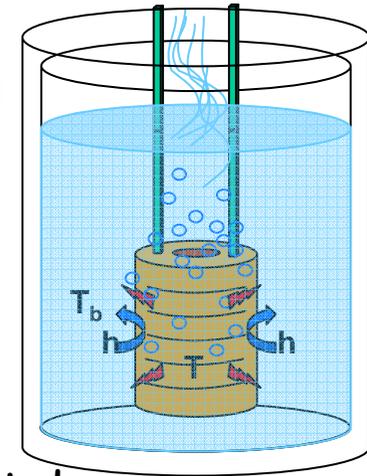
- "Wet magnet" : Contact between the cryogen and the conductor
  - Bath : single phase stagnant He II (Tore Supra, ISEULT, LHC, 45 T NHMFL,...)
  - Flow : single phase in CICC (W7X, ITER, ...)



- "Cryostable" or "adiabatic" magnets
  - "Cryostable"  $Q_R > Q_p + Q_t$  (Iseult, Tore Supra, ...)
  - "Adiabatic" (CMS, ...)

# Cooling method : The Baths

- Saturated bath (P=1 Atm et T<sub>sat</sub>)
  - Implementation
    - **Simple design and operation** for cryogenics
    - Latent heat cooling (phase change); (He 4.2 K, N<sub>2</sub> 77.3 K et H<sub>2</sub> 20.4 K)
    - Non uniform cooling due to **vapor formation**, dry out
  - Heat transfer in nucleate boiling :  $q_{\max} \approx 10^4 \text{ W/m}^2$  for  $\Delta T \approx 1 \text{ K}$  ⓘ
  - Large scale magnet or compact system (He  $\sim 1 \text{ W/m}$ )
  
- Pressurized He II (1.9 K at P=1 Atm)
  - Implementation
    - Design and operation of cryogenics **costly and more complicated**
    - Heat exchanger He II sat / He II p
    - Design for the heat paths between cable and the HX
  - Large Heat transfer :  $k \approx 10^5 \text{ W/m.K}$  for  $\Delta T \approx 0.3 \text{ K}$  and  $\mu \approx 3 \cdot 10^{-6} \text{ Pa.s}$  ⓘ
    - Thermal (Kapitza) resistance between solid and He II
      - $R_k = 3 \cdot 10^{-4} \text{ K.m}^2/\text{W}$  for Cu and  $R_k = 10^{-3} \text{ K.m}^2/\text{W}$  for Kapton
  - LHC  $\sim 1 \text{ W/m}$ , Concept extendable to 50 W/m with proper heat path (channels and insulation)



# Cooling method : Convection flow

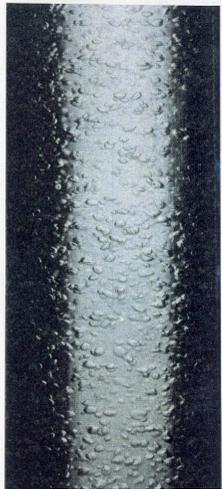
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- Single phase forced convection
  - Implementation
    - **Pressurization system** and **periodic recooling** for operation (series of large magnets)
    - **Simple design** with traditional heat transfer and pressure drop correlations
  - Heat transfer (sensible heat with temperature increase) ⓘ
    - Supercritical He ( $\sim 0.1$  kg/s and  $\sim 1-10$  W/m)  $P \approx 3-8$  bar,  $T \approx 4.4$  K,  $\Delta T \approx 50-150$  mK per magnet
    - He II ( $\sim 1$  W/m) Advection effect for 1m/s for  $\Delta T = 0.1$  K @ 1.8 K, Negative JT coefficient

- Two-phase forced or natural convection



P. Bredy, SACM

- Implementation
  - Same advantages and inconvenient than bath cooling but **lower quantity of cryogen**
  - Operation needs pressurization system in forced flow and none in natural convection
- Heat transfer due to nucleate boiling but degradation at high mass flow
  - Two-phase forced He flow  $q_{\max} \approx 10^4$  Wm<sup>-2</sup> for  $\varnothing 10$  mm  $m = 6$  gs<sup>-1</sup> and  $\Delta T \approx 1$  K ⓘ
  - Two-phase natural helium flow  $q_{\max} \approx 10^3$  Wm<sup>-2</sup> for  $\varnothing 10$  mm  $m = 20$  gs<sup>-1</sup> and  $\Delta T \approx 0.3$  K
- Forced convection : ATLAS (helium)
- Natural convection : CMS (helium), HTS Synchronous Machine (Nitrogen)

# Cooling method : Conduction

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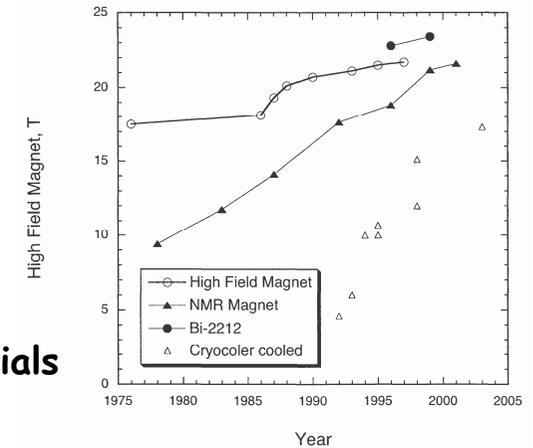
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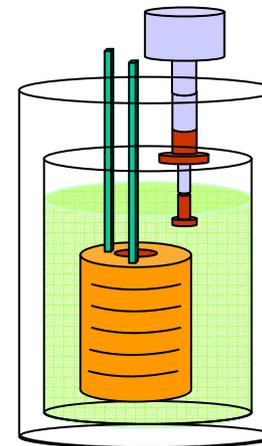
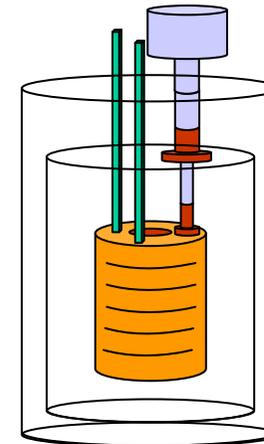
- Cryocooler
  - Implementation
    - Simple design and operation
    - Small LTS magnet or HTS magnet
    - Low thermal conductivity and diffusivity of materials
  - Performance
    - Commercial : 1.5 W at 4 K but fast improvements
    - R&D : 1 W at 1.8 K
  - Heat Transfer
    - Conduction through magnet or cryogen
  - Examples
    - 10T magnet class commercialized since 1990
    - 18T NbTi and Nb<sub>3</sub>Sn magnet (MIMS, Toshiba et TIT)
      - Cooled by CR de 1 W at 1.8 K
    - Magnet cooled with solid cryogen
      - HTS...



BB, Superconducting Magnet thematic day, CEA Dapnia, July 3<sup>rd</sup> 2006

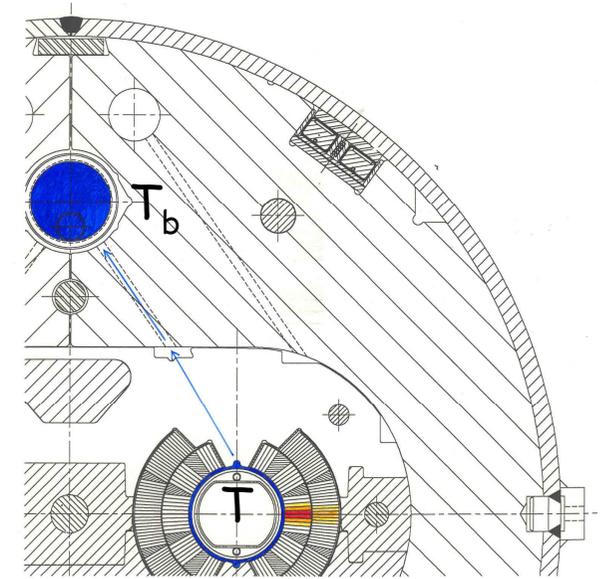


A. Sato, MiMS



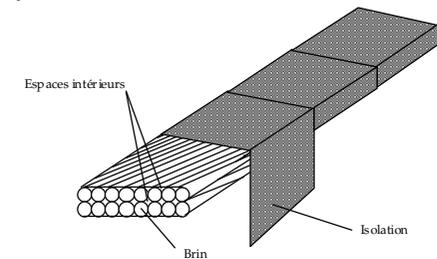
# Accelerator magnets

- "Wet" magnets with "heat exchanger"
  - Large internal losses and smaller stored energy
  - Cooling Source : Internal tube flow
  - Single phase coolant in contact with conductor



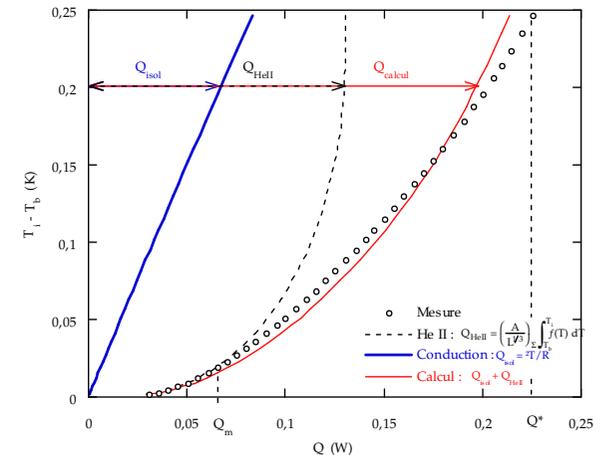
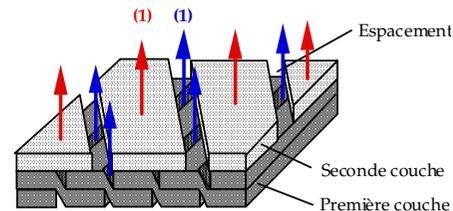
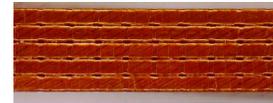
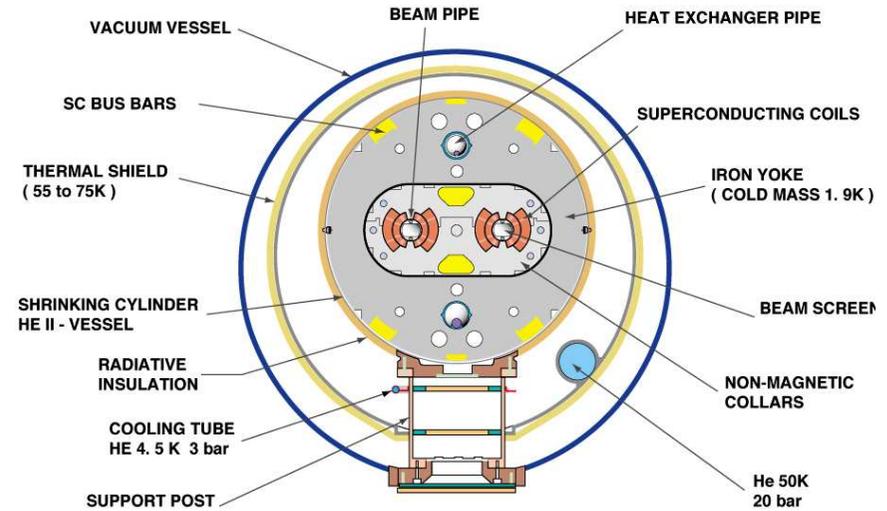
• Heat transfer between the conductor and the cooling source determines the temperature margin,  $\Delta T = T_b - T$

- **Electrical insulation constitutes the largest thermal barrier**
- Heat transfer R&D on the LHC insulation (90's) (Dapnia (C. Meuris) and KEK)
  - Permeability increase in the insulation to create heat paths
  - Creation of space between the insulations and the conductors
  - Removal of epoxy resin impregnation ("dry" magnet)
- **Little work on the materials**
  - Conductive doping, holes or porosity



# Accelerator magnets : LHC

- He II cooling
  - Two-phase He II for the exchanger
  - Stagnant He II for the magnet
- "Beam losses" in LHC
  - 10 mW/cm<sup>3</sup> or 0.4 W/m (cable)
  - $\Delta T < 0.3$  K with permeable insulation
  - $\Delta T \sim 4$  K with monolithic insulation
- Electrical Insulation is
  - Historically: double wrapping
    - Polyimide with 50% overlap
    - Fiberglass + epoxy resin with spacing
  - LHC Insulation : triple polyimide wrapping
    - First 2 wrappings without overlap
    - 3rd wrapping with spacing
- A thermal Insulation
  - Kapton/ Kapton : 120  $\mu$ m thick
  - $\varnothing \sim 10$   $\mu$ m, channel length of  $\sim$ mm
  - He II + Conduction



# Accelerator magnets : <sup>★</sup>Beyond LHC

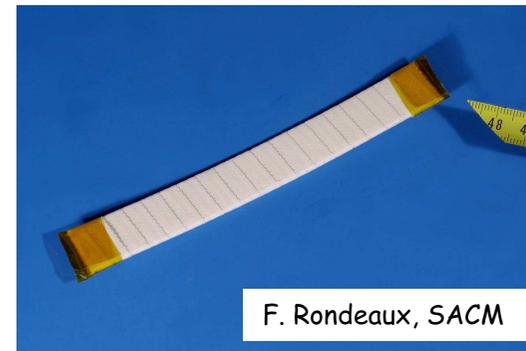
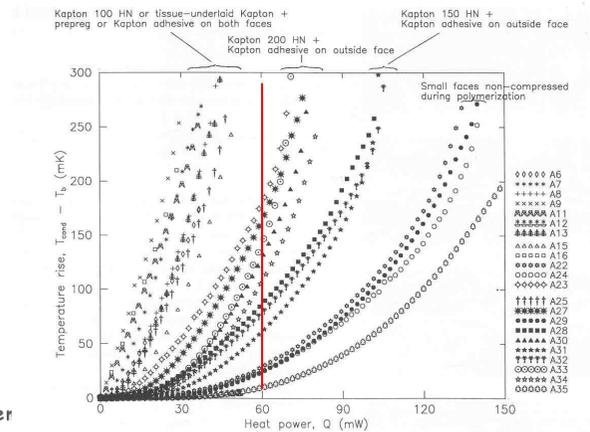
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- "Beam losses" of LHC upgrade with Nb<sub>3</sub>Sn Magnets
  - 50 to 80 mW/cm<sup>3</sup> or 2 to 3 W/m (cable) → ΔT?
- **Innovative ceramic insulation (under development)**
  - Thermal treatment (insulation+Nb<sub>3</sub>Sn, easier and less costly construction)
  - Fiberglass + ceramic precursor (CEA patent)
  - Heat transfer considerations
    - Higher heat transfer rate, larger He Volume in the insulation (Cp) and heat exchange surface increase (matrix participation)

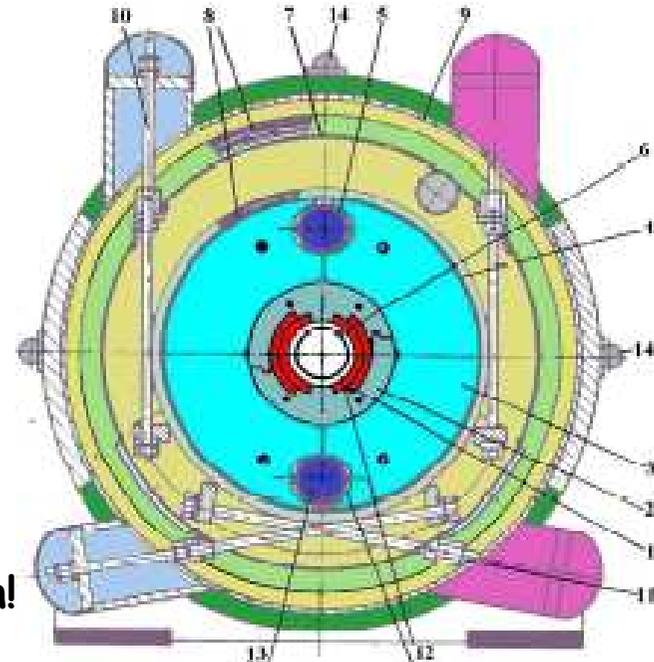
	Ceramic	Classic (Polyimid)
Pore size	d~100 μm (peak)	10 μm at Saclay to 100 μm at KEK
Porosity ε	4.5 to 29 %	~1 %
Conductivity	k≈4 10 <sup>-2</sup> W/Km	k <sub>kapton</sub> ≈10 <sup>-2</sup> W/Km @ 2 K



F. Rondeaux, SACM

# Pulsed magnets at GSI

- **Cooling**
  - He two phase flow at 4.2 K & 1 bar
  - Supercritical helium flow
    - 4,4 K at 3 bar and 5 g/s
- **"AC losses"**
  - SIS 300 (UNK) 1 T/s  $\rightarrow$  0.6 W/m
  - $\Delta T \sim 2$  K with impermeable insulation
  - $\Delta T \sim 200$  mK with permeable insulation!
- **Insulation with Holes?**
  - 2 layers of Polyimide 25  $\mu\text{m}$  with adhesive (50 % overlap)
  - 26% of the surface in contact with He
- **R&D to be done on insulation heat transfer**
  - Tests at SACM in 2007
  - In supercritical, static He (3 bars)



M. Wilson, GSI

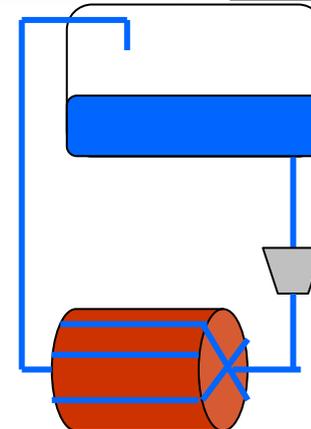
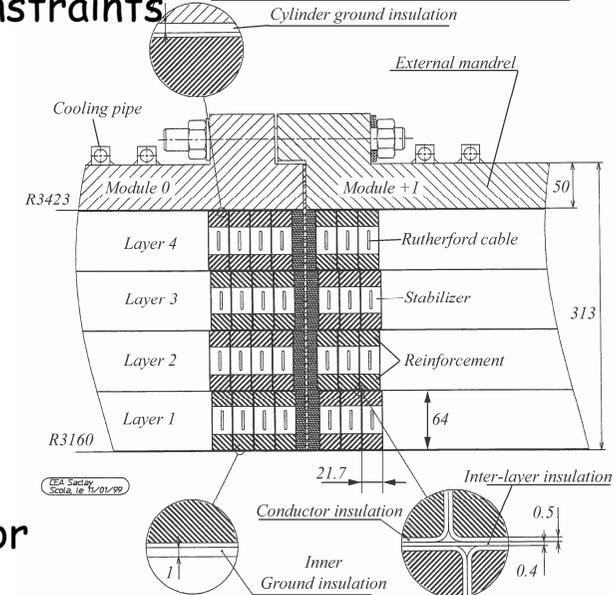
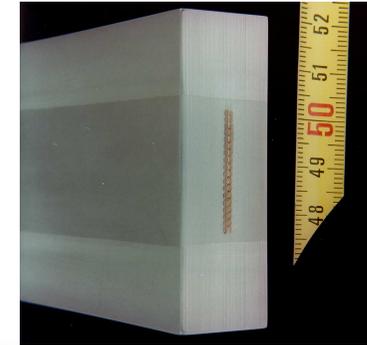
# Detector Magnets

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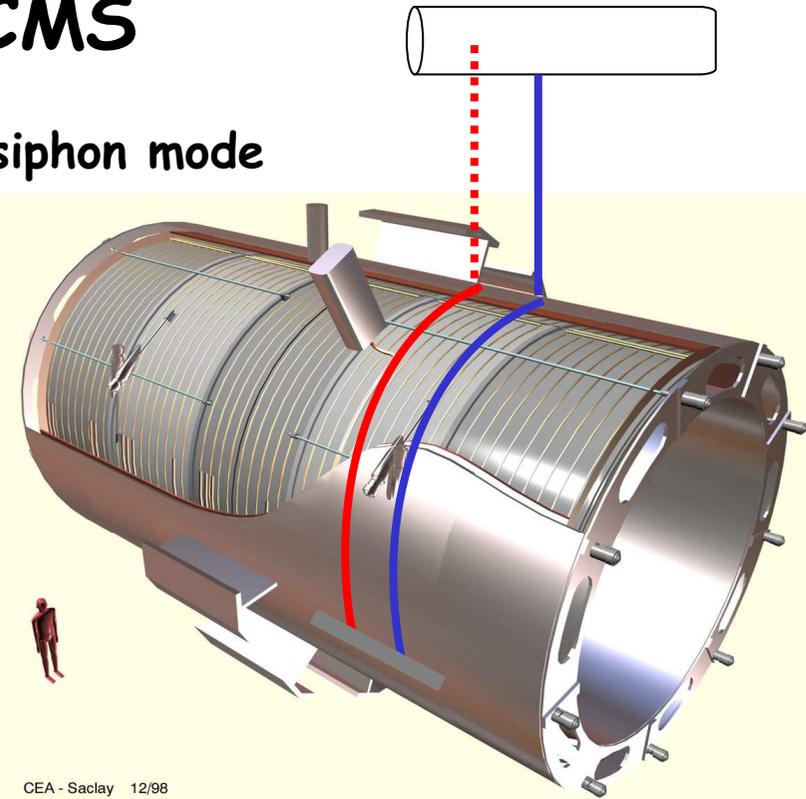
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- Large scale magnet
  - Larger stored energy and smaller thermal losses
  - Large thermal stabilizer Cross-sectional needed
  - $T_{\max}$  and  $\nabla T$  to minimize the mechanical constraints
- Dry" magnet
  - Reduced quantity of cryogen
  - High purity aluminum stabilized conductor
  - Fully impregnated coil with epoxy resin
- Heat transfer
  - Cold source : He reservoir / phase separator
  - Two-phase flow of He I in external tubes
    - Forced flow or natural two-phase flow



# Detector Magnets : CMS

- Two-phase convection in thermosiphon mode
  - Solenoid with "vertical parts"
- Heat transfer
  - 4.5 K at 1.25 bars
  - Tests at CERN  $\Delta T = 0.1$  K et 0.2 K



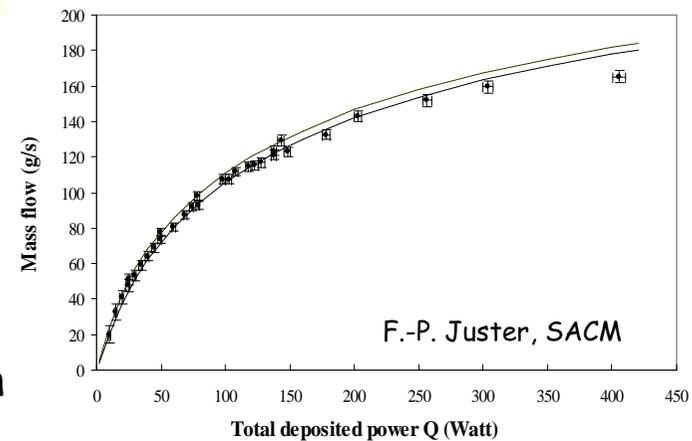
CEA - Saclay 12/98  
 DSM DAPNIA STCM

CMS Solenoïde



P. Bredy, SACM

- R&D done on "Thermosiphon" flow
  - Validation Homogeneous model
  - "Large scale" experimental validation



F.-P. Juster, SACM

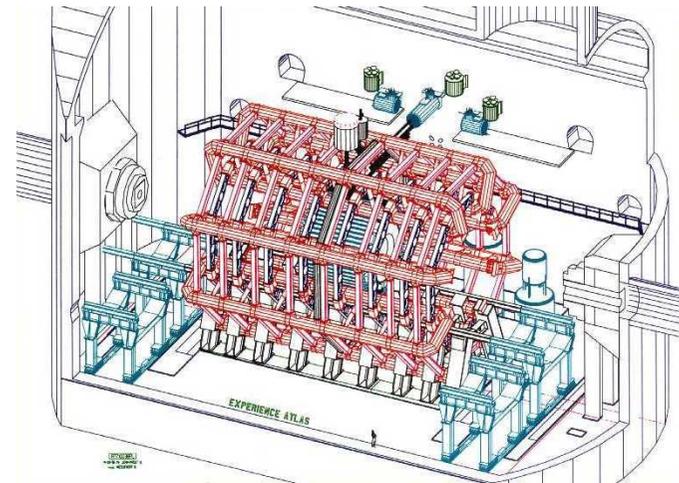
# Detector Magnets : ATLAS

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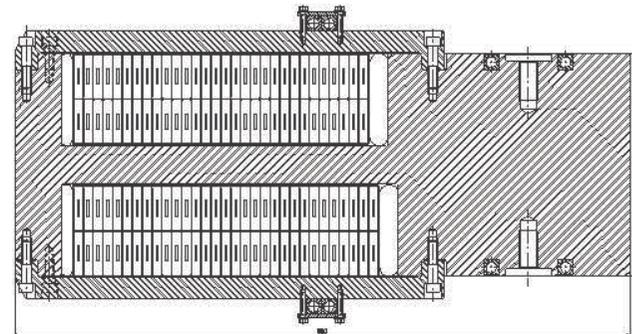


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- Helium two-phase forced convection
  - Toroid with long horizontal parts
- Heat transfer
  - 4.5 K at 1.5 bars
  - $\Delta T=0.15$  K et  $\Delta p=0.2$  bars



C. Mayri, SACM



- R&D done at Saclay on circulator
  - 0.1 kg/s  $\rightarrow$  1.2 kg/s
  - Tests of 0.6 kg/s circulators

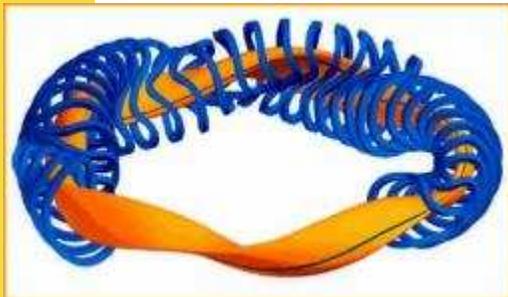
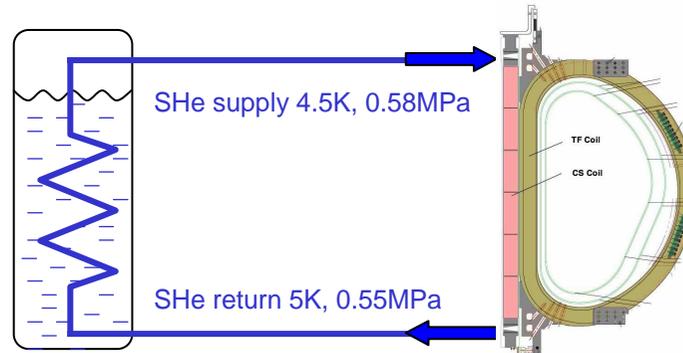
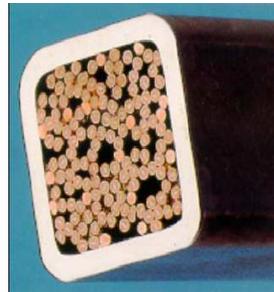
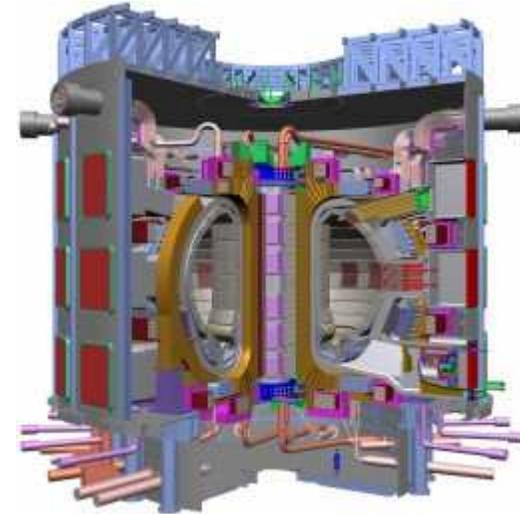
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# Magnets for fusion

- Large losses due to plasma and radiation
- Direct cooling with Cable in conduit conductor
- ITER
  - Enormous, known and tested technology
  - Supercritical helium flow at 4.5 K and 6 bars



- W7X
  - Supercritical helium at 3.8 K and 6 bars max
  - Experimental testing facility at Saclay
    - 4.5 K to 7.6 K, p=6 to 10 bars and  $I \approx 18$  kA
  - Largest experimental data base on CICC cooled magnet in operation at Saclay

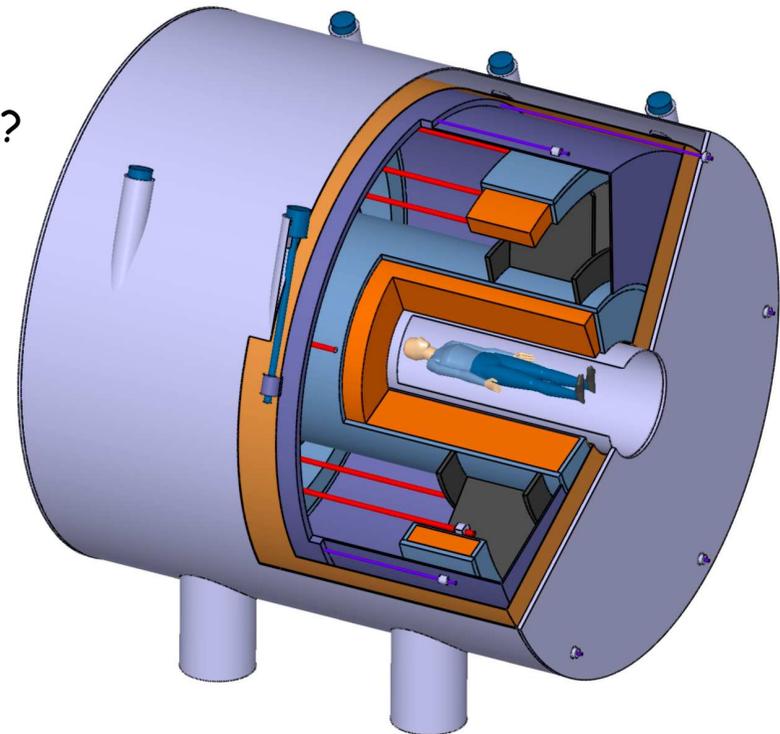
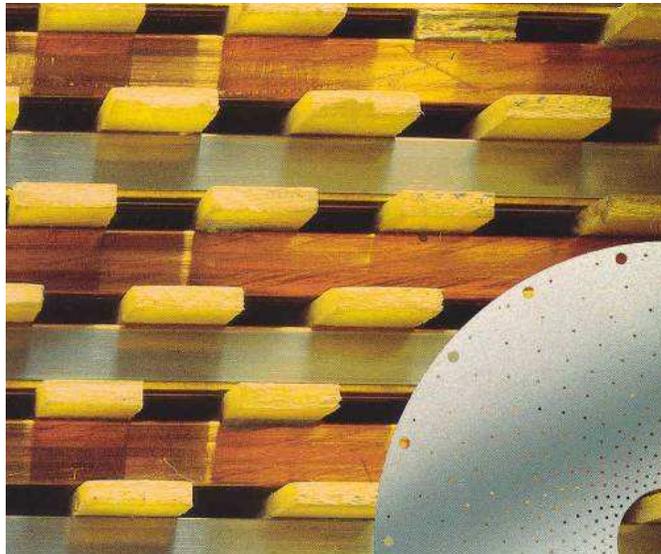
# Magnet for life science

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- "Wet" and "cryostable" magnet
  - Cold source : He II static helium
  - Large He II bath (volume ~ 1000 l)
  - No perturbation of the medical environment!
- Heat transfer
  - T=1.8 K at 1.25 bars
  - Insulator/separator of conductors creates channels
  - Channel heat transfer know in He II
- Transient heat transfer and hydraulics?



# Design limits and future needs

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- "Wet" magnets cooled with single phase submitted to phase change
  - Iseult ou LHC
  - Pressure rise due to magnet quench

**Development of experimental and theoretical thermo hydraulics models**

- Next generation of accelerator magnets

**Improvement of heat transfer in the magnet (Insulation et design)**

- HTS magnets / Single unit magnet
  - Cryocooler and fluid coupling

**Autonomous cooling device : cryocooler + fluid**

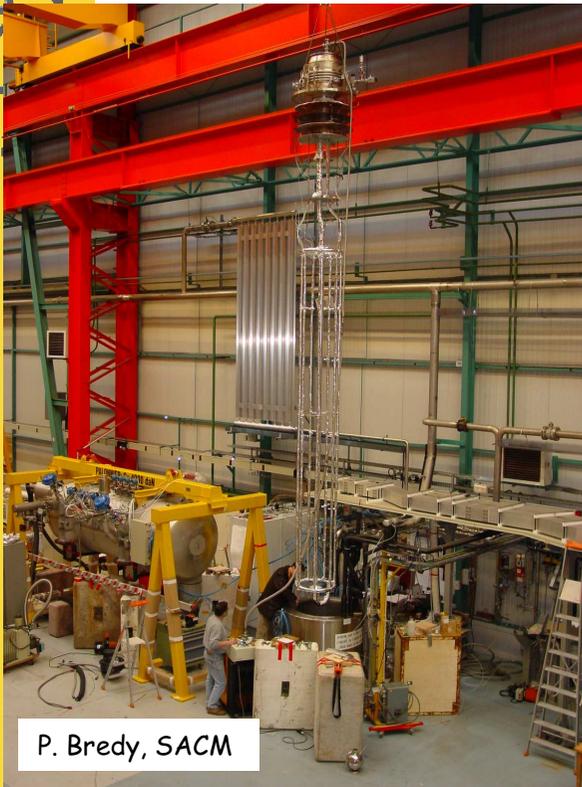
# Cryogenics R&D at Dapnia (1/3)

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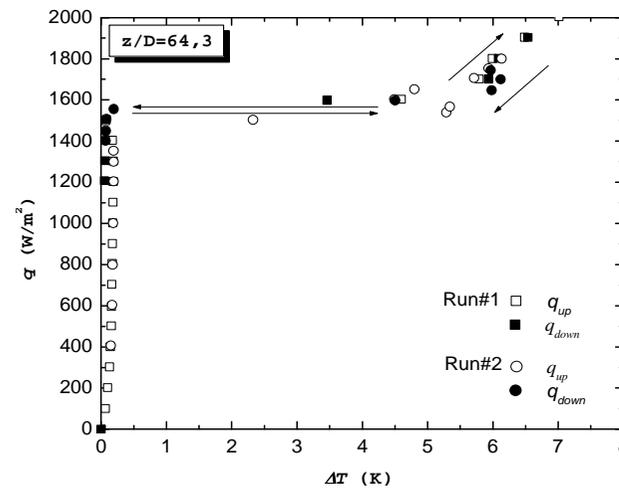
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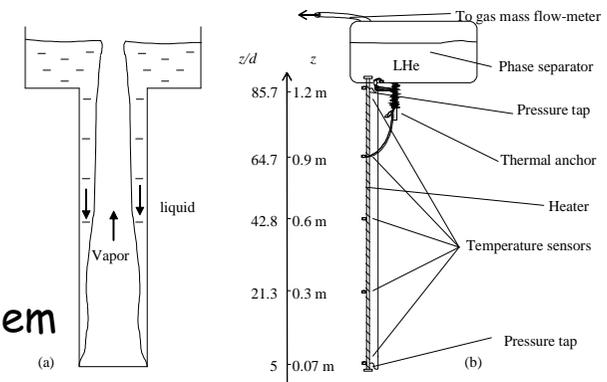
- Fluid dynamics and heat transfer in a He two-phase thermosiphon (CMS)
  - 1 m Experimental loop (Fundamental flow properties, models, 1 PhD)
  - 9 m Experimental loop (Large scale)



P. Bredy, SACM

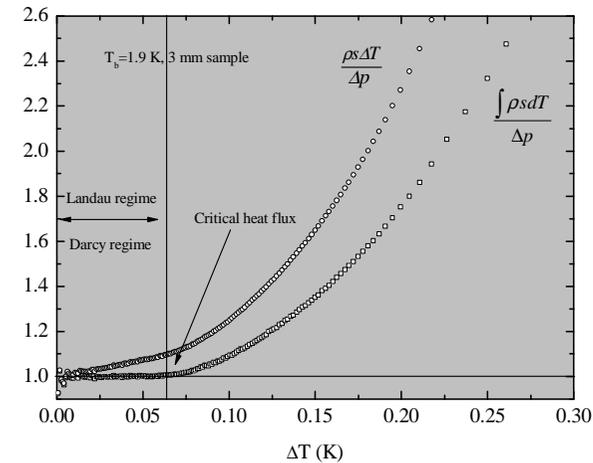
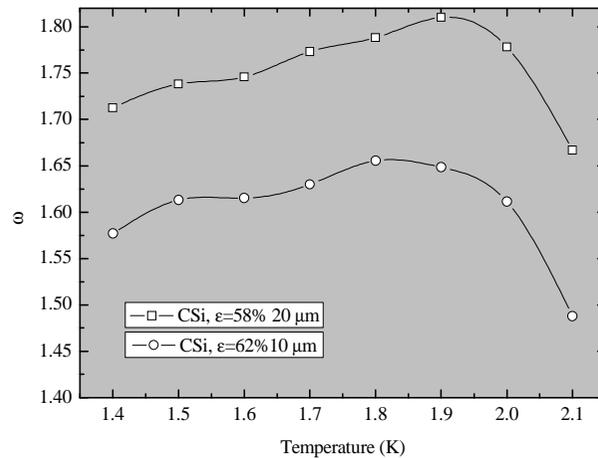
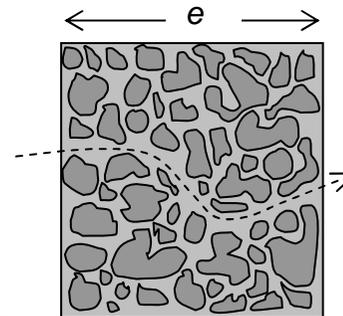
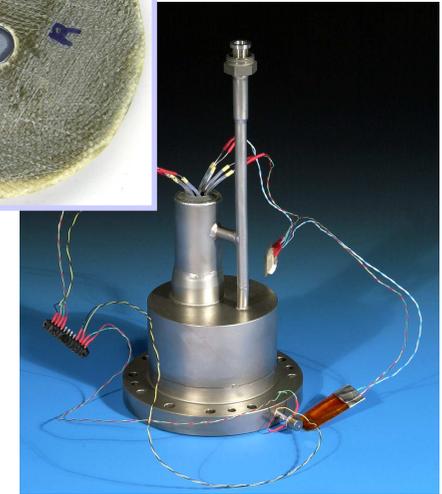


- Helium "Heat pipe" development
  - Internal R&D interne for autonomous system
    - Cryocooler + fluids



# Cryogenics R&D at Dapnia (2/3)

- He II Heat transfer in porous media
  - Tests on porous “scaled” sample
- Fundamentals on transport properties
  - Permeability  $K(T)$
  - Tortuosity  $\omega$



$$\Delta p = \left[ \int \rho s \vec{\nabla} T \right] \neq \rho s \Delta T$$

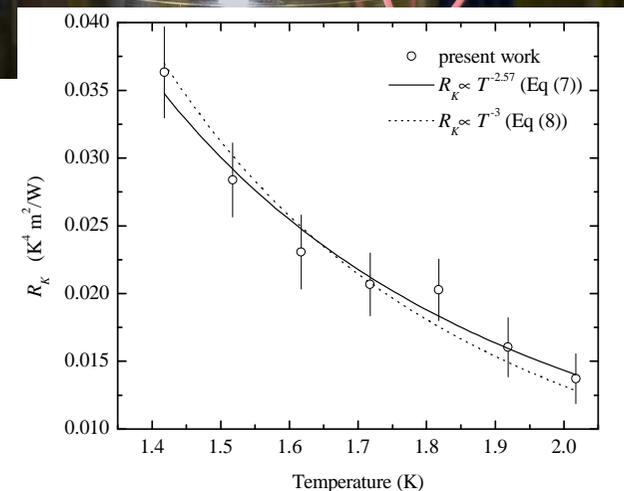
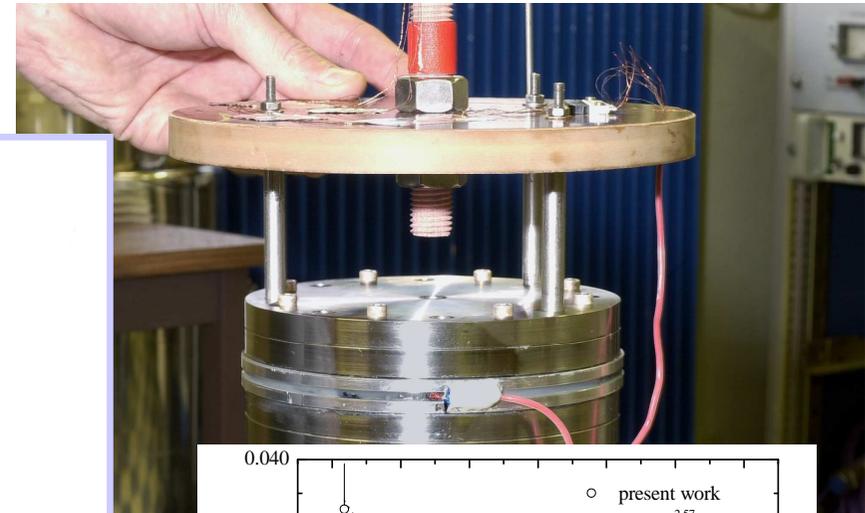
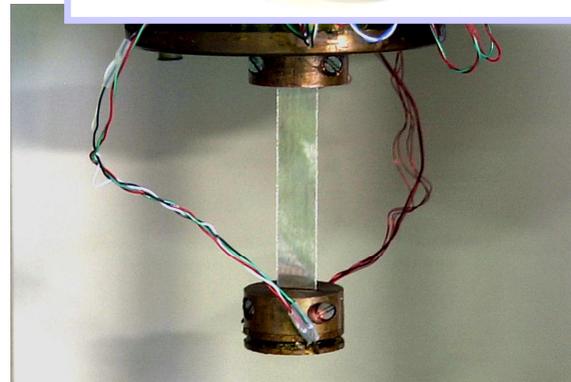
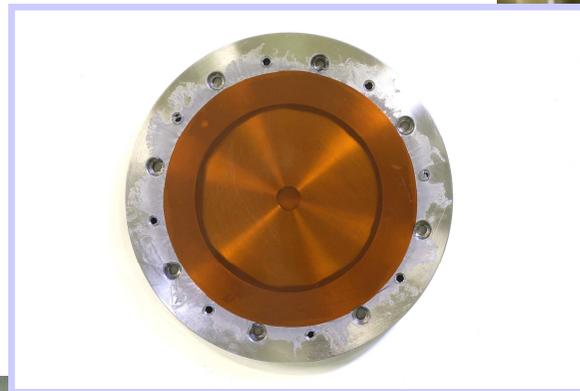
# Cryogenics R&D at Dapnia (3/3)

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- Thermal properties of materials
  - Kapitza resistance and thermal conductivity in He II
    - Kapton, Mylar, Apical, ...
- Thermal conductivity and diffusivity (4 K à 300 K)
  - Insulators and conductors



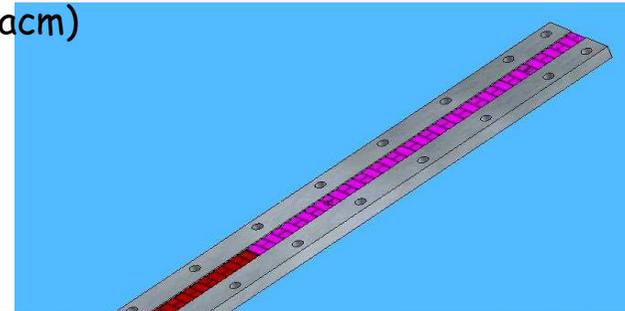
# R&D propositions (1/3)

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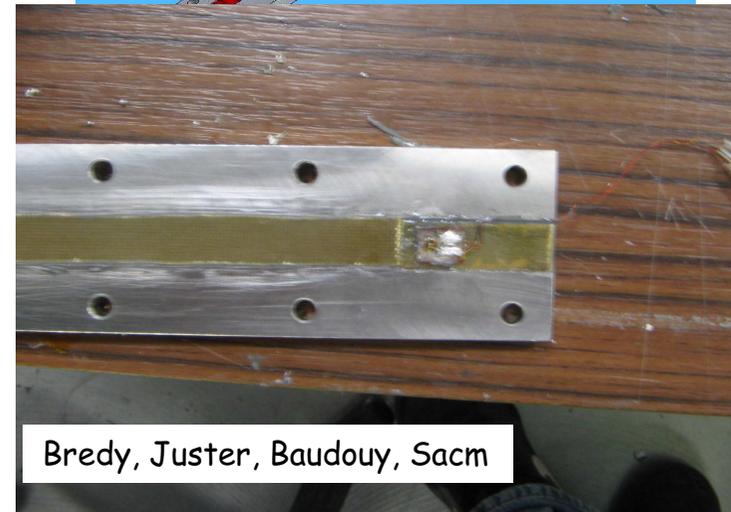
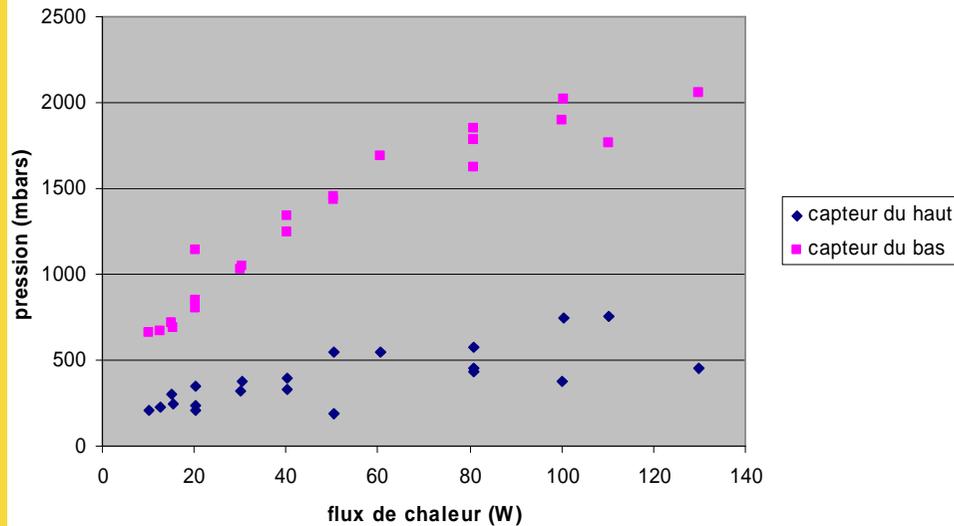


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- Pressure rise in magnets due to quench (transient thermo-hydraulics)
  - In the frame work of Iseult and SEHT
    - First experimental rig and first results on channel pressure rise in He II
    - Analytical work in progress (C. Meuris, Sacm)



évolution des pressions maximum en fonction du flux de chaleur pour l'hélium superfluide à 1,8K et 16mbars



To be continued... and generalized to accelerator magnet

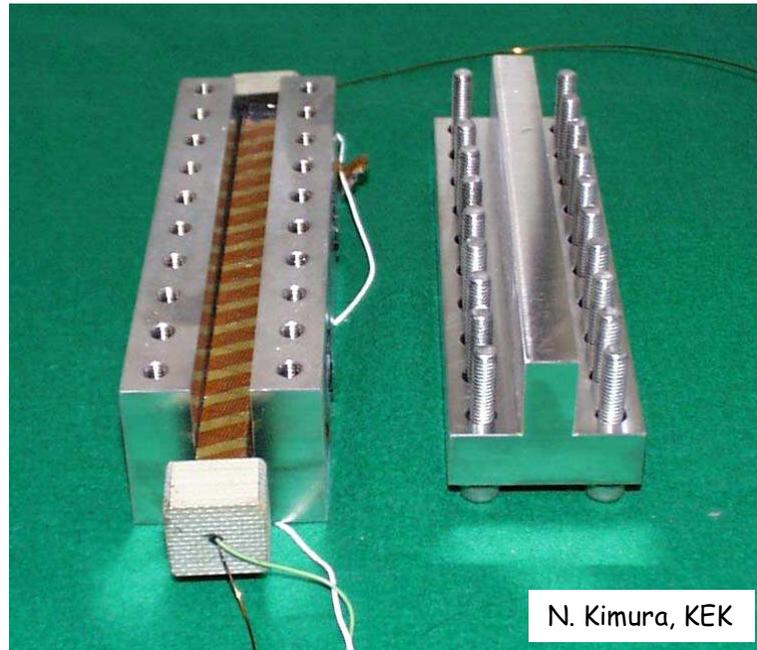
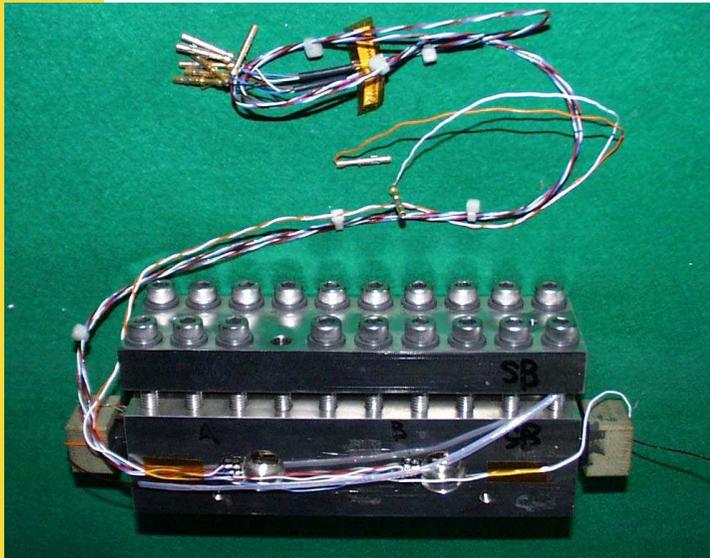
## R&D propositions (2/3)

dapnia



saclay

- He II heat transfer through innovative insulation
  - Experimental and theoretical work on "scaled" porous media
    - NIFS, IMFT
  - Experimental work and modeling on stack of conductors (coil) (NED)
    - KEK, CERN, WTU



- To be continued in the framework of NED or any another...

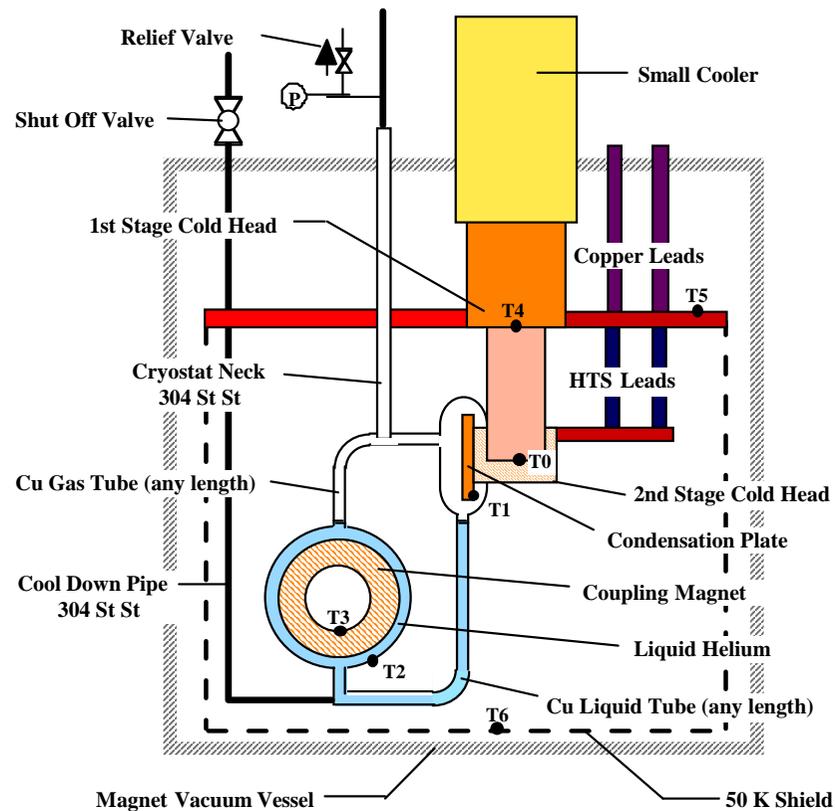
# R&D propositions (3/3)

dapnia

cea

saclay

- Autonomous loop with cryocooler and fluids
  - For small magnet, Targets and magnet for other scientific communities



Mice

- To be started... to be in the train...