

# **Beam optics correction and non-linear magnet calibration from resonant driving terms**

Andrea Franchi (ESRF, Grenoble)

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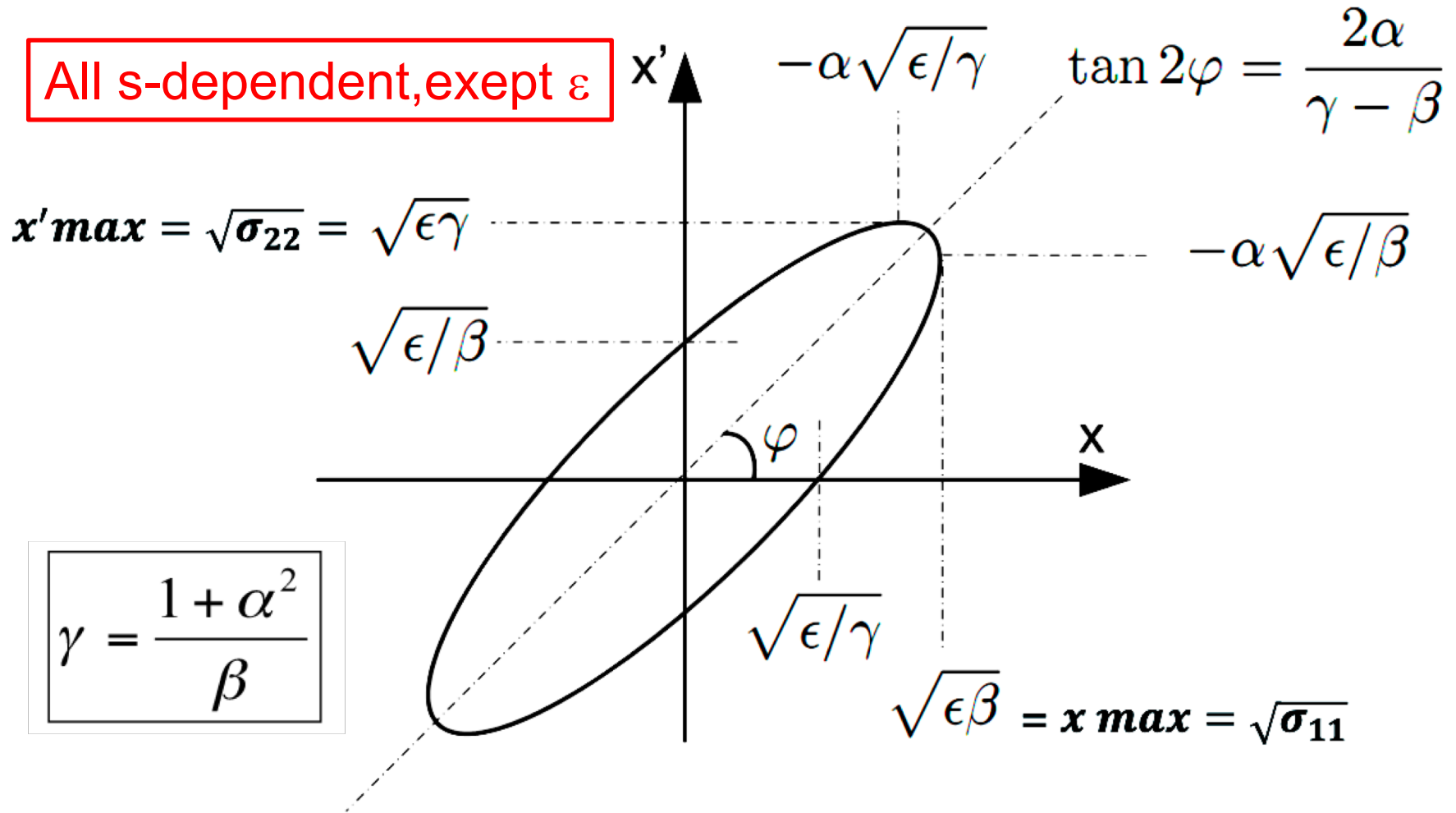
- Resonance Driving Terms Introductory (15')
- Linear optics errors (10')
  1. RDTs Vs beta-beating and phase advance error
  2. RDTs measurements & correction
  3. Accuracy and precision analysis
- Betatron coupling (10')
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  1. Localization & detection of nonlinearities via RDTs
  2. RDTs Vs chromatic functions and orbit feed-downs



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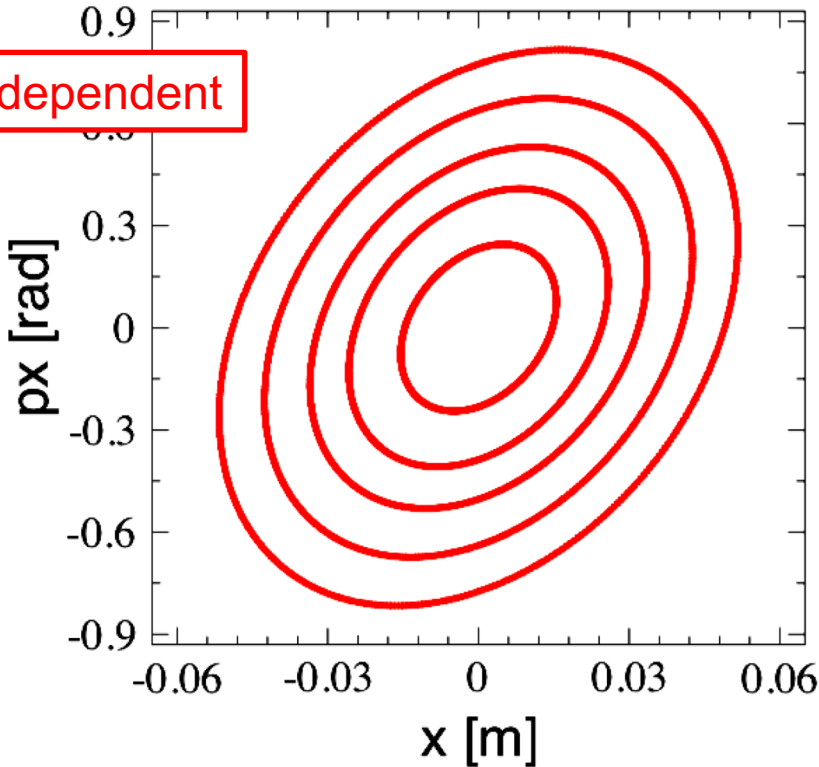
## Linear lattice phase space (Cartesian coordinates) & physical meaning of the Twiss parameters

All s-dependent, except  $\epsilon$



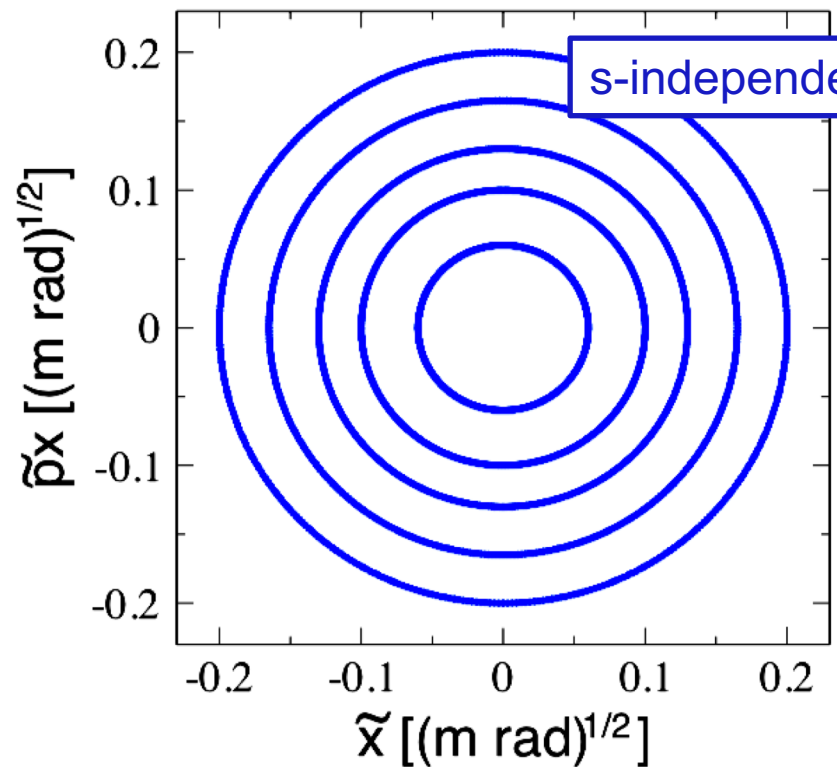
## Linear lattice phase space (@ “small” amplitudes)

CARTESIAN COORDINATES



s-dependent

COURANT-SNYDER COORDINATES



s-independent

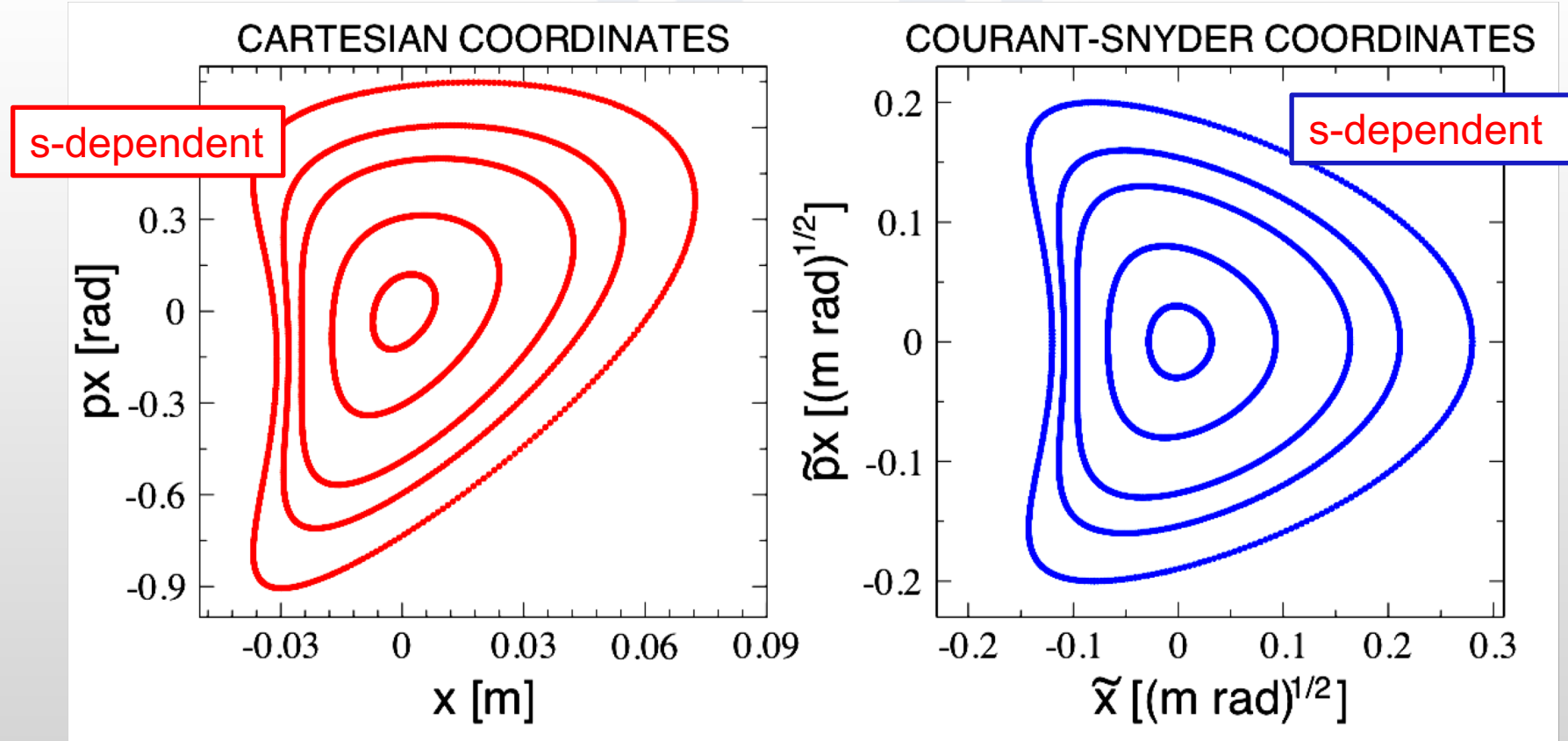
$$\begin{pmatrix} \tilde{x} \\ \tilde{p}_x \end{pmatrix} = \begin{pmatrix} (\beta_x)^{-1/2} & 0 \\ \alpha_x (\beta_x)^{-1/2} & (\beta_x)^{1/2} \end{pmatrix} \begin{pmatrix} x \\ p_x \end{pmatrix}$$

s-dependent

tune (i.e. phase-space rotation  $R$ ) is amplitude independent

$R$

## Nonlinear lattice phase space (@ “large” amplitudes)

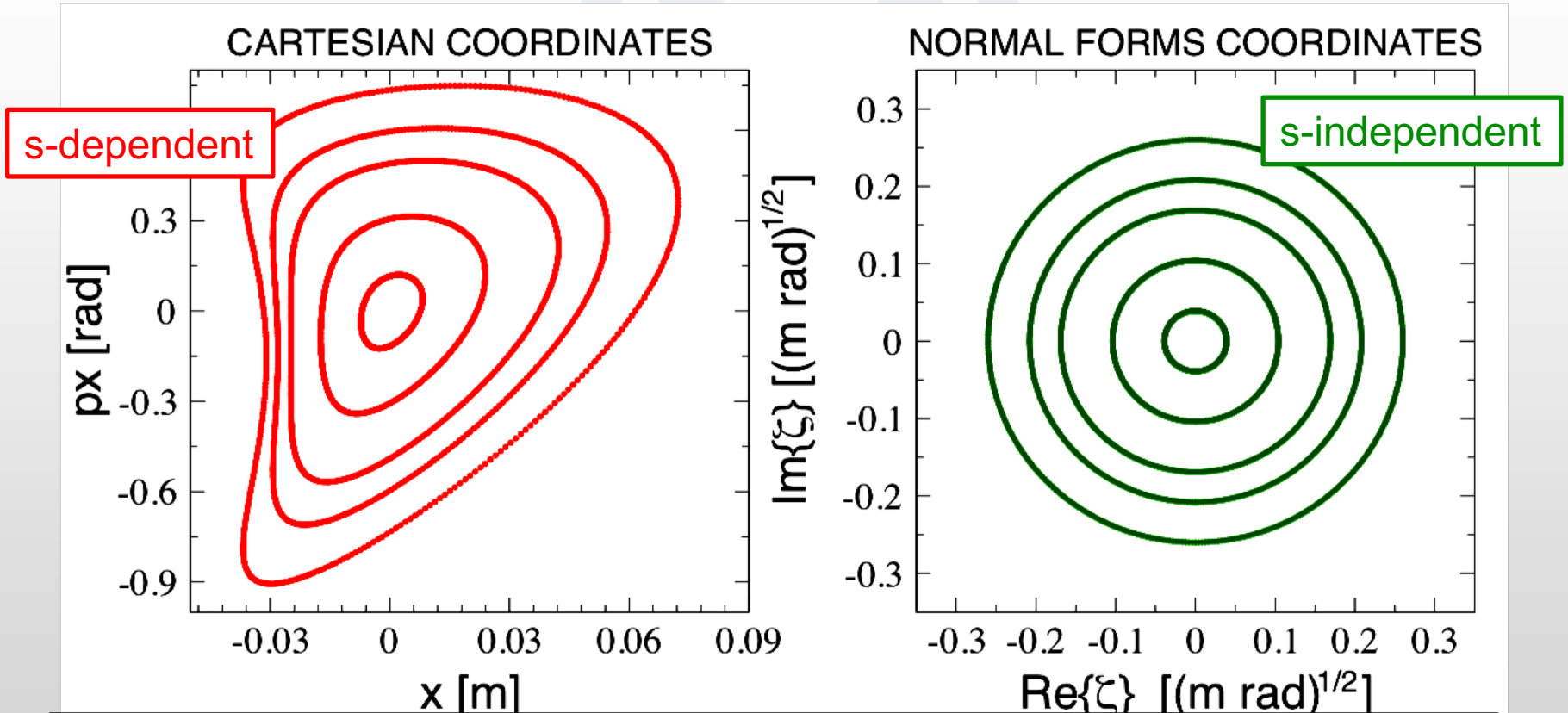


$$\begin{pmatrix} \tilde{x} \\ \tilde{p}_x \end{pmatrix} = \begin{pmatrix} (\beta_x)^{-1/2} & 0 \\ \alpha_x (\beta_x)^{-1/2} & (\beta_x)^{1/2} \end{pmatrix} \begin{pmatrix} x \\ p_x \end{pmatrix}$$

s-dependent

**C-S transformation not sufficient to retrieve s-independent circles**

## Nonlinear lattice phase space (@ “large” amplitudes)



Stable (nonlinear) motion => closed phase-space curves => it must exist a transformation that converts  $(x, px)$  **distorted curves** into **circles**: **Normal Forms transformation** whose coefficients are the Resonance Driving Terms (i.e. generalization of Twiss parameters)

## Nonlinear lattice phase space (@ “large” amplitudes)

	linear case	nonlinear case
1. Cartes. phase space	ellipse	closed distorted
2. C-S transformation	Twiss parameters (real)	
3. C-S phase space	circle	closed distorted
4. Nor. For. transformat.		RDTs (complex)
5. Nor. For. phase space		circle
6. tune	amplitude indep.	amplitude dep.

Stable (nonlinear) motion => closed phase-space curves => it must exist a transformation that converts  $(x, px)$  **distorted curves** into **circles**: **Normal Forms transformation** whose coefficients are the Resonance Driving Terms (i.e. generalization of Twiss parameters)

## Twiss parameters ( $\beta$ , $\alpha$ , $\phi$ , $\gamma$ )

- describe and account for **linear focusing** lattice
- transform phase space **elliptic orbits** into circles (tune amplitude independent)
- are measurable and deviation from model values reveal errors in **quadrupoles**

## RDTs $f_{jklm}$

- describe and account for **coupling & nonlinear focusing** lattice
- transform phase space **distorted orbits** into circles (tune amplitude dependent)
- are (most of the time) measurable and deviation from model values reveal errors in **sextupoles, octupoles**, etc ...

Stable (nonlinear) motion => closed phase-space curves => it must exist a transformation that converts (**x,px**) **distorted curves** into **circles**: **Normal Forms transformation** whose coefficients are the Resonance Driving Terms (i.e. generalization of Twiss parameters)

How are RDTs  $f_{jklm}$  selected and computed?

multipole kind	$n$	potential term	index relations
norm. quad. $x$	2	$x^2$	$j + k = 2 \quad m + l = 0$
norm. quad. $y$	2	$y^2$	$j + k = 0 \quad m + l = 2$
skew quad.	2	$xy$	$j + k = 1 \quad m + l = 1$
norm. sext. 1	3	$x^3$	$j + k = 3 \quad m + l = 0$
norm. sext. 2	3	$xy^2$	$j + k = 1 \quad m + l = 2$
skew sext. 1	3	$y^3$	$j + k = 0 \quad m + l = 3$
skew sext. 2	3	$x^2y$	$j + k = 2 \quad m + l = 1$



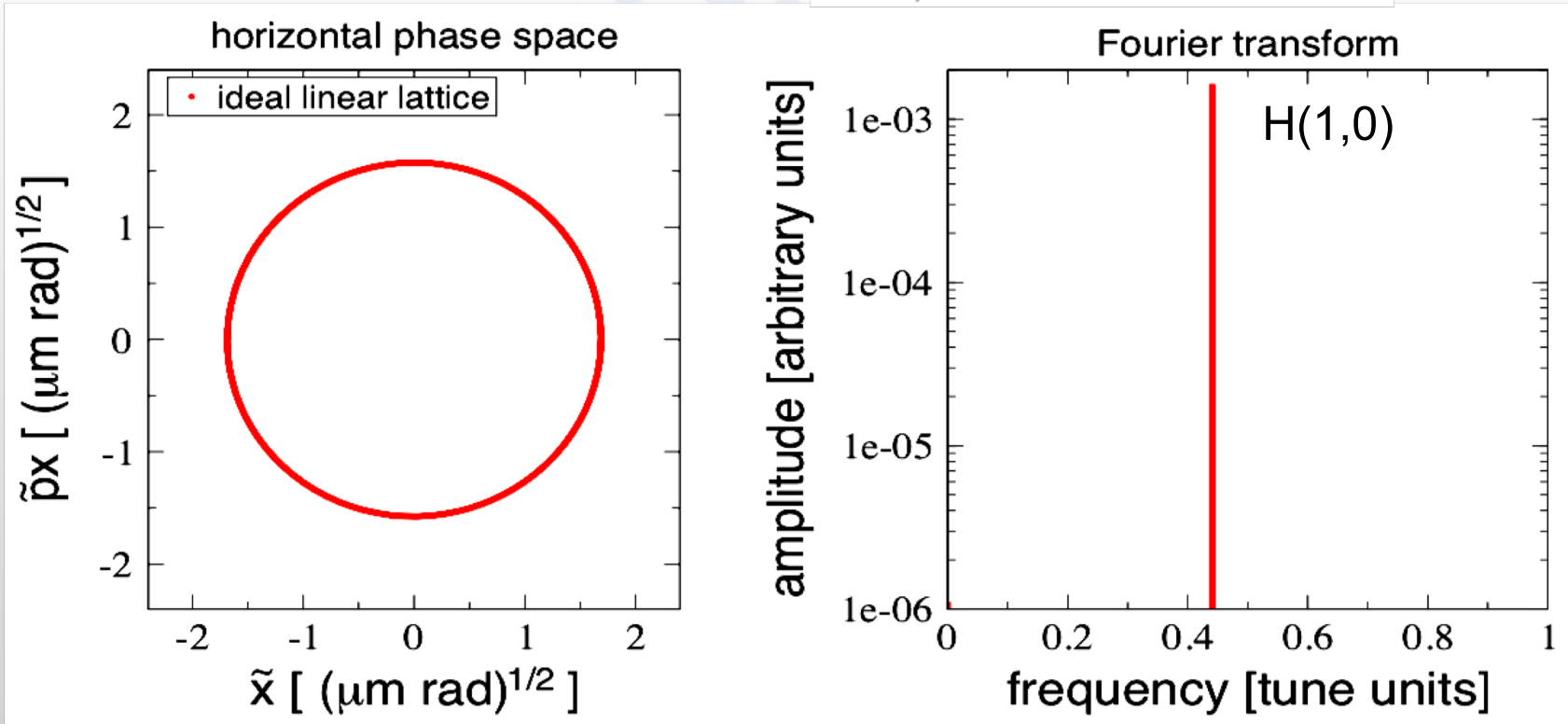
## How are RDTs $f_{jklm}$ selected and computed?

RDT	resonance and magnetic term
$f_{1001}^{(1)} = \frac{\sum_w J_{w,1} \sqrt{\beta_x^w \beta_y^w} e^{i(\Delta\phi_{w,x} - \Delta\phi_{w,y})}}{4 [1 - e^{2\pi i(Q_x - Q_y)}]}$	(1,-1) skew quadrupole
$f_{1010}^{(1)} = \frac{\sum_w J_{w,1} \sqrt{\beta_x^w \beta_y^w} e^{i(\Delta\phi_{w,x} + \Delta\phi_{w,y})}}{4 [1 - e^{2\pi i(Q_x + Q_y)}]}$	(1, 1) skew quadrupole

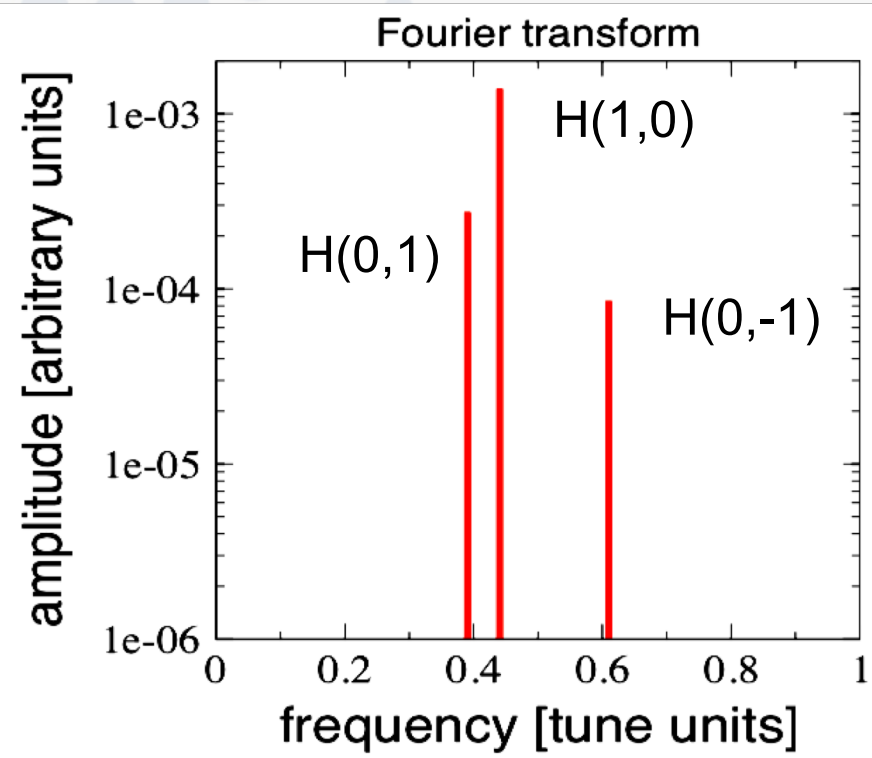
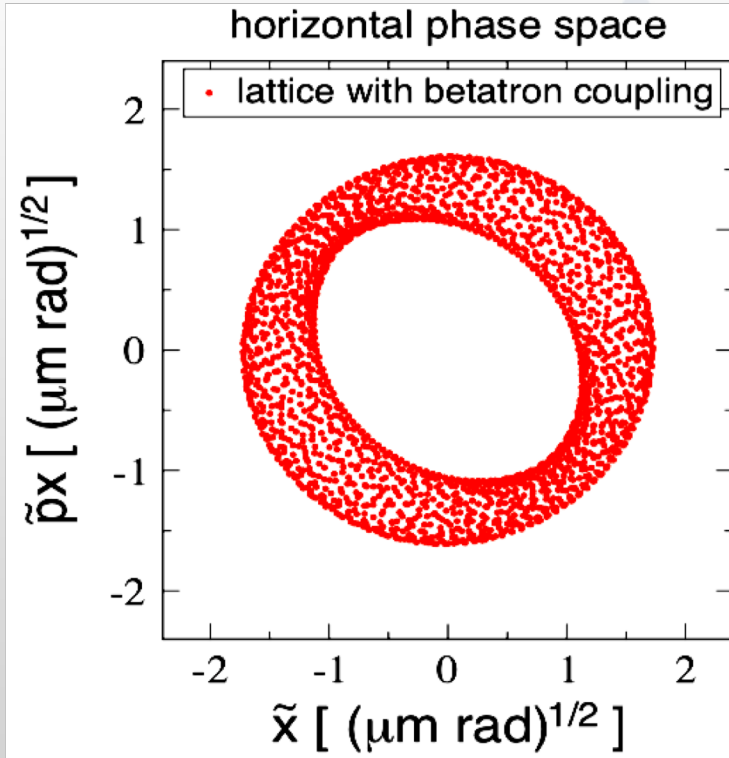
- scale linearly with (all) magnet strengths  $J_1, K_2, ..$
- small denominators depend on tune resonant condition  $(j-k)Q_x + (l-m)Q_y = M \Rightarrow$  name Resonance Driving Terms
- scale differently on beta functions

RDT	resonance and magnetic term
$f_{3000}^{(1)} = -\frac{\sum_w K_{w,2} (\beta_x^w)^{3/2} e^{i(3\Delta\phi_{w,x})}}{48 [1 - e^{2\pi i(3Q_x)}]}$	(3,0) normal sextupole
$f_{1200}^{(1)} = -\frac{\sum_w K_{w,2} (\beta_x^w)^{3/2} e^{i(-\Delta\phi_{w,x})}}{16 [1 - e^{2\pi i(-Q_x)}]}$	(1,0) normal sextupole
$f_{1020}^{(1)} = \frac{\sum_w K_{w,2} \sqrt{\beta_x^w \beta_y^w} e^{i(\Delta\phi_{w,x} + 2\Delta\phi_{w,y})}}{16 [1 - e^{2\pi i(Q_x + 2Q_y)}]}$	(1,2) normal sextupole
$f_{0120}^{(1)} = \frac{\sum_w K_{w,2} \sqrt{\beta_x^w \beta_y^w} e^{i(-\Delta\phi_{w,x} + 2\Delta\phi_{w,y})}}{16 [1 - e^{2\pi i(-Q_x + 2Q_y)}]}$	(1,-2) normal sextupole
$f_{0111}^{(1)} = \frac{\sum_w K_{w,2} \sqrt{\beta_x^w \beta_y^w} e^{i(-\Delta\phi_{w,x})}}{8 [1 - e^{2\pi i(-Q_x)}]}$	(1,0) normal sextupole

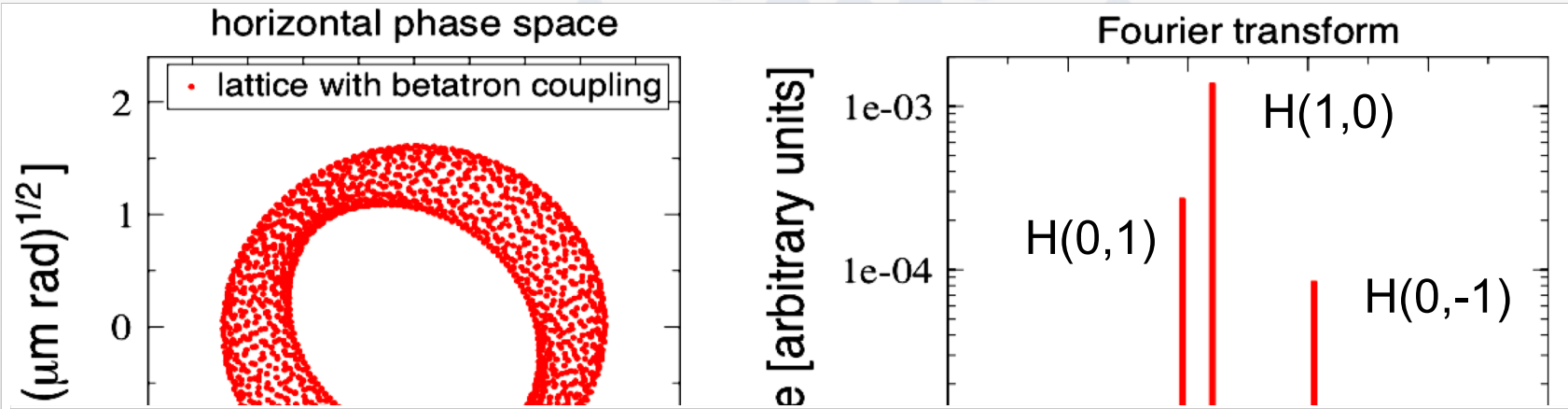
How are RDT  $f_{jklm}$  measured? Harmonic analysis of TbT BPM (complex) data  $h_{x,\pm} = \tilde{x} \pm i\tilde{p}_x$



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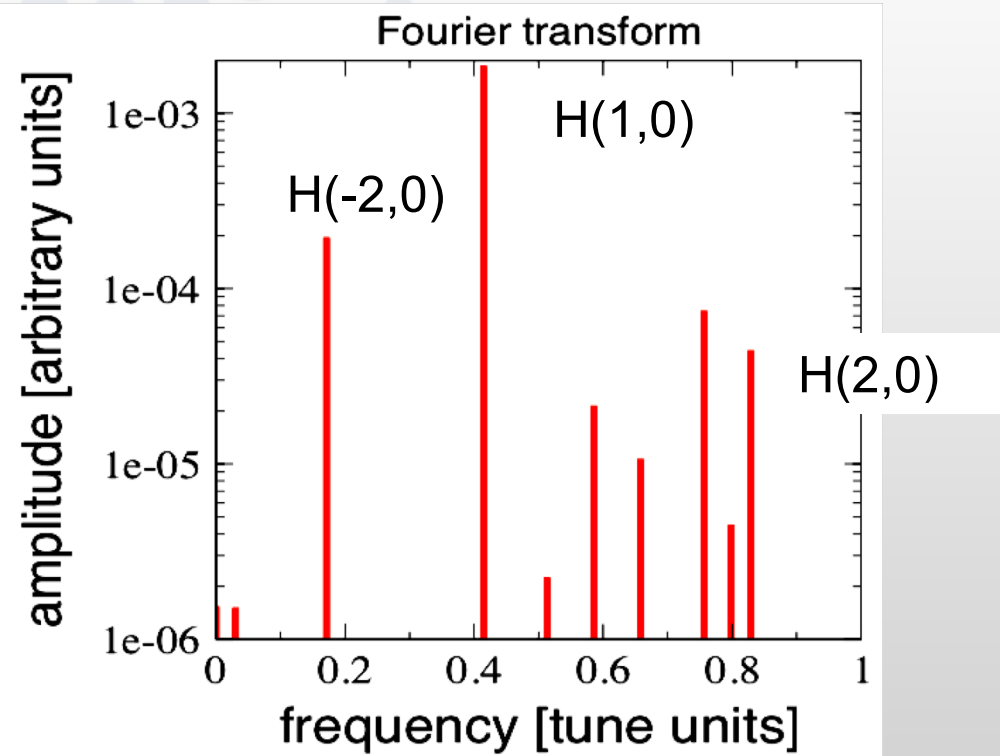
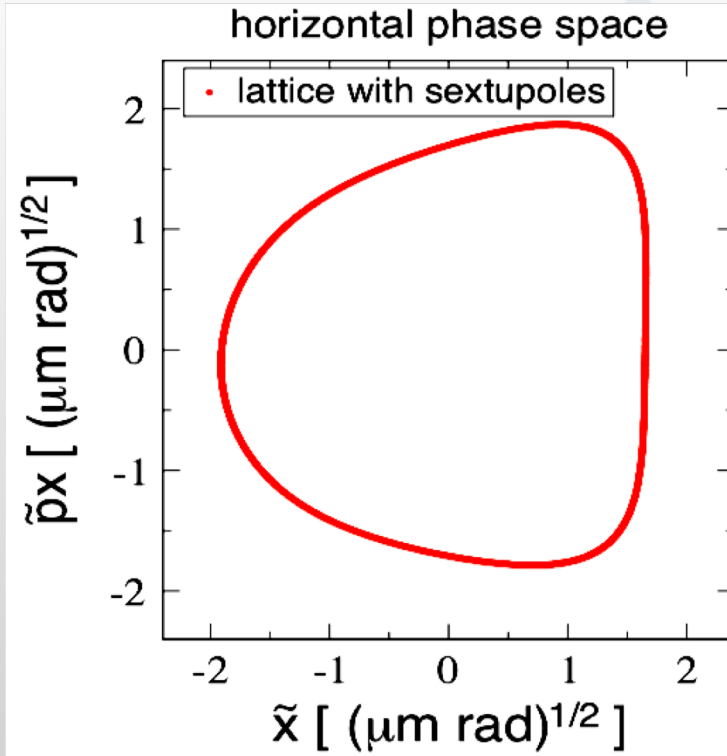


How are RDT  $f_{jklm}$  measured? Harmonic analysis of TbT BPM (complex) data  $h_{x,\pm} = \tilde{x} \pm i\tilde{p}_x$

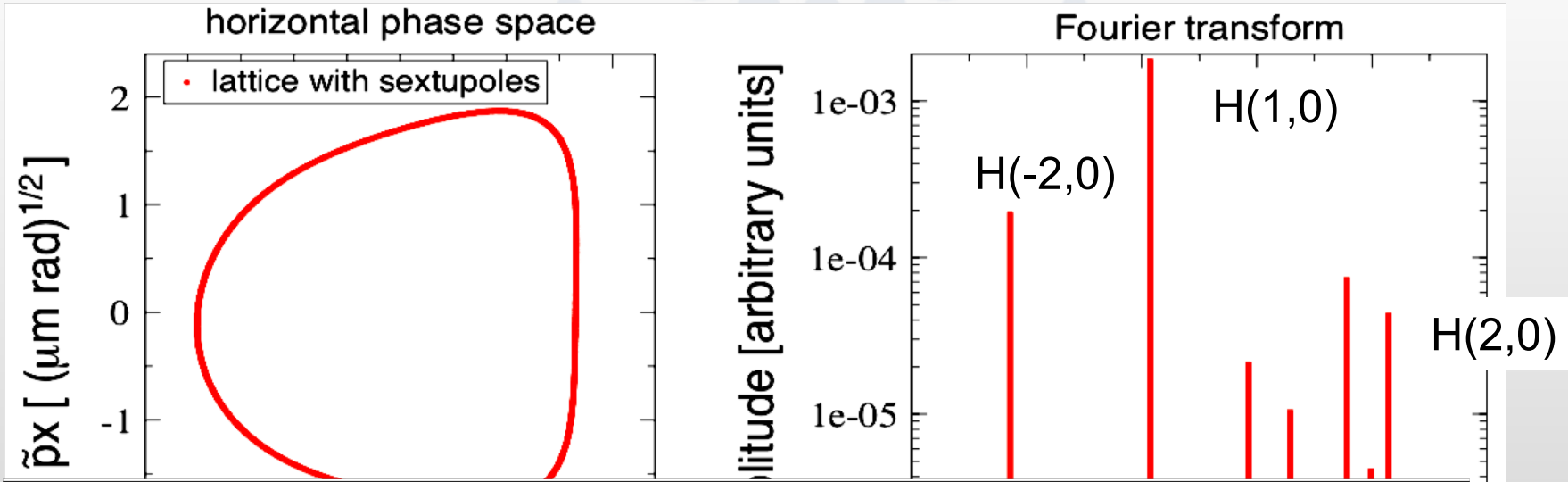


$jklm$	resonance	H-line	V-line	$ a_{jklm} $	$\phi_{jklm}^a$
0110	(1,-1)		(1,0)	$2 f_{0110} (2I_x)^{1/2}$	$\phi_{0110}^f + \psi_{x,0} - \frac{\pi}{2}$
1001	(1,-1)	(0,1)		$2 f_{1001} (2I_y)^{1/2}$	$\phi_{1001}^f + \psi_{y,0} - \frac{\pi}{2}$
1010	(1,1)	(0,-1)	(-1,0)	H: $2 f_{1010} (2I_y)^{1/2}$	H: $\phi_{1010}^f - \psi_{y,0} - \frac{\pi}{2}$
				V: $2 f_{1010} (2I_x)^{1/2}$	V: $\phi_{1010}^f - \psi_{x,0} - \frac{\pi}{2}$

How are RDT  $f_{jklm}$  measured? Harmonic analysis of TbT BPM (complex) data  $h_{x,\pm} = \tilde{x} \pm i\tilde{p}_x$



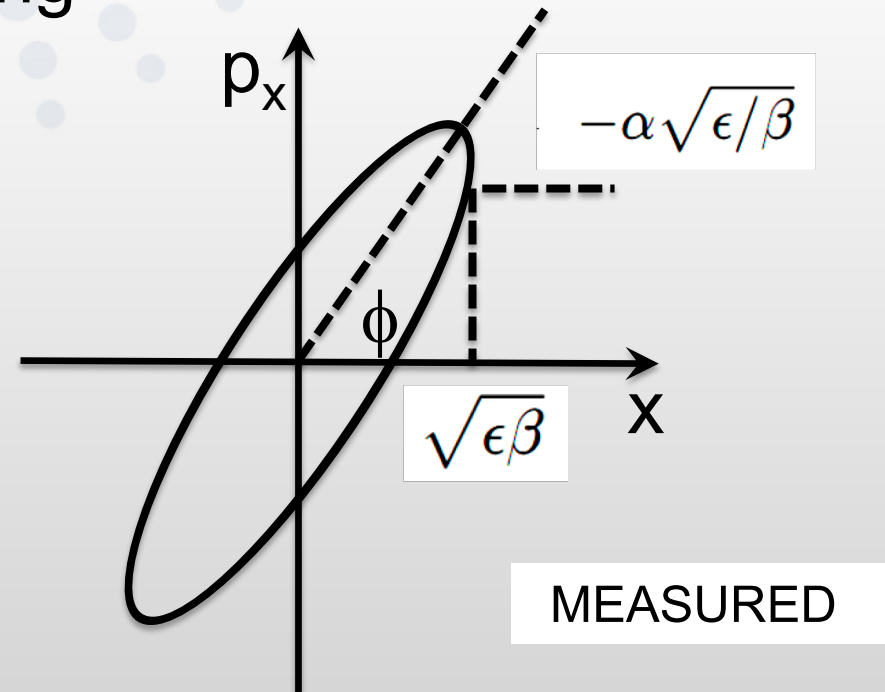
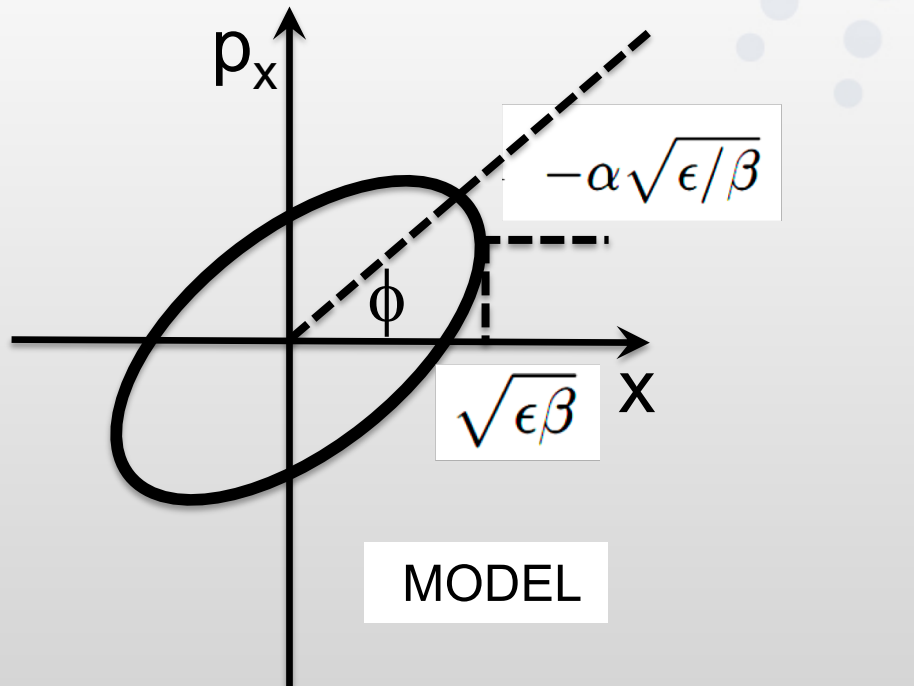
How are RDT  $f_{jklm}$  measured? Harmonic analysis of TbT BPM (complex) data  $h_{x,\pm} = \tilde{x} \pm i\tilde{p}_x$



$jklm$	resonance	H-line	V-line	$ a_{jklm} $	$\phi_{jklm}^a$	
1200	(1,0)	(2,0)		$2 f_{1200} (2I_x)$	$\phi_{1200}^f + 2\psi_{x,0} - \frac{\pi}{2}$	
2100	(1,0)	(0,0)		$4 f_{2100} (2I_x)$	$\phi_{2100}^f - \frac{\pi}{2}$	not observable
3000	(3,0)	(-2,0)		$6 f_{3000} (2I_x)$	$\phi_{3000}^f - 2\psi_{x,0} - \frac{\pi}{2}$	

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Focusing (quadrupole) errors induce deformation of phase space ellipse (i.e. of Twiss  $\beta$  and  $\alpha$ ) **and** betatron phase  $\phi$  along the ring



$$\frac{\Delta\beta}{\beta} = \frac{\beta^{(meas)} - \beta^{(mod)}}{\beta^{(mod)}}$$

$$\delta\phi_{ij} = \Delta\phi_{ij}^{(meas)} - \Delta\phi_{ij}^{(mod)}$$

$$\Delta\phi_{ij} = \phi_i - \phi_j \quad @ \text{ BPMs } i \& j$$



Focusing (quadrupole) errors  $\delta K_1$  excite half-integer resonance and the corresponding RDT  $f_{2000}$  (closely related to  $\beta$ -beating and phase errors)

$$f_{2000,j} = \frac{\sum_w^W \beta_{x,w}^{(mod)} \delta K_{w,1} e^{2i\Delta\phi_{x,wj}^{(mod)}}}{8(1 - e^{4\pi i Q_x})} + O(\delta K_1^2)$$

$$\left( \frac{\Delta\beta_x}{\beta_x} \right)_j = 8\Im \{ f_{2000,j} \} + O(|f_{2000}|^2)$$

$$\Delta\phi_{x,ij} \simeq \Delta\phi_{x,ij}^{(mod)} - 2h_{x,ij} + 4\Re \{ f_{2000,i} - f_{2000,j} \}$$

**Remark # 1:** By minimizing RDT  $f_{2000}$  @ BPMs,  $\beta$ -beating is automatically corrected, though not necessarily the phase errors, because detuning term  $h_{x,ij}$  is not observable

$$h_{x,ij} = -\frac{1}{4} \sum_{j < w < i} \beta_{x,w}^{(mod)} \delta K_{w,1} + O(\delta K_1^2)$$

$$\left( \frac{\Delta \beta_x}{\beta_x} \right)_j = 8 \Im \{ f_{2000,j} \} + O(|f_{2000}|^2)$$

$$\Delta \phi_{x,ij} \simeq \Delta \phi_{x,ij}^{(mod)} - 2h_{x,ij} + 4 \Re \{ f_{2000,i} - f_{2000,j} \}$$

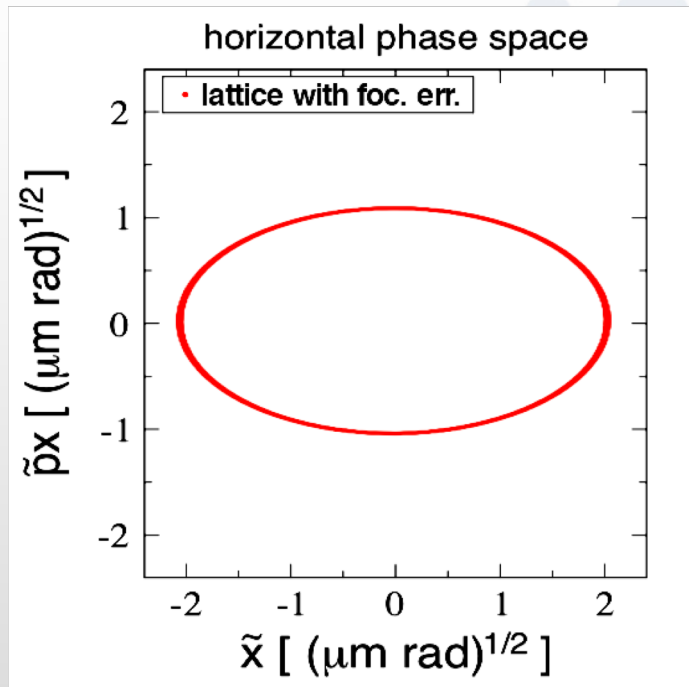
**Remark # 2:** It is not true that BPM phase advance shift depends on the quad errors between BPMs only (i.e. on  $h_{x,ij}$ ). It depends also on quad errors  $\delta K_1$  elsewhere via the RDT  $f_{2000}$

$$h_{x,ij} = -\frac{1}{4} \sum_{j < w < i} \beta_{x,w}^{(mod)} \delta K_{w,1} + O(\delta K_1^2)$$

$$\left( \frac{\Delta \beta_x}{\beta_x} \right)_j = 8 \Im \{ f_{2000,j} \} + O(|f_{2000}|^2)$$

$$\Delta \phi_{x,ij} \simeq \Delta \phi_{x,ij}^{(mod)} - 2h_{x,ij} + 4 \Re \{ f_{2000,i} - f_{2000,j} \}$$

## Measuring RDT $f_{2000}$ (TbT BPM data)



complex C-S TbT signal

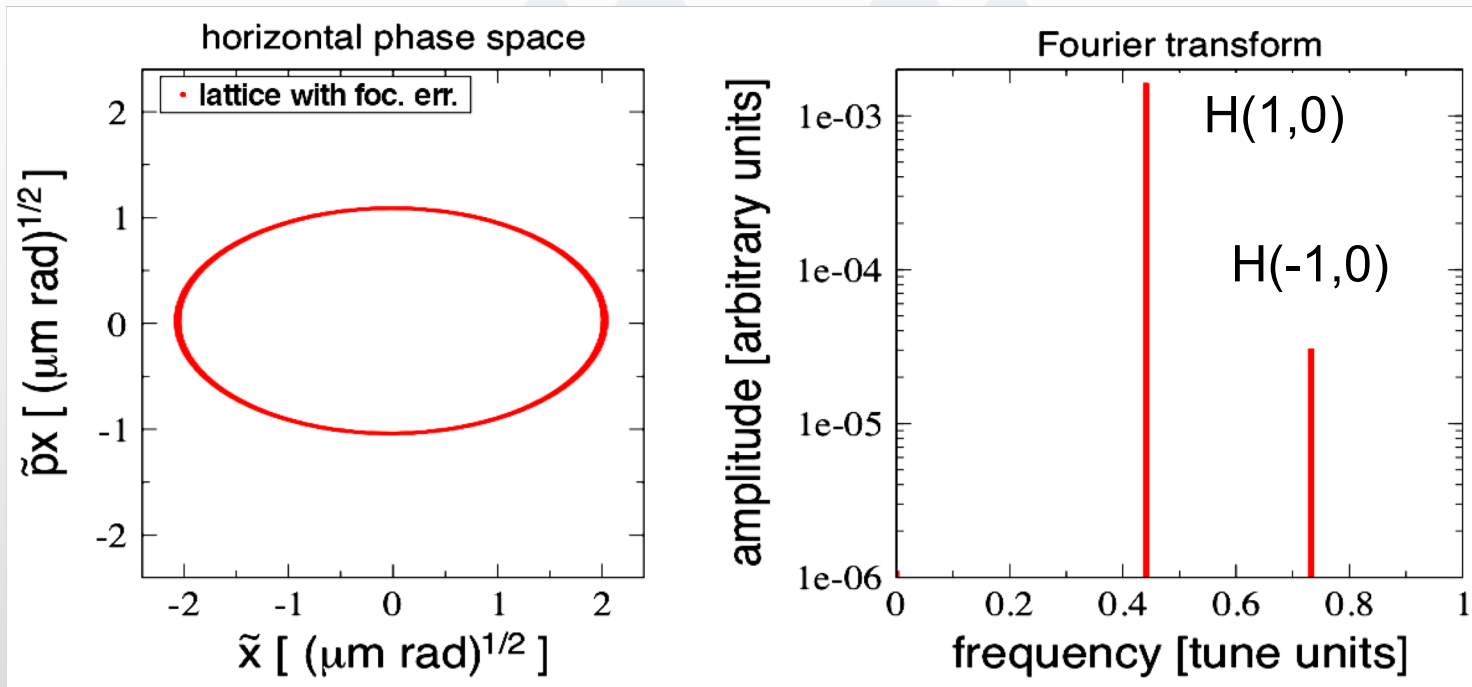
$$h_x = \tilde{x} - i\tilde{p}_x$$

$$\tilde{p}_{i,x} = (\tilde{x}_{i+1} - \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

$$\tilde{p}_{i,x} = (-\tilde{x}_{i-1} + \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

assumption: no nonlinear magnets between BPMs or “low” amplitude !!

## Measuring RDT $f_{2000}$ (TbT BPM data)



complex C-S TbT signal

$$h_x = \tilde{x} - i\tilde{p}_x$$

$$|f_{2000}| = \frac{1}{4} \operatorname{arctanh} \frac{|H_h(-1, 0)|}{|H_h(1, 0)|}$$

$$Q_{2000} = \Phi_{H_h(-1,0)} + \Phi_{H_h(1,0)} + \frac{\pi}{2}$$

## Measuring RDT $f_{2000}$ (orbit BPM data)

$$\begin{pmatrix} \vec{O}_x \\ \vec{O}_y \end{pmatrix} = \mathbf{ORM} \begin{pmatrix} \vec{\Theta}_x \\ \vec{\Theta}_y \end{pmatrix}, \quad \mathbf{ORM} = \begin{pmatrix} \mathbf{O}^{(xx)} & \mathbf{O}^{(xy)} \\ \mathbf{O}^{(yx)} & \mathbf{O}^{(yy)} \end{pmatrix}$$

$$O_{wj}^{(xx)} = \frac{\partial O_{x,j}}{\partial \Theta_{x,w}}, \quad O_{wj}^{(xy)} = \frac{\partial O_{x,j}}{\partial \Theta_{y,w}}, \quad 1 < j < N_B$$

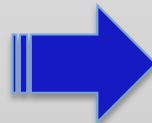
$$O_{wj}^{(yx)} = \frac{\partial O_{y,j}}{\partial \Theta_{x,w}}, \quad O_{wj}^{(yy)} = \frac{\partial O_{y,j}}{\partial \Theta_{y,w}}, \quad 1 < w < N_S$$

$$\delta \mathbf{ORM} = \mathbf{ORM}^{(\text{meas})} - \mathbf{ORM}^{(\text{ideal})}$$

pseudo-inverted (SVD)

$$\begin{pmatrix} \delta \vec{O}^{(xx)} \\ \delta \vec{O}^{(yy)} \\ \delta \vec{D}_x \end{pmatrix} = \mathbf{N} \begin{pmatrix} \delta \vec{K}_1 \\ \delta K_0 \end{pmatrix}$$

$$\begin{pmatrix} \delta \vec{O}^{(xy)} \\ \delta \vec{O}^{(yx)} \\ \delta \vec{D}_y \end{pmatrix} = \mathbf{S} \begin{pmatrix} \vec{J}_1 \\ \vec{J}_0 \end{pmatrix}$$



$$f_{2000,j} = \frac{\sum_w \beta_{x,w}^{(mod)} \delta K_{w,1} e^{2i\Delta\phi_{x,wj}^{(mod)}}}{8(1 - e^{4\pi i Q_x})}$$

## Correcting RDT $f_{2000}$ (and dispersion)

$$\begin{pmatrix} a_1 \vec{f}_{2000} \\ a_1 \vec{f}_{0020} \\ a_2 \delta \vec{D}_x \end{pmatrix}_{\text{meas}} = -\mathbf{N} \vec{K}_c$$

to be pseudo-inverted (SVD). Output is a vector containing the trim strengths of the (corrector) quadrupoles

$$f_{2000,j} = \frac{\sum_w^W \beta_{x,w}^{(mod)} \delta K_{w,1} e^{2i\Delta\phi_{x,wj}^{(mod)}}}{8(1 - e^{4\pi i Q_x})}$$

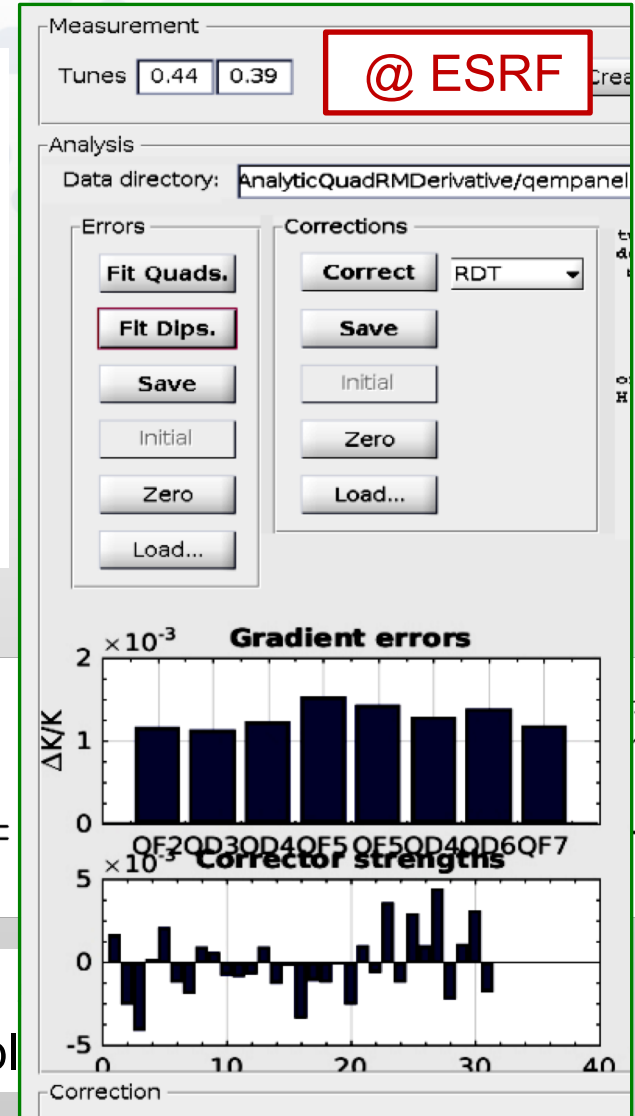
$f_{2000}$  from same formula in vertical plane

## Correcting RDT $f_{2000}$ (and dispersion)

$$\begin{pmatrix} a_1 \vec{f}_{2000} \\ a_1 \vec{f}_{0020} \\ a_2 \delta \vec{D}_x \end{pmatrix}_{\text{meas}} = -\mathbf{N} \vec{K}_c$$

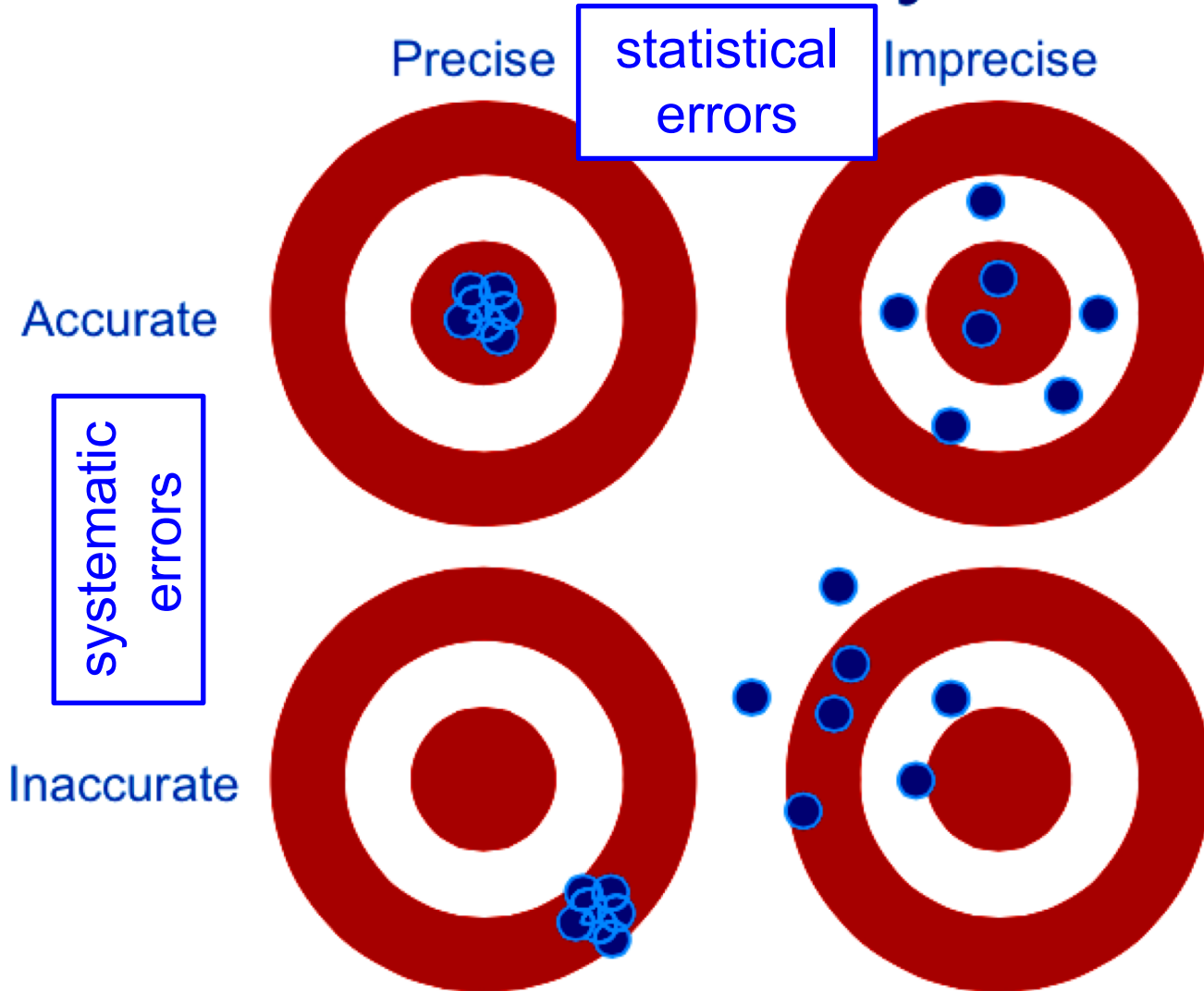
$f_{2000,j} =$

$f_{2000}$  from vertical pl





## Precision / Accuracy



## Error contribution to rms $\beta$ -beating @ ESRF (in ‰)

- Statistical errors (precision) the most significant (machine vibrations, orbit drifts [@ ESRF 15  $\mu\text{m}$  rms => 5‰], ...)
- Systematic (accuracy): SVD on ORM: 3‰ (simulations over ten sets, w/wo 10 nm BPM noise)
- Reproducibility (precision): 5‰ (H) & 2‰(V) over 5 consecutive ORM measurements (orbit corrected within 2 $\mu\text{m}$  rms)
- Lattice non-linearities polluting TbT tune line (from simulations): 1-2‰ accuracy @ lowest kick amplitude
- BPM noise and harmonic analysis of TbT data: depends on methods

Method	Mean error	$\beta_x$ -beating precision [‰]	$\beta_y$ -beating precision [‰]
TbT @ ESRF		4	4
ORM @ ESRF		6	4

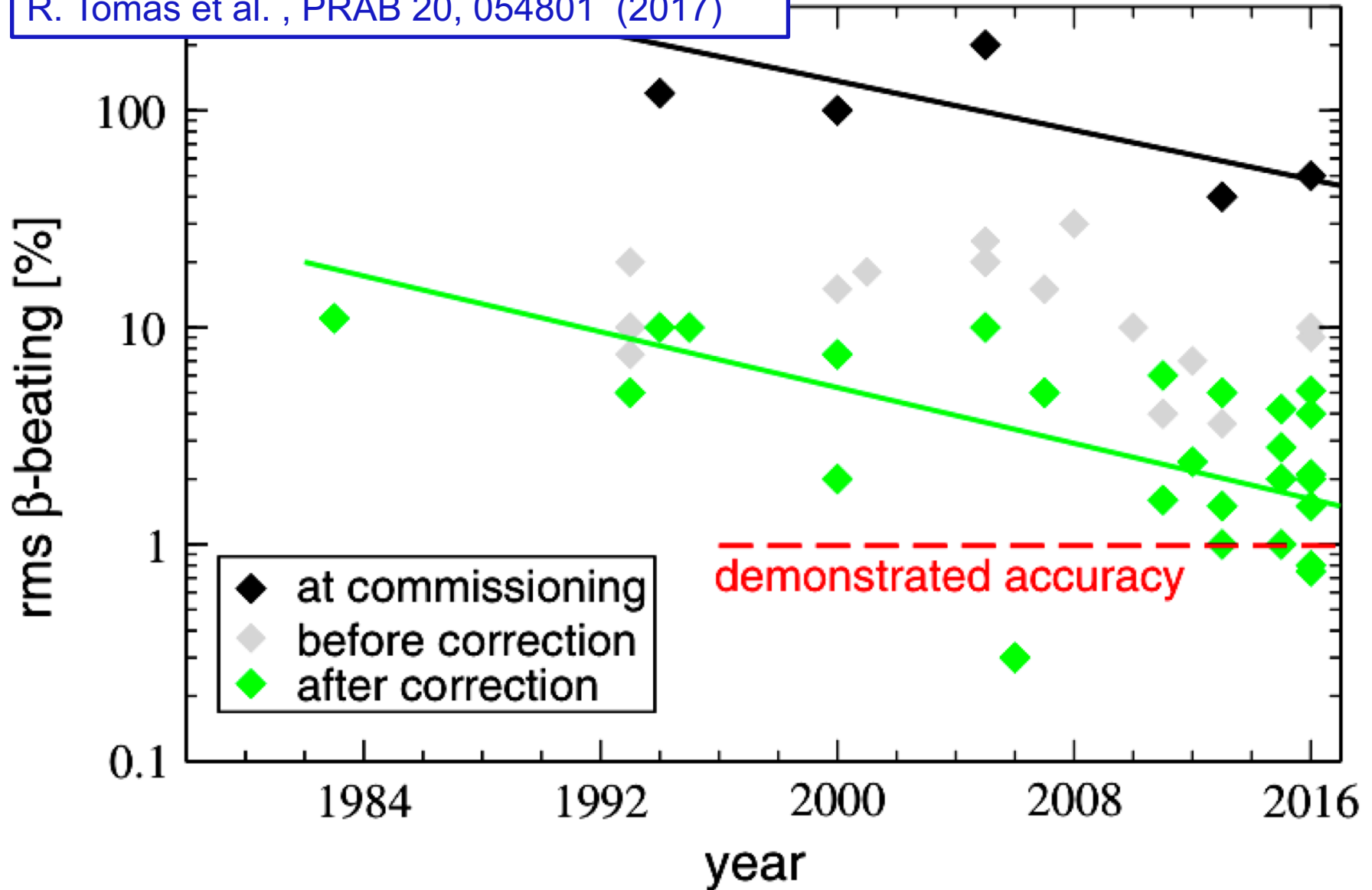
L. Malina et al. , PRAB 20, 082802 (2017)

## Error contribution to rms $\beta$ -beating @ ESRF (in ‰)

- Statistical errors (precision) the most significant (machine vibrations, orbit drifts [@ ESRF 15  $\mu\text{m}$  rms => 5‰], ...)
- **$\beta$ -beating from TbT and ORM analysis differs by ~1% rms (demonstrated accuracy @ ESRF, ALBA, ...)**
- Lattice non-linearities pending for take into (from simulations) ~2‰ accuracy @ lowest kick amplitude
- BPM noise and harmonic analysis of TbT data: depends on methods

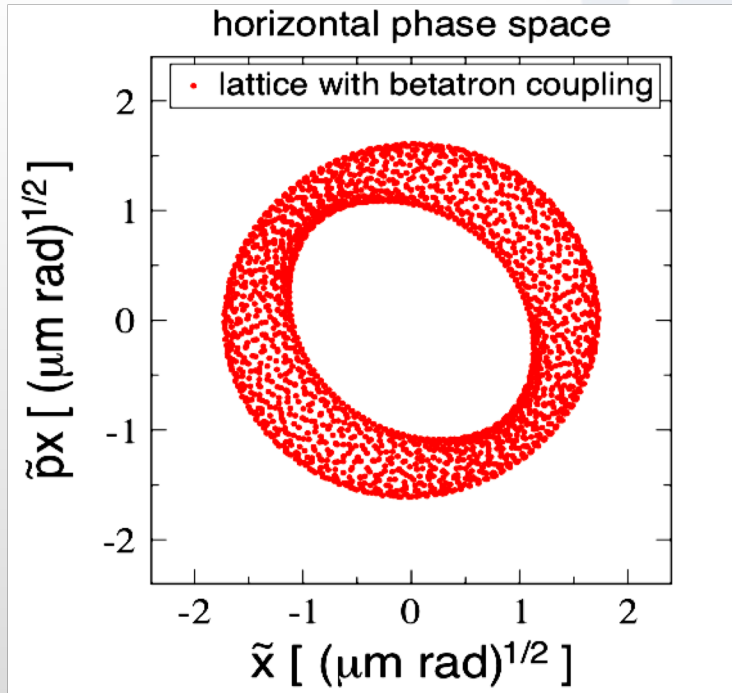
Method	Mean error	$\beta_x$ -beating precision [‰]	$\beta_y$ -beating precision [‰]
TbT @ ESRF		4	4
ORM @ ESRF		6	4

R. Tomas et al. , PRAB 20, 054801 (2017)



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## Measuring RDTs $f_{1001}$ & $f_{1010}$ (TbT BPM data)



complex C-S TbT signal

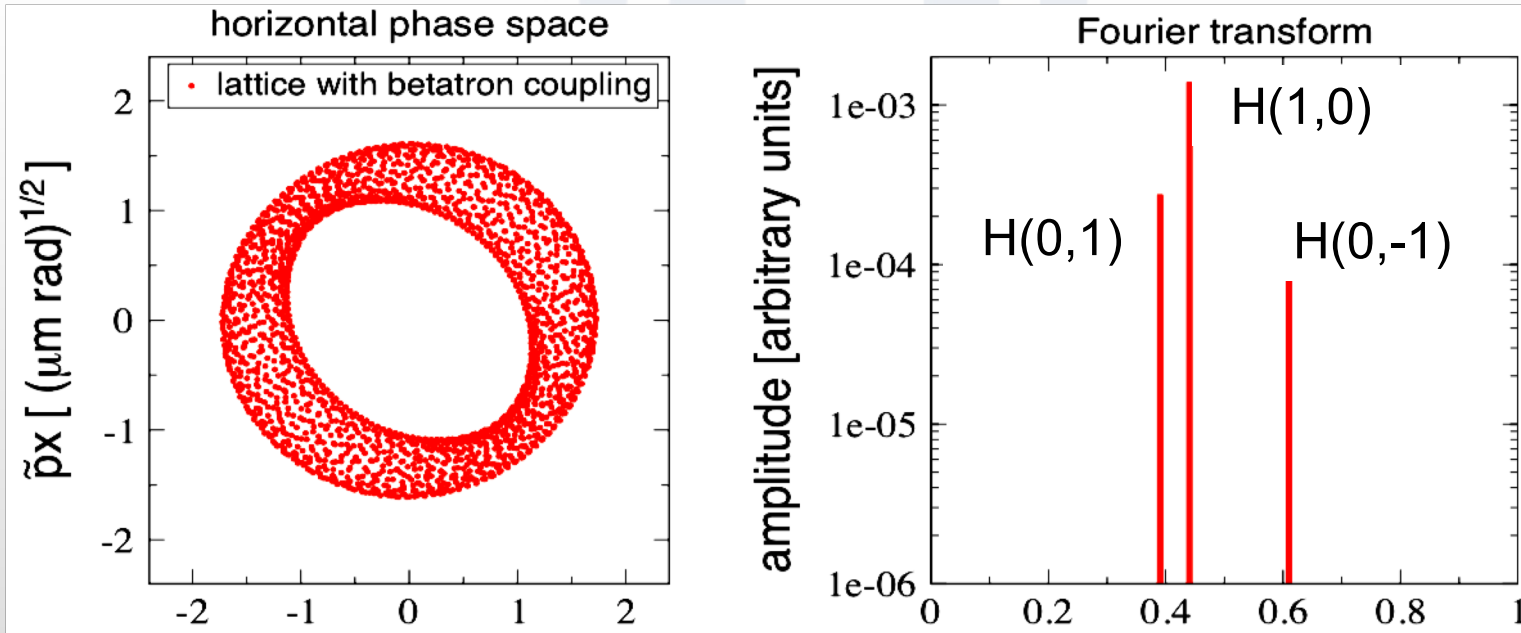
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$$\tilde{p}_{i,x} = (\tilde{x}_{i+1} - \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

$$\tilde{p}_{i,x} = (-\tilde{x}_{i-1} + \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

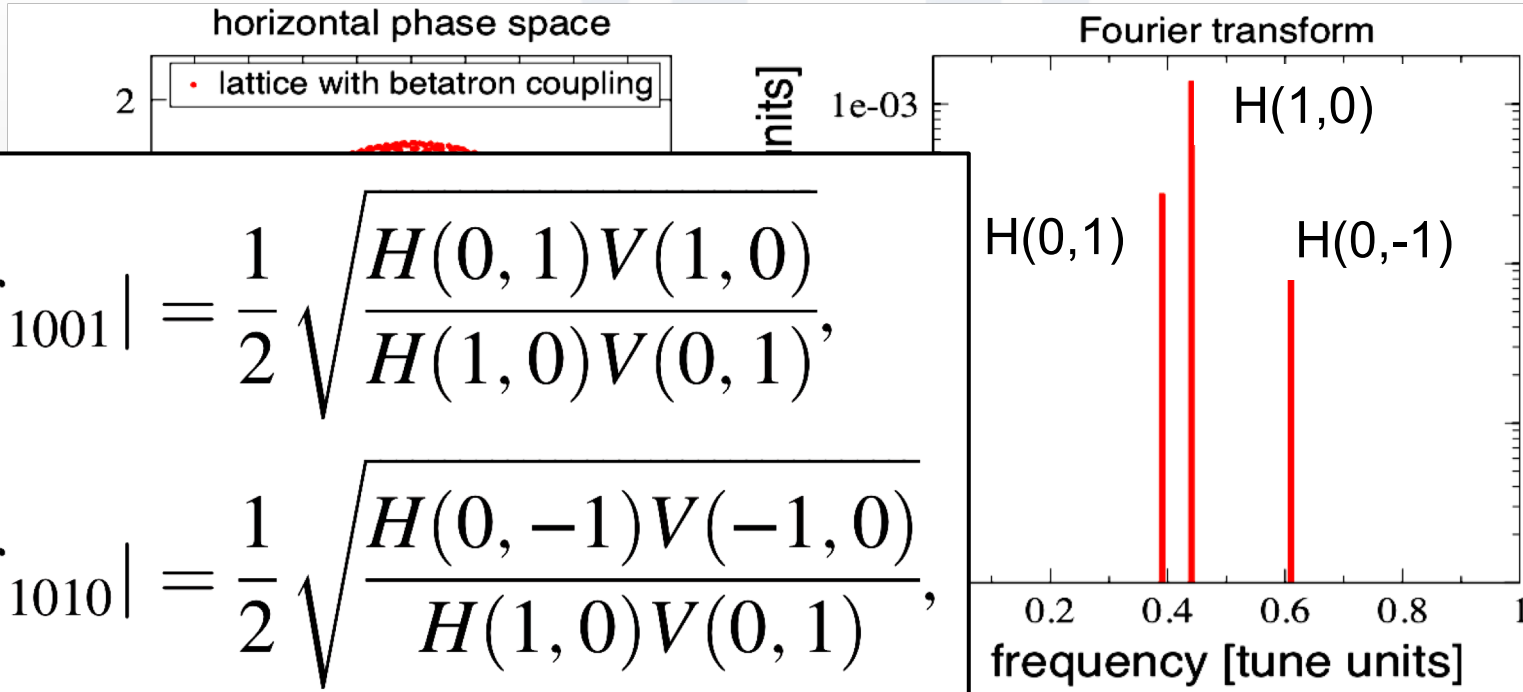
assumption: no nonlinear magnets between BPMs or “low” amplitude !!

## Measuring RDTs $f_{1001}$ & $f_{1010}$ (TbT BPM data)



$jklm$	resonance	H-line	V-line	$ a_{jklm} $	$\phi_{jklm}^a$
0110	(1,-1)		(1,0)	$2 f_{0110} (2I_x)^{1/2}$	$\phi_{0110}^f + \psi_{x,0} - \frac{\pi}{2}$
1001	(1,-1)	(0,1)		$2 f_{1001} (2I_y)^{1/2}$	$\phi_{1001}^f + \psi_{y,0} - \frac{\pi}{2}$
1010	(1,1)	(0,-1)	(-1,0)	H: $2 f_{1010} (2I_y)^{1/2}$	H: $\phi_{1010}^f - \psi_{y,0} - \frac{\pi}{2}$
				V: $2 f_{1010} (2I_x)^{1/2}$	V: $\phi_{1010}^f - \psi_{x,0} - \frac{\pi}{2}$

## Measuring RDTs $f_{1001}$ & $f_{1010}$ (TbT BPM data)



$$|f_{1001}| = \frac{1}{2} \sqrt{\frac{H(0,1)V(1,0)}{H(1,0)V(0,1)}}$$

$$|f_{1010}| = \frac{1}{2} \sqrt{\frac{H(0,-1)V(-1,0)}{H(1,0)V(0,1)}}$$

$$q_{1001} = \frac{1}{2} \left( \phi_{H(0,1)} + \phi_{H(1,0)} - \phi_{V(1,0)} - \phi_{V(0,1)} \right)$$

$$q_{1010} = \frac{1}{2} \left( \phi_{H(0,-1)} + \phi_{H(1,0)} + \phi_{V(-1,0)} + \phi_{V(0,1)} + \pi \right)$$



## Measuring RDTs $f_{1001}$ & $f_{1010}$ (orbit BPM data)

$$\begin{pmatrix} \vec{O}_x \\ \vec{O}_y \end{pmatrix} = \mathbf{ORM} \begin{pmatrix} \vec{\Theta}_x \\ \vec{\Theta}_y \end{pmatrix}, \quad \mathbf{ORM} = \begin{pmatrix} \mathbf{O}^{(xx)} & \mathbf{O}^{(xy)} \\ \mathbf{O}^{(yx)} & \mathbf{O}^{(yy)} \end{pmatrix}$$

$$O_{wj}^{(xx)} = \frac{\partial O_{x,j}}{\partial \Theta_{x,w}}, \quad O_{wj}^{(xy)} = \frac{\partial O_{x,j}}{\partial \Theta_{y,w}}, \quad 1 < j < N_B$$


$$O_{wj}^{(yx)} = \frac{\partial O_{y,j}}{\partial \Theta_{x,w}}, \quad O_{wj}^{(yy)} = \frac{\partial O_{y,j}}{\partial \Theta_{y,w}}, \quad 1 < w < N_S$$

$$\delta \mathbf{ORM} = \mathbf{ORM}^{(\text{meas})} - \mathbf{ORM}^{(\text{ideal})}$$

pseudo-inverted (SVD)

$$\begin{pmatrix} \delta \vec{O}^{(xx)} \\ \delta \vec{O}^{(yy)} \\ \delta \vec{D}_x \end{pmatrix} = \mathbf{N} \begin{pmatrix} \delta \vec{K}_1 \\ \delta \vec{K}_0 \end{pmatrix}$$

$$\begin{pmatrix} \delta \vec{O}^{(xy)} \\ \delta \vec{O}^{(yx)} \\ \delta \vec{D}_y \end{pmatrix} = \mathbf{S} \begin{pmatrix} \vec{J}_1 \\ \vec{J}_0 \end{pmatrix}$$



$$f_{\begin{matrix} 1001 \\ 1010 \end{matrix}}, j = \frac{\sum_w J_{w,1} \sqrt{\beta_{w,x} \beta_{w,y}} e^{i(\Delta\phi_{x,wj} \mp \Delta\phi_{y,wj})}}{4(1 - e^{2\pi i(Q_u \mp Q_v)})}$$

## Correcting RDTs $f_{1001}$ & $f_{1010}$ (& vertical dispersion)

$$\begin{pmatrix} a_1 \vec{f}_{1001} \\ a_1 \vec{f}_{1010} \\ a_2 \vec{D}_y \end{pmatrix}_{\text{meas}} = -\mathbf{M} \vec{J}_c$$

to be pseudo-inverted (SVD). Output is a vector containing the trim strengths of the corrector skew quadrupoles

$$f_{\begin{matrix} 1001 \\ 1010 \end{matrix}, j} = \frac{\sum_w^W J_{w,1} \sqrt{\beta_{w,x} \beta_{w,y}} e^{i(\Delta\phi_{x,wj} \mp \Delta\phi_{y,wj})}}{4(1 - e^{2\pi i(Q_u \mp Q_v)})}$$

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$$\begin{pmatrix} a_1 \vec{f}_{1001} \\ a_1 \vec{f}_{1010} \\ a_2 \vec{D}_y \end{pmatrix}_{\text{meas}} = -\mathbf{M} \vec{J}_c$$

Analysis  
Data directory: /mntdirect/\_machfs/luuzzo

@ ESRF

Errors

Fit Quads. Disp. 0.0

Fit Dips.

Save

Zero

Load...

Corrections

Retune

Correct RDT

Save

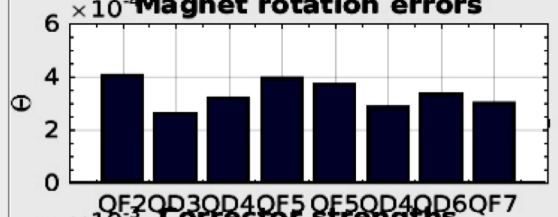
Initial Disp. 0.4

Zero

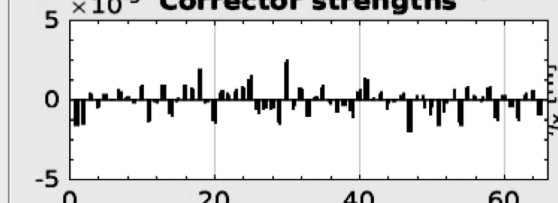
Load...

Display  
ID25 spot

**Magnet rotation errors**



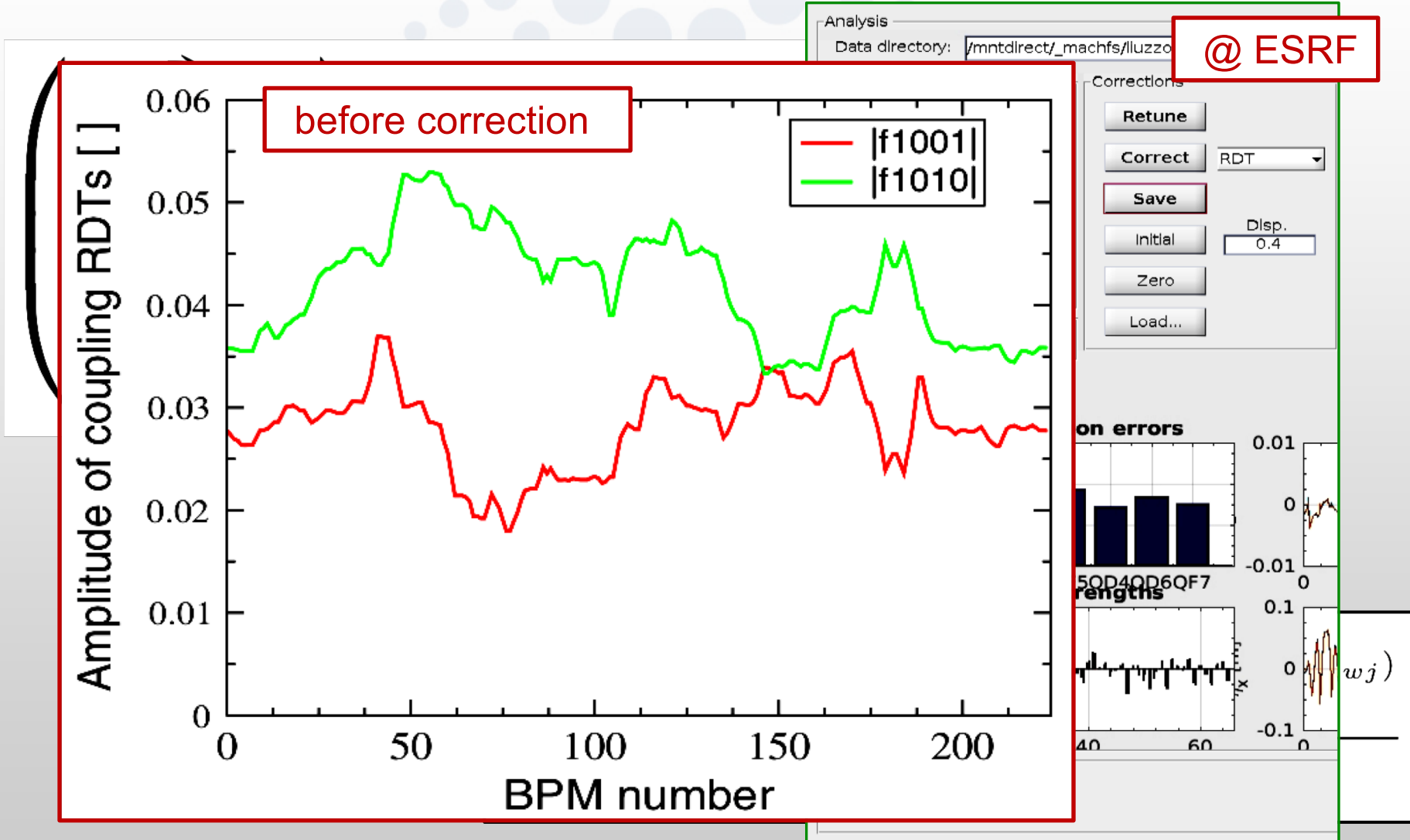
**Corrector strengths**



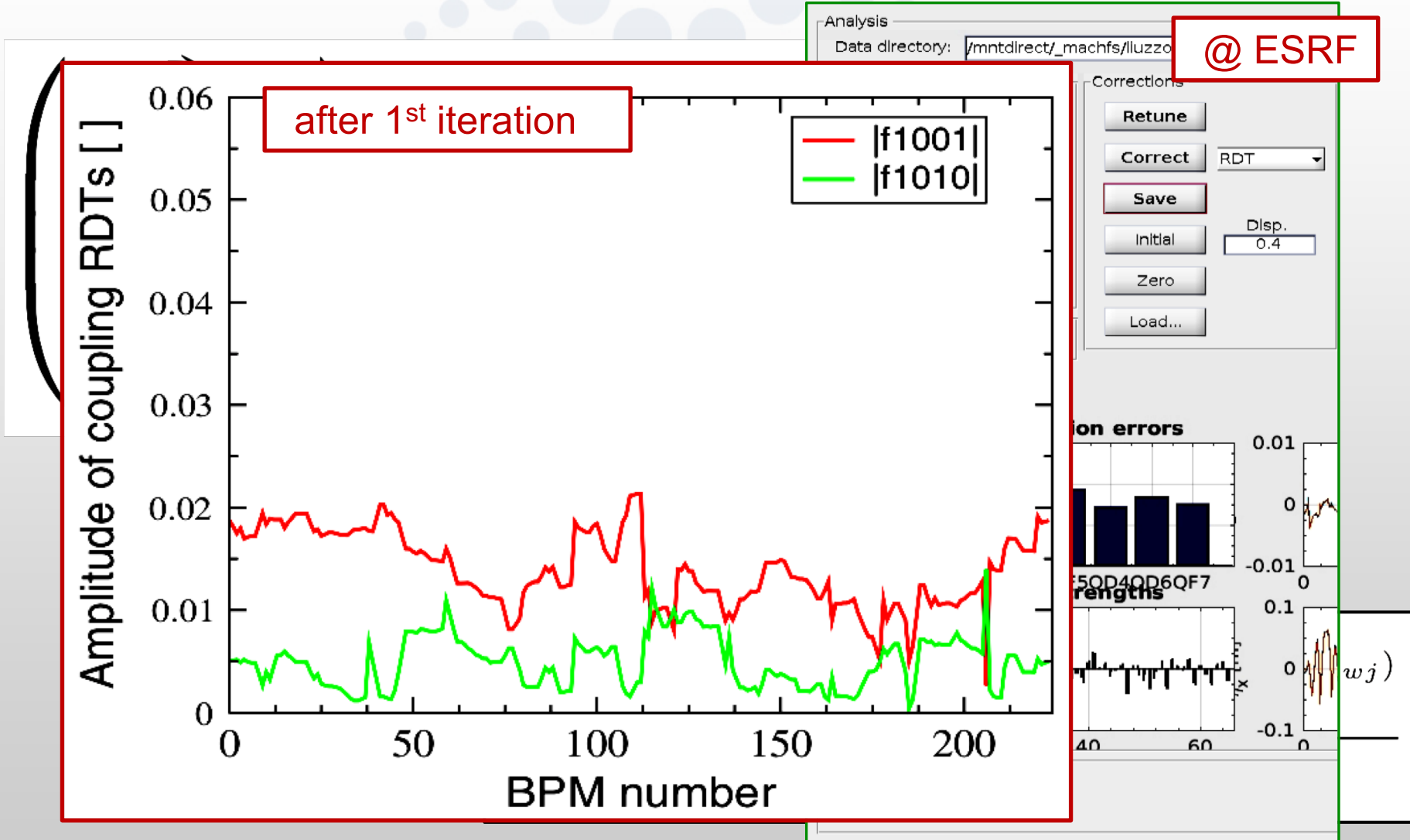
Correction  
Apply correction

$$f_{\begin{matrix} 1001 \\ 1010 \end{matrix}, j} = \frac{W}{w} \sum J_j$$

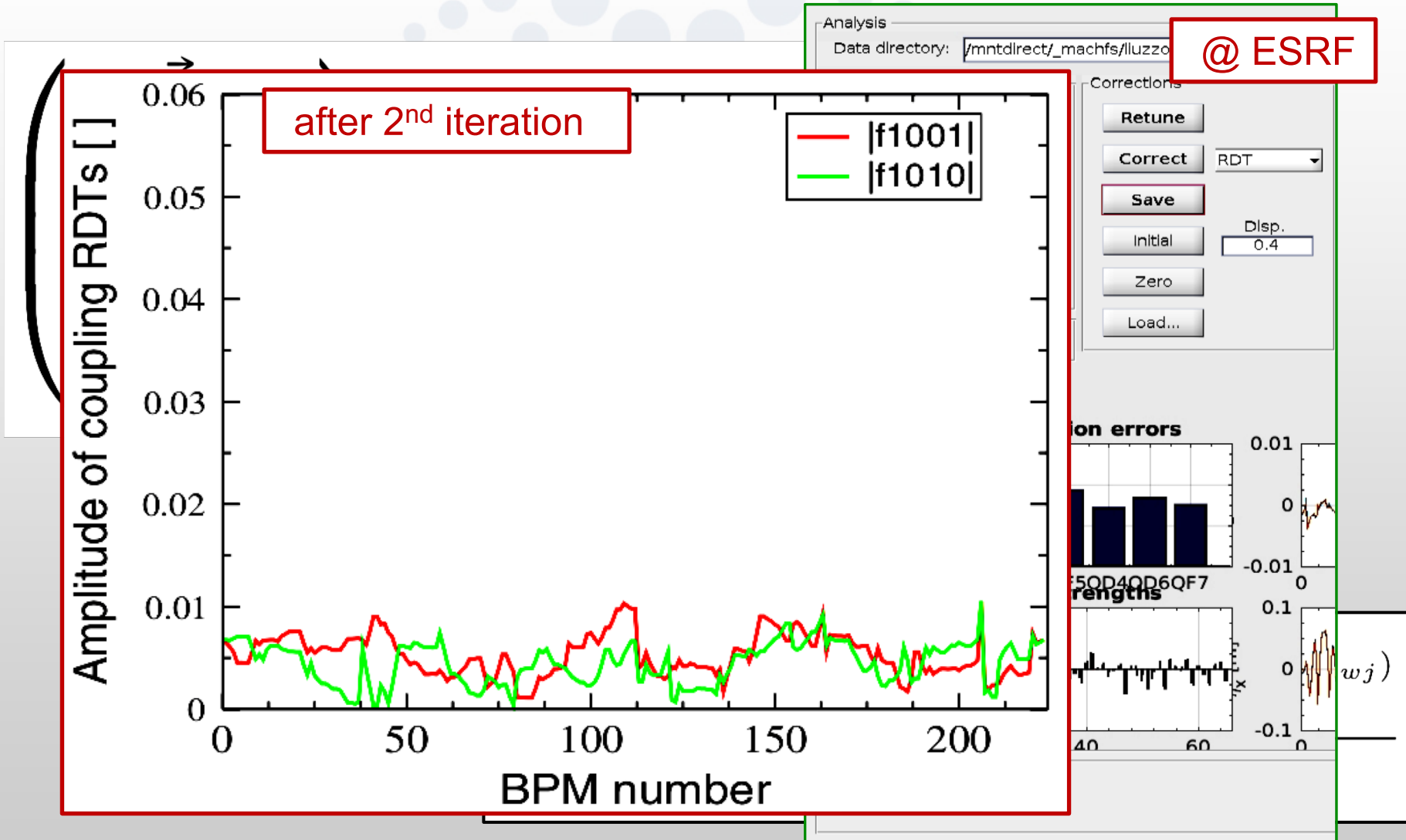
## Correcting RDTs $f_{1001}$ & $f_{1010}$ (& vertical dispersion)



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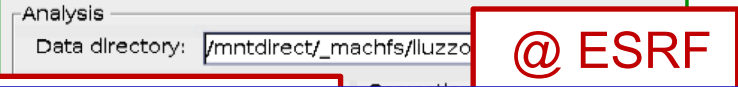
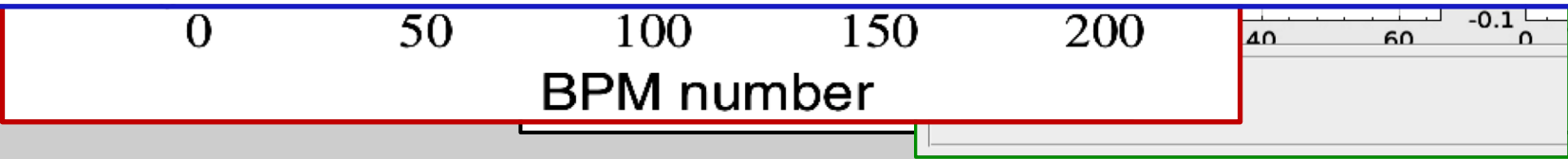


TABLE I. Summary table of the first correction with RDTs of January 16, 2010. The corresponding horizontal emittance is  $\epsilon_x \simeq \mathbb{E}_x \simeq \mathcal{E}_u \simeq 4$  nm. Beta beat refers to the peak value.

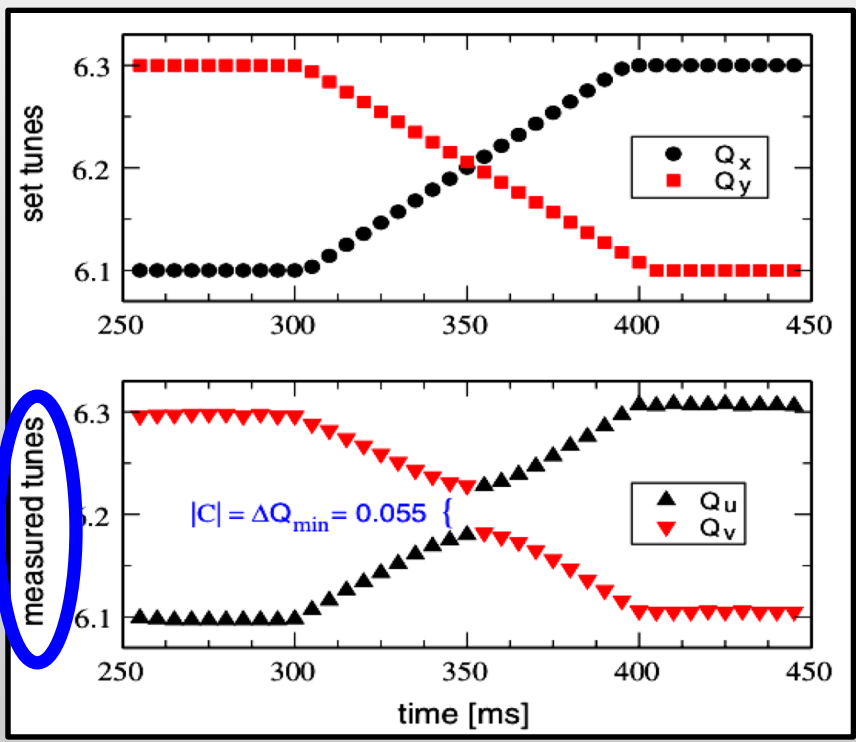
Condition	$\bar{\epsilon}_y \pm \delta\epsilon_y$ [pm]	$\beta$ beat [%]
With 2009 correction	$46 \pm 18$	5
All correctors OFF	$237 \pm 122$	50
After 1st correction	$23.6 \pm 6.3$	8
After 2nd correction	$11.5 \pm 4.3$	5



## Hadron Vs lepton machines

~ hadrons

$$\Delta Q_{\min} = \left| \frac{1}{2\pi} \oint ds j(s) \sqrt{\beta_x \beta_y} e^{-i(\phi_x - \phi_y) + i(\hat{Q}_x - \hat{Q}_y)s/R} \right|,$$





## Hadron Vs lepton machines

$$Q_x - Q_y$$

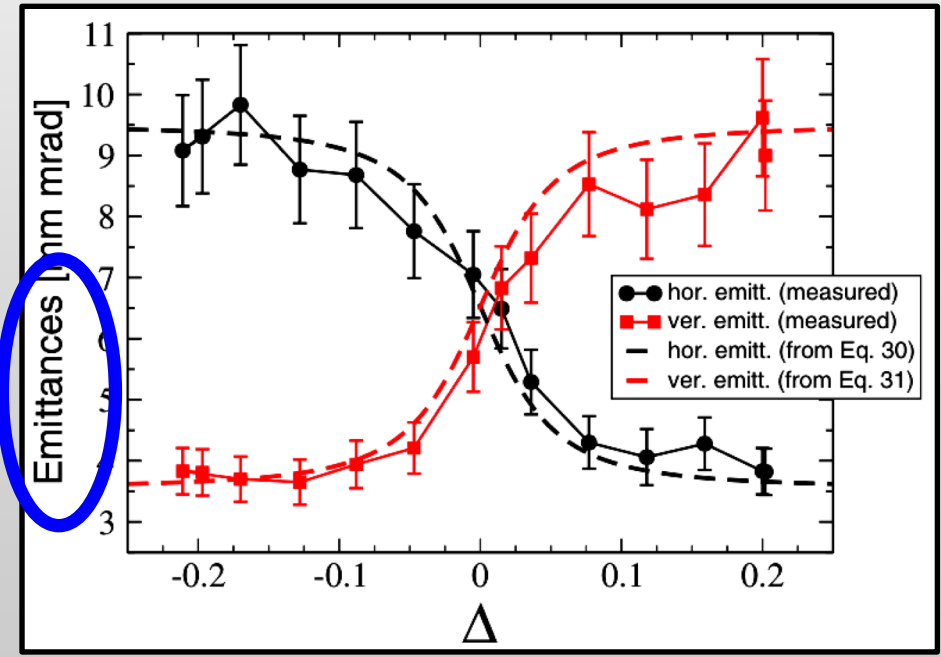
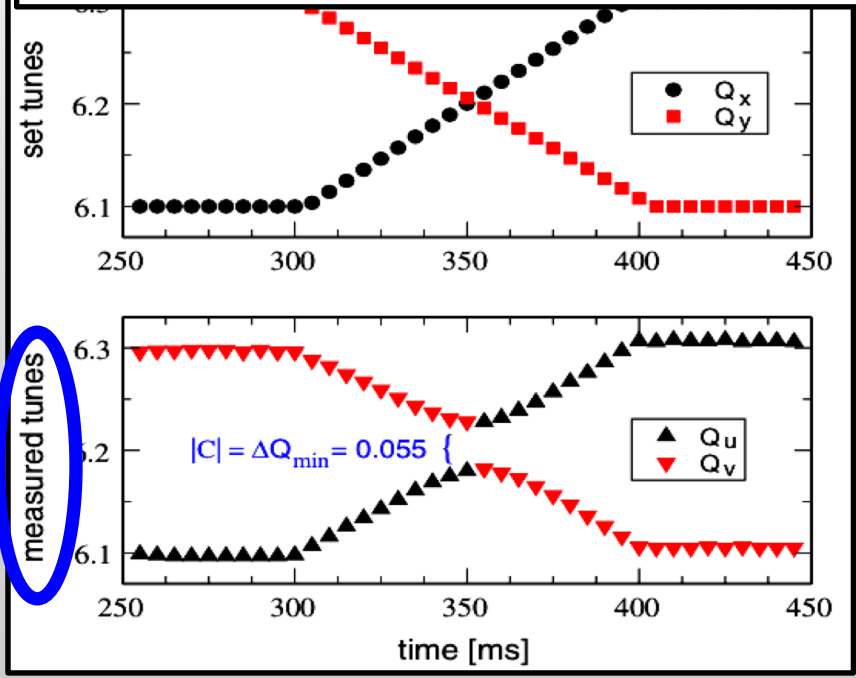
$$\Delta Q_{\min} = \left| \frac{1}{2\pi} \oint ds j(s) \sqrt{\beta_x \beta_y} e^{-i(\phi_x - \phi_y) + i(\hat{Q}_x - \hat{Q}_y)s/R} \right|,$$

~ hadrons

~ leptons

$\varepsilon_y/\varepsilon_x \approx 1$  fully coupled

$\varepsilon_y/\varepsilon_x \approx 1\%$  ultra-low coupling



## Hadron Vs lepton machines

$$\Delta Q_{\min} = \left| \frac{1}{2\pi} \oint ds j(s) \sqrt{\beta_x \beta_y} e^{-i(\phi_x - \phi_y) + i(\hat{Q}_x - \hat{Q}_y)s/R} \right|, \quad \sim \text{hadrons}$$

$\varepsilon_y/\varepsilon_x \approx 1$  fully coupled       $\varepsilon_y/\varepsilon_x \approx 1\%$  ultra-low coupling       $\sim \text{leptons}$

$$Q_x \approx Q_y \quad \Rightarrow \quad |f_{1010}| \ll |f_{1001}|$$

$$\Delta Q_{\min} \approx \left| 4(\hat{Q}_x - \hat{Q}_y) \overline{f_{1001}} e^{-i(\phi_x - \phi_y)} \right| \lesssim 4 |\hat{Q}_x - \hat{Q}_y| \overline{|f_{1001}|}$$

**round beams usually ( $\varepsilon_y/\varepsilon_x \approx 1$ ) from injection even with ultra-low coupling ( $\Delta Q_{\min}$  @ LHC  $\sim 2 \times 10^{-4}$ )**

## Hadron Vs lepton machines

$$Q_x - Q_y$$

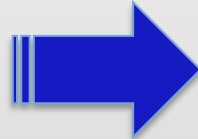
$$\Delta Q_{\min} = \left| \frac{1}{2\pi} \oint ds j(s) \sqrt{\beta_x \beta_y} e^{-i(\phi_x - \phi_y) + i(\hat{Q}_x - \hat{Q}_y)s/R} \right|,$$

~ hadrons

~ leptons

$\varepsilon_y/\varepsilon_x \approx 1$  fully coupled       $\varepsilon_y/\varepsilon_x \approx 1\%$  ultra-low coupling

$$Q_x \gg Q_y$$



$$|f_{1010}| \approx |f_{1001}|$$

$$\mathcal{E}_x = \mathcal{C}^2 \mathcal{E}_u + [S_-^2 + S_+^2 - 2S_- S_+ \cos(q_+ + q_-)] \mathcal{E}_v$$

$$\mathcal{E}_y = \mathcal{C}^2 \mathcal{E}_v + [S_-^2 + S_+^2 - 2S_- S_+ \cos(q_+ - q_-)] \mathcal{E}_u$$

$$\mathcal{P} = \sqrt{-|f_{1001}|^2 + |f_{1010}|^2}$$

$$\mathcal{C} = \cosh(2\mathcal{P})$$

$$S_{\pm} = \frac{\sinh(2\mathcal{P})}{\mathcal{P}} |f_{1001}|$$



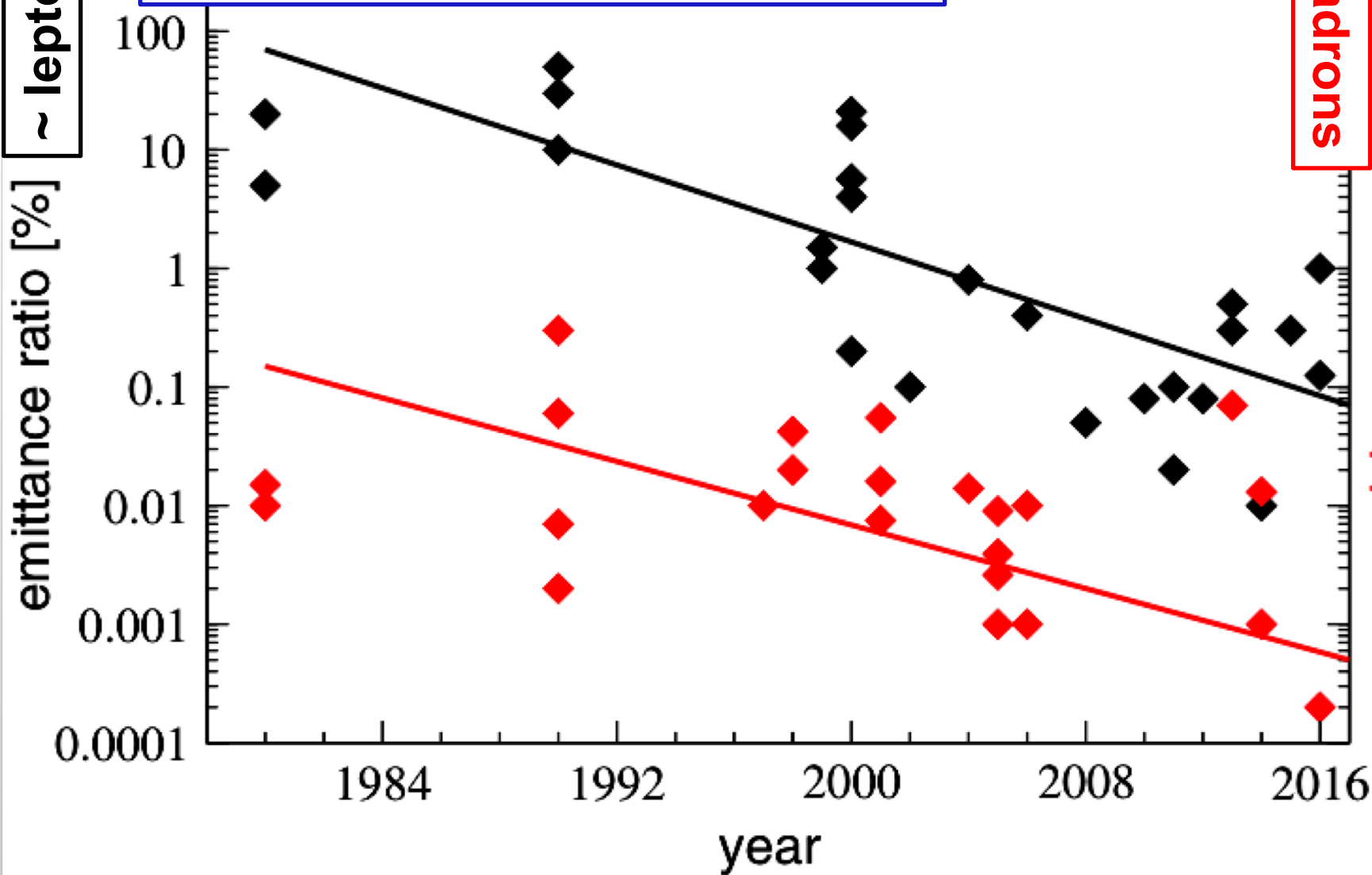
# betatron coupling

R. Tomas et al. , PRAB 20, 054801 (2017)

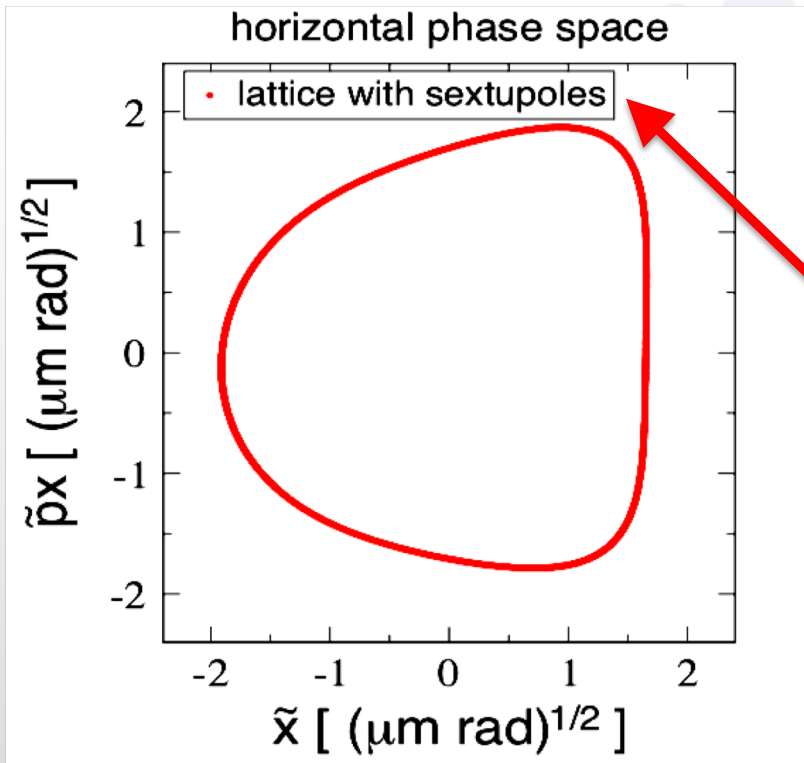
~ leptons

~ hadrons

closest tune approach



- Resonance Driving Terms Introductory (15')
- Linear optics errors (10')
  1. RDTs Vs beta-beating and phase advance error
  2. RDTs measurements & correction
  3. Accuracy and precision analysis
- Betatron coupling (10')
  1. RDTs measurements & correction
  2. Hadron Vs lepton machines
- **Nonlinear lattice error (model) (15')**
  1. Localization & detection of nonlinearities via RDTs
  2. RDTs Vs chromatic functions and orbit feed-downs



**1<sup>st</sup> caveat: measuring nonlinear RDTs from complex C-S signal is affected by a systematic error in the reconstruction of  $p_x$**

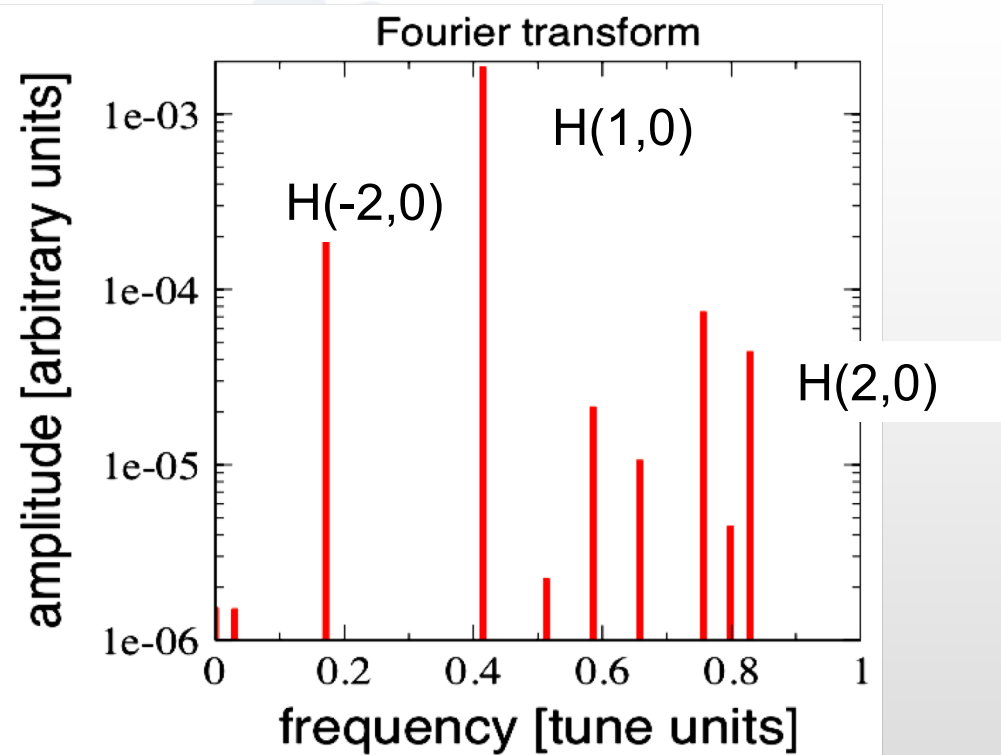
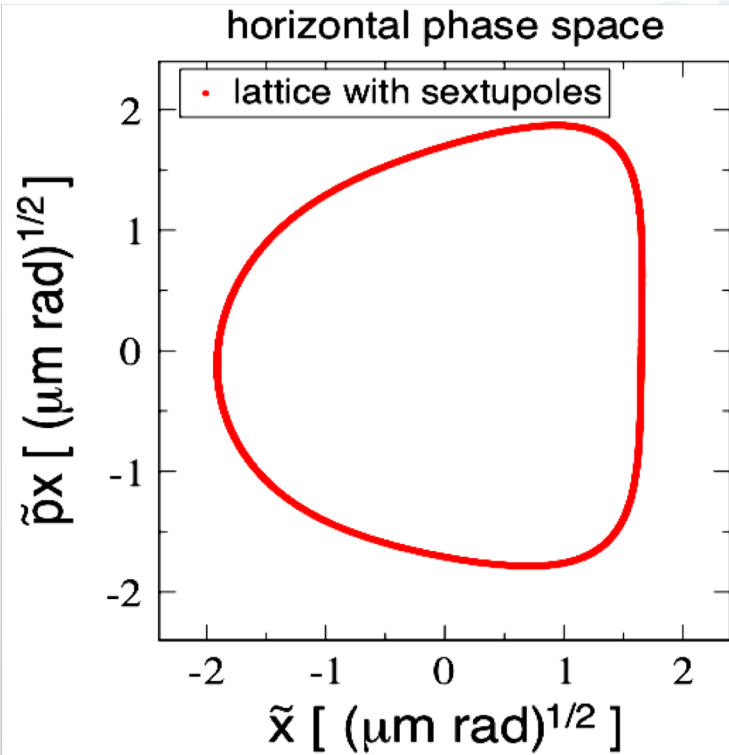
complex C-S TbT signal

$$h_x = \tilde{x} - i\tilde{p}_x$$

$$\tilde{p}_{i,x} = (\tilde{x}_{i+1} - \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

$$\tilde{p}_{i,x} = (-\tilde{x}_{i-1} + \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

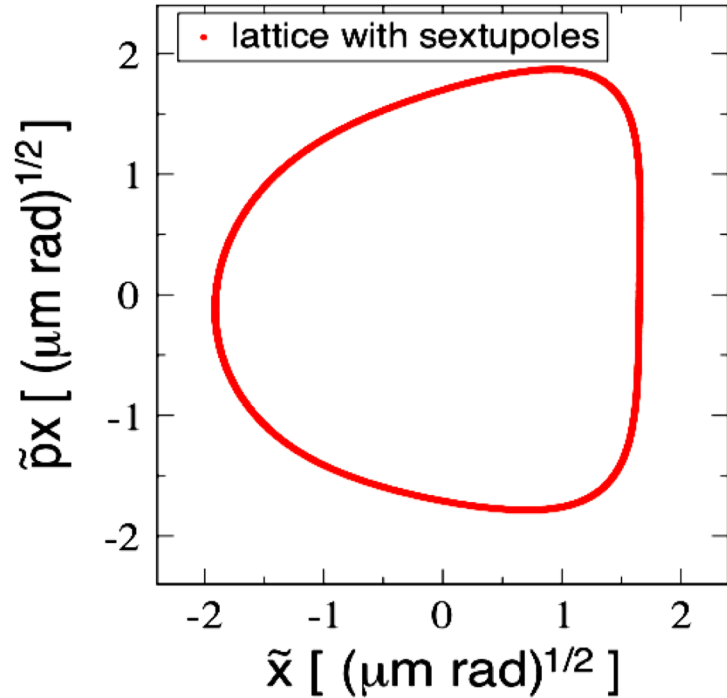
assumption: no nonlinear magnets between BPMs or “low” amplitude !!



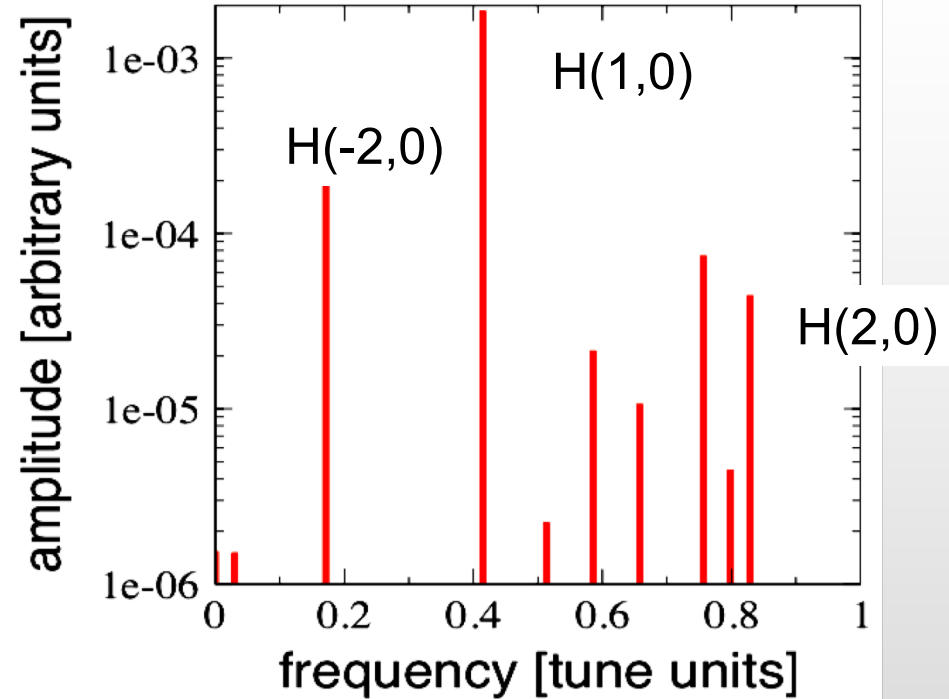
$jklm$	resonance	H-line	V-line	$ a_{jklm} $	$\phi_{jklm}^a$
1200	(1,0)	(2,0)		$2 f_{1200} (2I_x)$	$\phi_{1200}^f + 2\psi_{x,0} - \frac{\pi}{2}$
2100	(1,0)	(0,0)		$4 f_{2100} (2I_x)$	$\phi_{2100}^f$
3000	(3,0)	(-2,0)		$6 f_{3000} (2I_x)$	$\phi_{3000}^f - 2\psi_{x,0} - \frac{\pi}{2}$

let's focus on this

horizontal phase space



Fourier transform



$$|f_{3000}| = \frac{H(-2,0)}{6H(1,0)^2}$$

**2<sup>nd</sup> caveat: measured RDTs affected by BPM calibration error (if unknown)**

$$q_{1001} = \phi_{H(-2,0)} + 2\phi_{H(1,0)} + \frac{\pi}{2}$$



$$h_{w,3000} e^{-i3\phi_x^w} = f_{3000}^{(w)} e^{-i3\Delta\phi_x^{w,w-1}} - f_{3000}^{(w-1)}$$

$$h_{w,3000} = K_{w,2} \beta_{w,x}^{3/2} / 16$$

**The RDT amplitude between two BPMs (w-1) & (w) changes only if there is at least one corresponding magnet (sextupole in the case of  $f_{3000}$ ) within the two BPMs => This can be used to localize and calibrate magnets !!!**

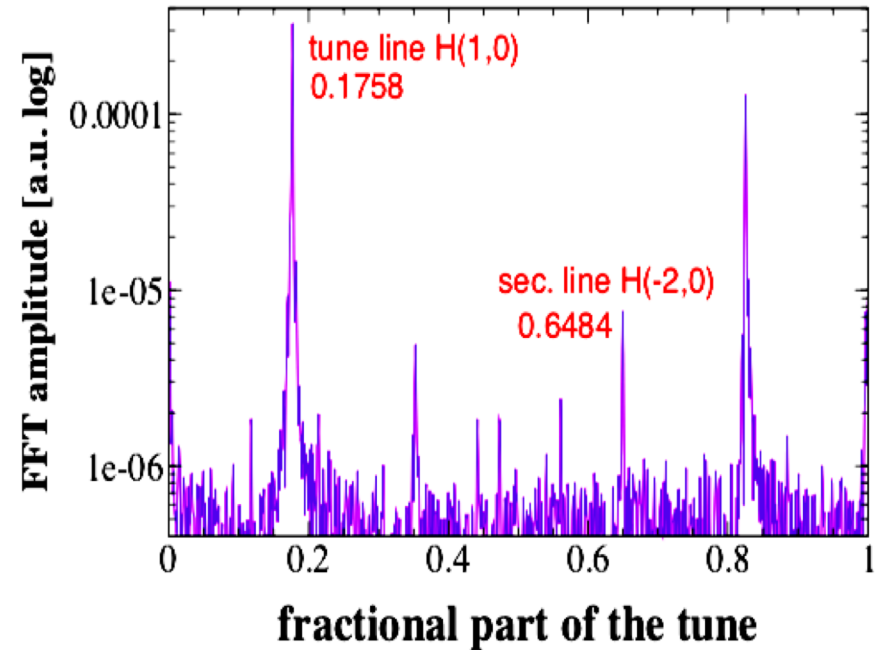
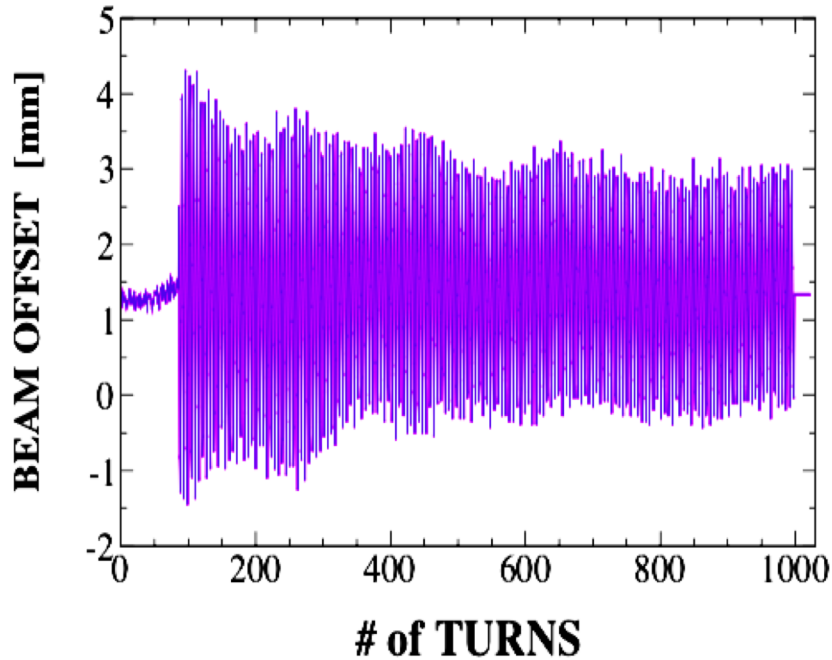
$$|f_{3000}| = \frac{H(-2,0)}{6H(1,0)^2}$$

$$q_{1001} = \phi_{H(-2,0)} + 2\phi_{H(1,0)} + \frac{\pi}{2}$$

## $f_{3000}$ and sextupole strength measurement @ SPS

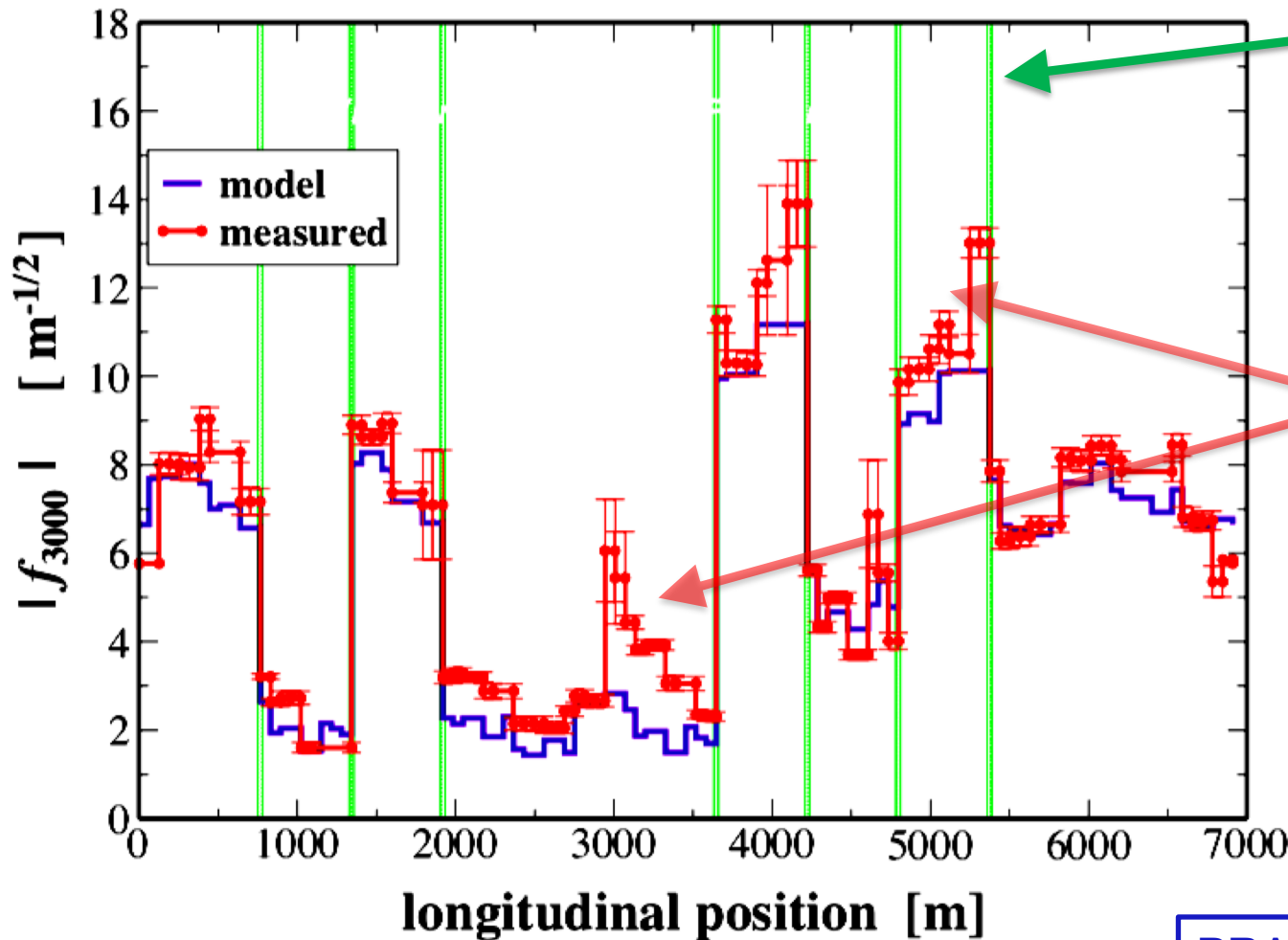
PRAB 10, 074001 (2007)

SPS turn-by-turn BPM data



**3<sup>rd</sup> caveat: sextupole (and higher-order) spectral lines are close to the background noise for operational setting. @ SPS and ESRF sextupoles were modified to enhance them.**

## $f_{3000}$ and sextupole strength measurement @ SPS

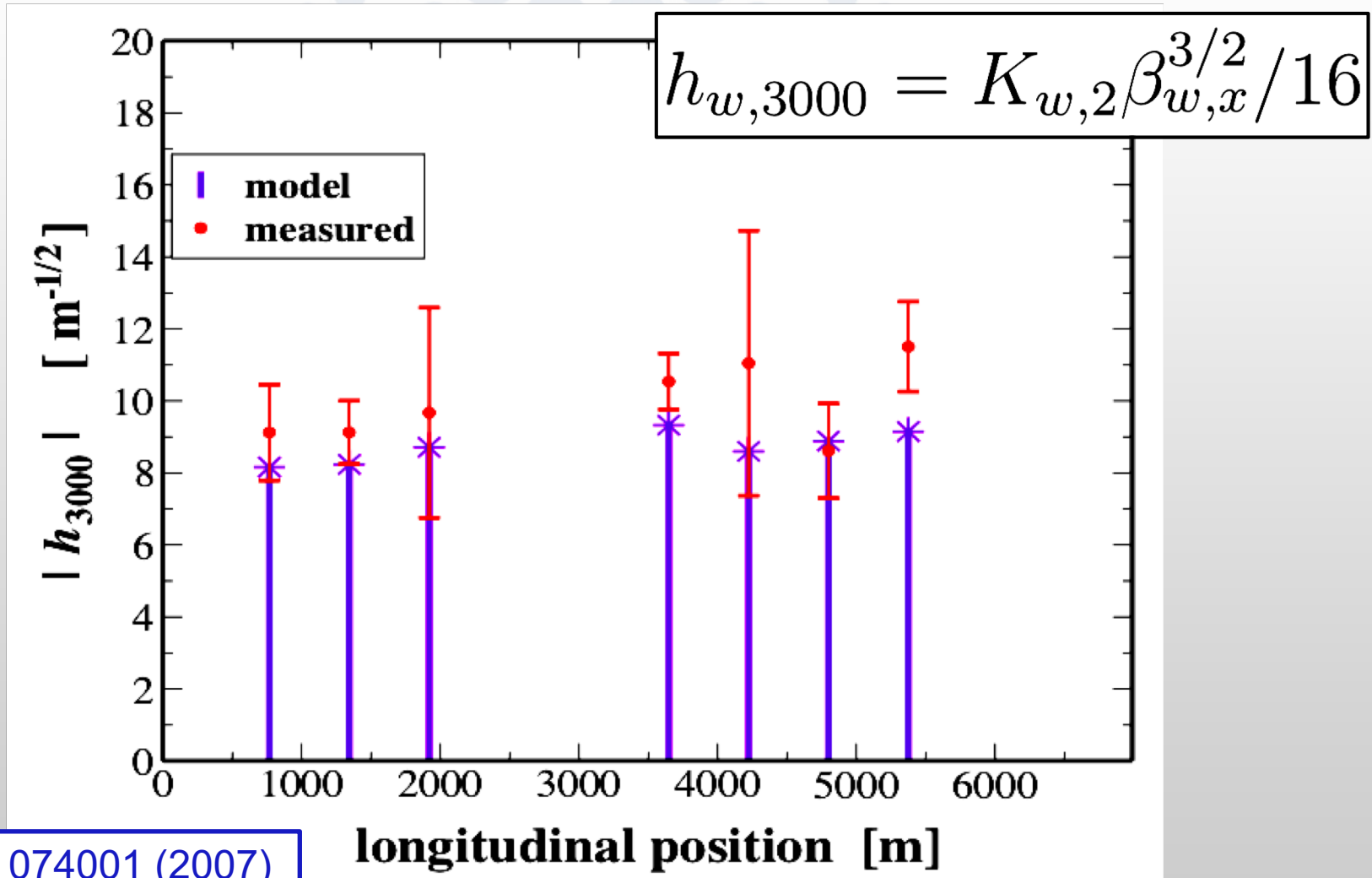


7 strong slow-extraction sextupoles

artificial jumps from wrong  $p_x$  reconstruction due to (weak) chromatic sextupoles

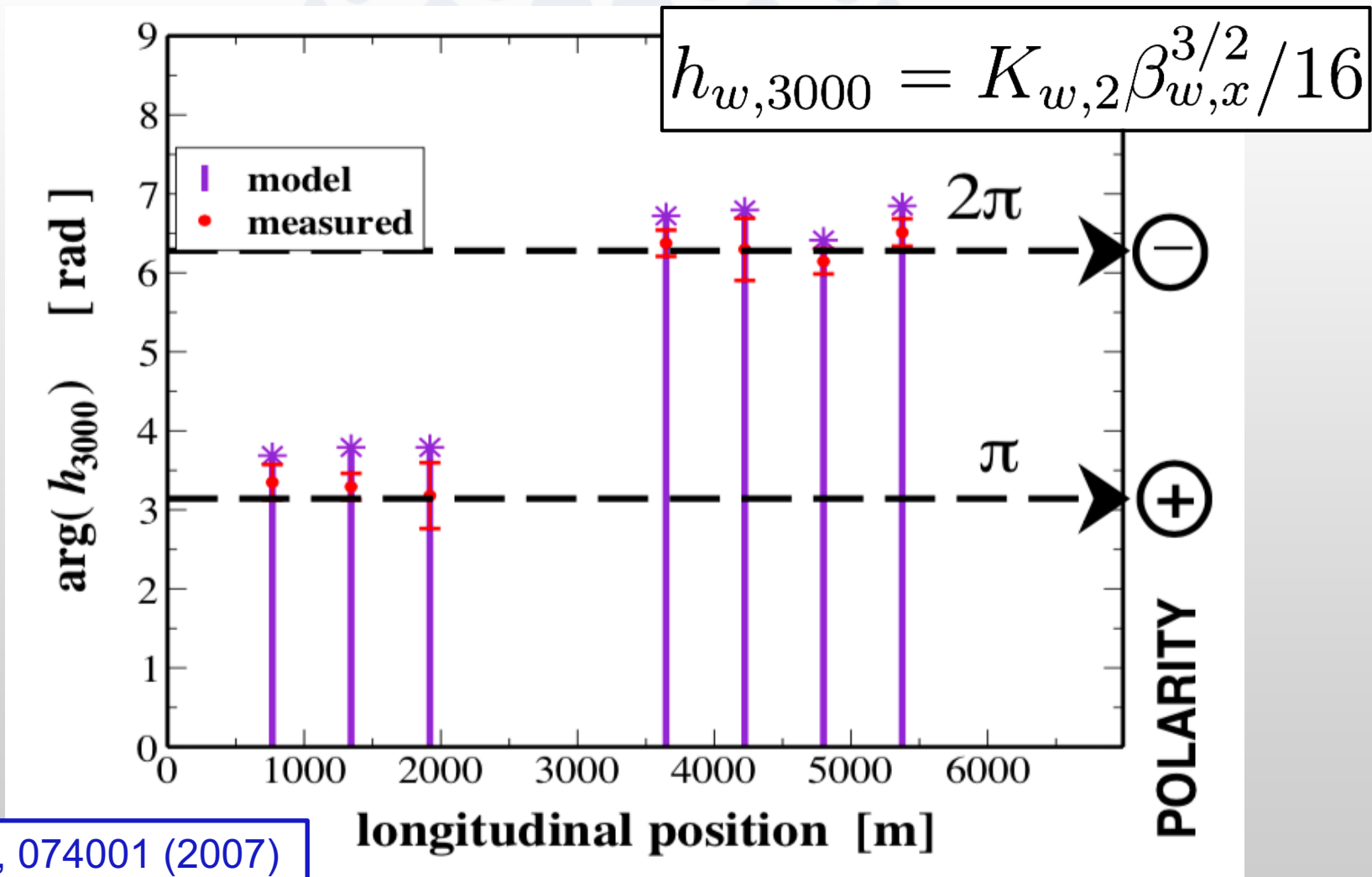
PRAB 10, 074001 (2007)

## $f_{3000}$ and sextupole strength measurement @ SPS



PRAB 10, 074001 (2007)

## $f_{3000}$ and sextupole strength measurement @ SPS



PRAB 10, 074001 (2007)

## Caveats & cures when measuring nonlinear RDTs

**1. measuring nonlinear RDTs from complex C-S signal is affected by a systematic error in the reconstruction of  $p_x$**

$$h_x = \tilde{x} - i\tilde{p}_x$$

$$\tilde{p}_{i,x} = (\tilde{x}_{i+1} - \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

assumption: no nonlinear magnets between BPMs or low amplitude

## Caveats &amp; cures when measuring nonlinear RDTs

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assumption: no nonlinear magnets between BPMs or low amplitude

**solution 1 (SPS, RHIC): combine signal from 3 BPMs to cancel out error in the reconstruction of  $p_x$ . No good when BPM phase advance multiple of  $90^\circ$  (IRs)**

## Caveats & cures when measuring nonlinear RDTs

**1. measuring nonlinear RDTs from complex C-S signal is affected by a systematic error in the reconstruction of  $p_x$**

$$h_x = \tilde{x} - i\tilde{p}_x \quad \tilde{p}_{i,x} = (\tilde{x}_{i+1} - \tilde{x}_i \cos \Delta\phi_x) / \sin \Delta\phi_x$$

assumption: no nonlinear magnets between BPMs or low amplitude

**solution 2 (ESRF): FFT on real C-S signal  $\tilde{x}$  only.  
Combined RDTs (CRDTs) can be measured**

$$F_{NS3} = 3f_{3000} - f_{1200}^* = \sum_w \frac{K_{w,2}\beta_{w,x}^{3/2}}{16} \left[ \frac{e^{-3i\Delta\phi_{x,bw}}}{1 - e^{i6\pi Q_x}} - \frac{e^{i\Delta\phi_{x,bw}}}{1 - e^{i2\pi Q_x}} \right]$$

$$\vec{F}_{NS,meas} - \vec{F}_{NS,mod} = \mathbf{M}_{NS} \Delta \vec{K}_2$$

pseudo-inverted  
(SVD)



## Caveats & cures when measuring nonlinear RDTs

### 2. Measured RDTs affected by BPM calibration errors (if unknown)

$$|f_{3000}| = \frac{H(-2,0)}{6H(1,0)^2}$$

## Caveats & cures when measuring nonlinear RDTs

### 2. Measured RDTs affected by BPM calibration errors (if unknown)

$$|f_{3000}| = \frac{H(-2,0)}{6H(1,0)^2} \quad \tilde{H}(-2,0) = \frac{H(-2,0)}{H(1,0)} = 6|f_{3000}|\sqrt{2I_x}$$

**solution 1 (SPS, RHIC):** measure calibration-free  $\tilde{H}$ ,  
 repeat measurement @ different kicker strengths, i.e.  $\sqrt{2I_x}$   
 and infer  $|f_{3000}|$  from slope of linear fit Vs  $\sqrt{2I_x}$ , i.e. tune  
 line amplitude  $H(1,0)$ .

## Caveats & cures when measuring nonlinear RDTs

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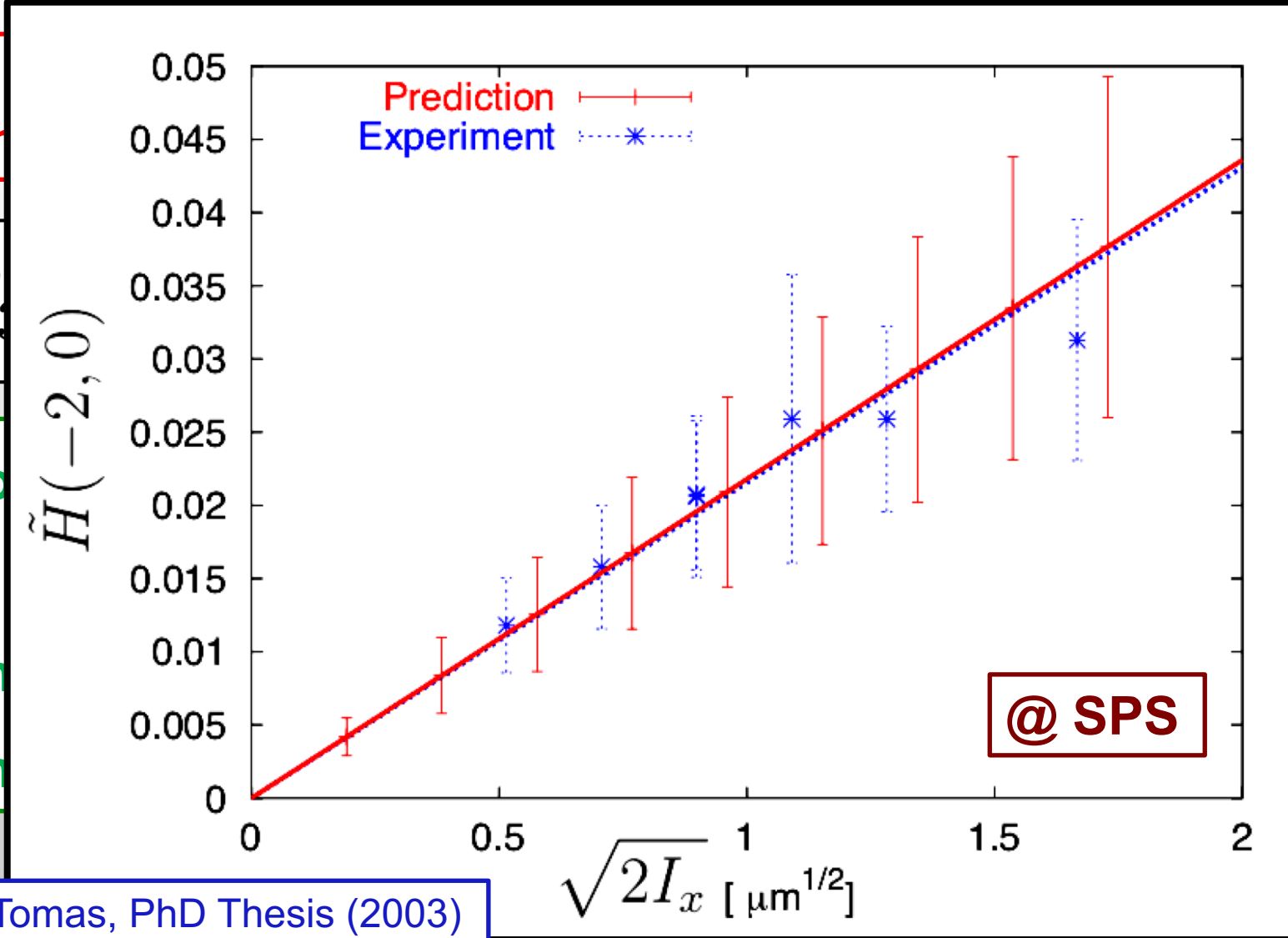
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R. Tomas, PhD Thesis (2003)

## Caveats & cures when measuring nonlinear RDTs

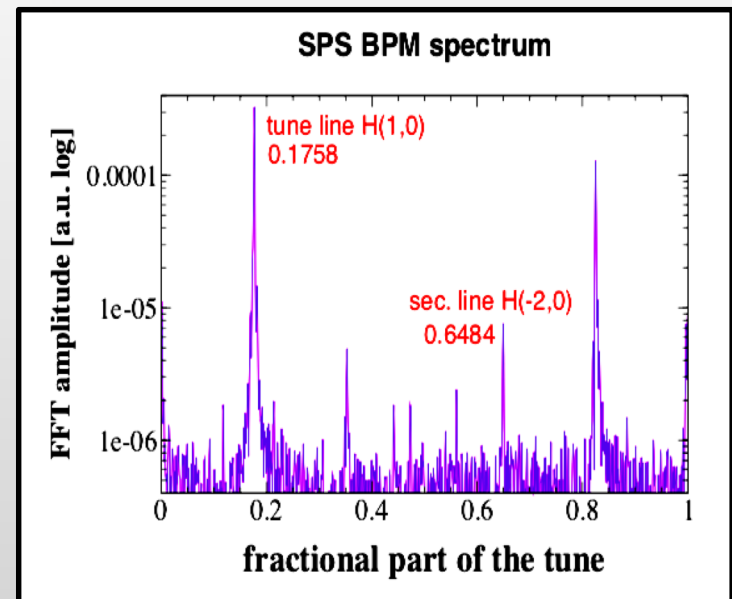
### 2. Measured RDTs affected by BPM calibration errors (if unknown)

$$|f_{3000}| = \frac{H(-2,0)}{6H(1,0)^2}$$

**solution 2 (ESRF): infer BPM calibration errors from ORM fit and use them on TbT data. Remark # 1: not significant impact @ ESRF (errors ~ 1-2%). Remark # 2: is assumes that DC calibration errors are frequency independent**

## Caveats &amp; cures when measuring nonlinear RDTs

**3. sextupole (and higher-order) spectral lines are close to the background noise for operational setting.**

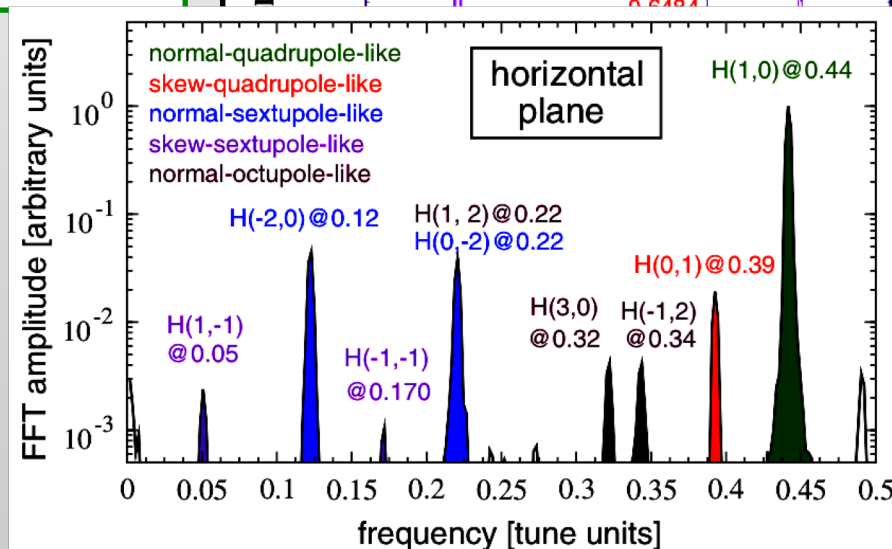
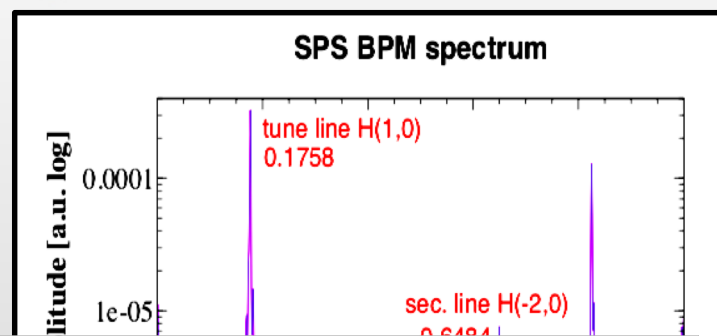


## Caveats & cures when measuring nonlinear RDTs

**3. sextupole (and higher-order) spectral lines are close to the background noise for operational setting.**

**solution (SPS & ESRF): Use modified (non-operational) sextupole setting to carry RDT measurement**

impractical @ LHC

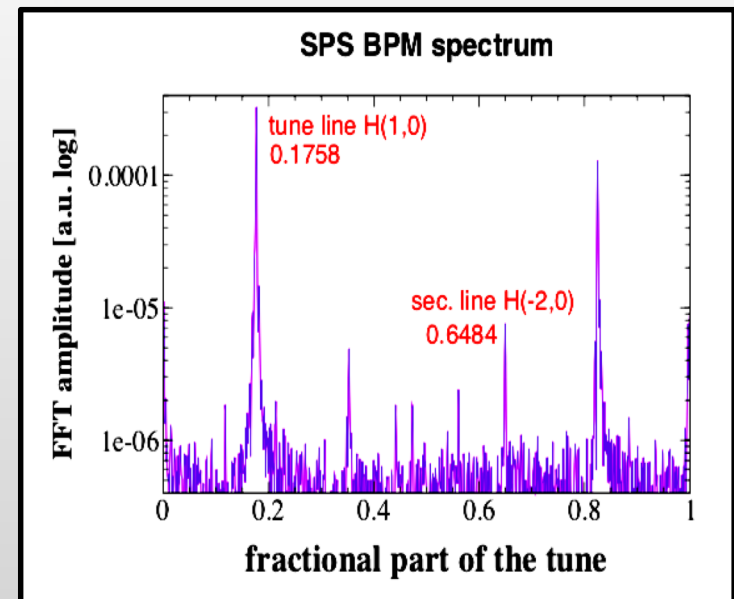


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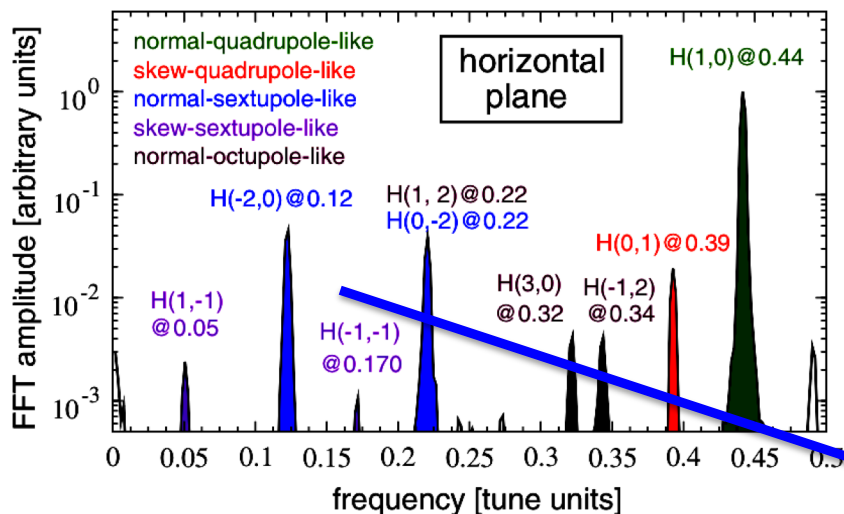
impractical @ LHC



**4. @ LHC & RHIC AC dipole is used instead of pulsed kicker: AC dipole alter the content of sextupole (and higher-order) spectral lines, theory not yet available**

## Measurement of nonlinear CRDTs @ ESRF

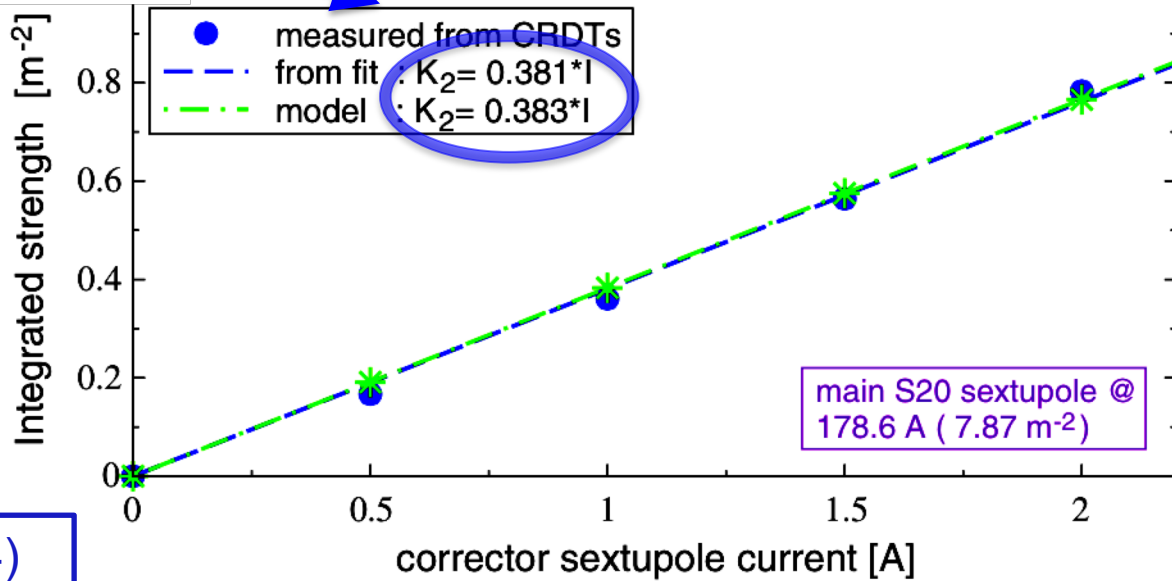
beam-based  
sextupole error model



FFT on real C-S  
signal  $\tilde{x}$  only.

$$F_{NS3} = 3f_{3000} - f_{1200}^*$$

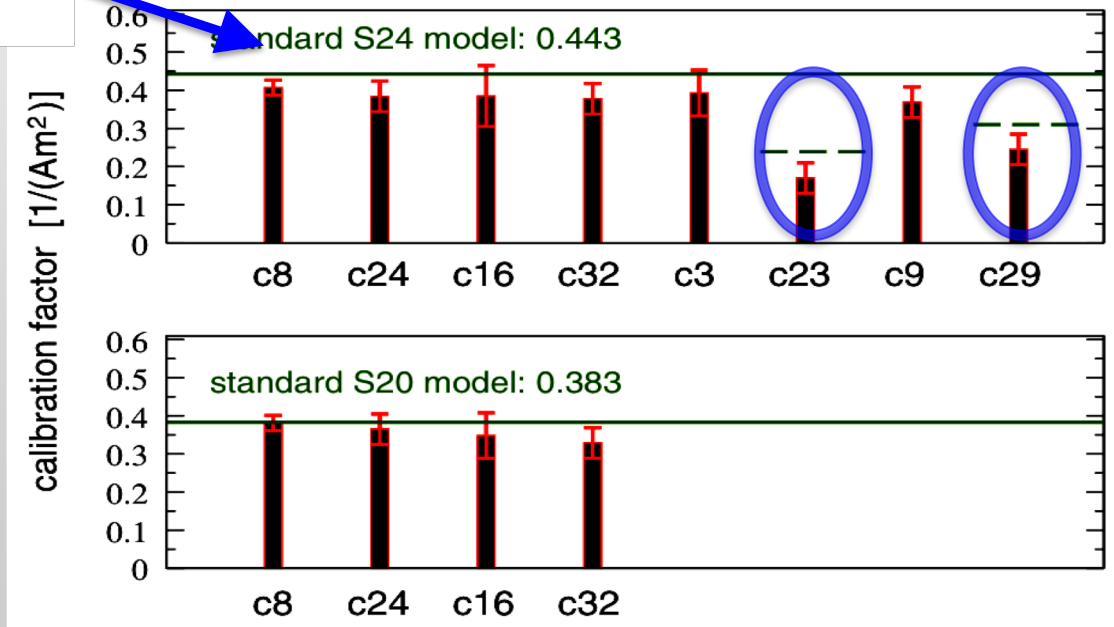
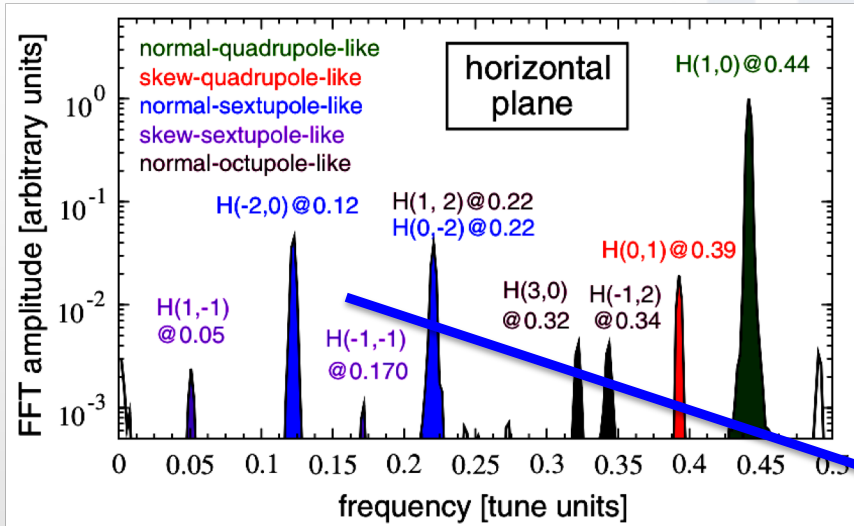
PRAB, 17, 074001 (2014)





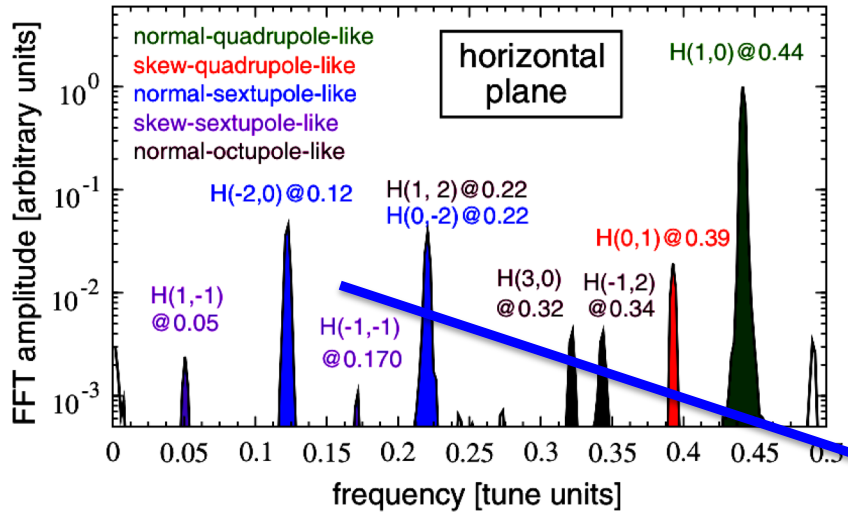
## Measurement of nonlinear CRDTs @ ESRF

beam-based  
sextupole error model

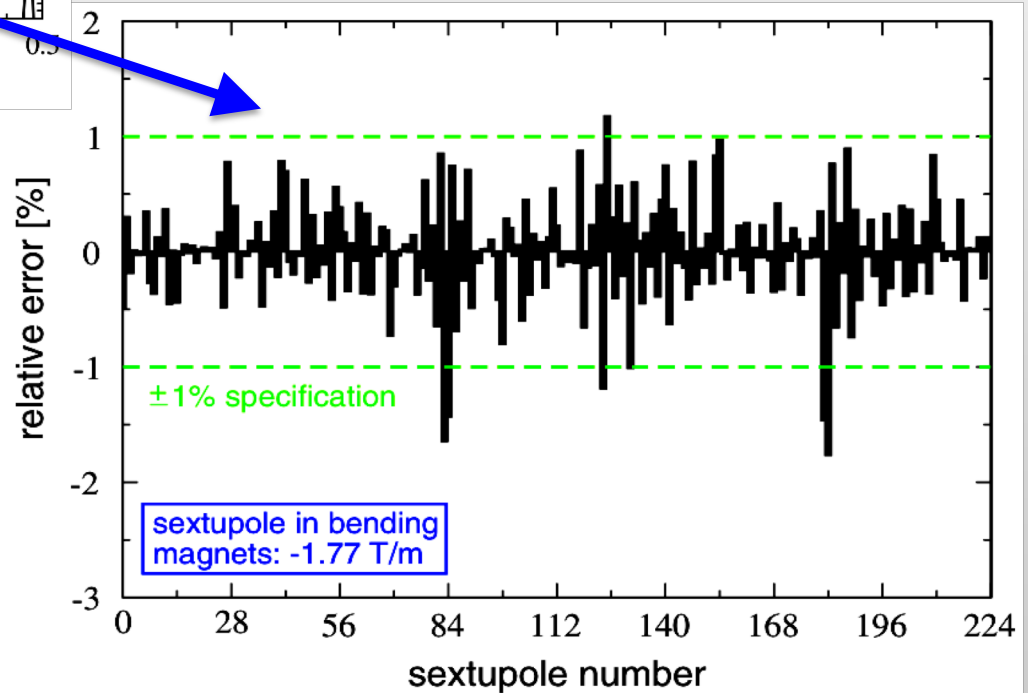


PRAB, 17, 074001 (2014)

## Measurement of nonlinear CRDTs @ ESRF



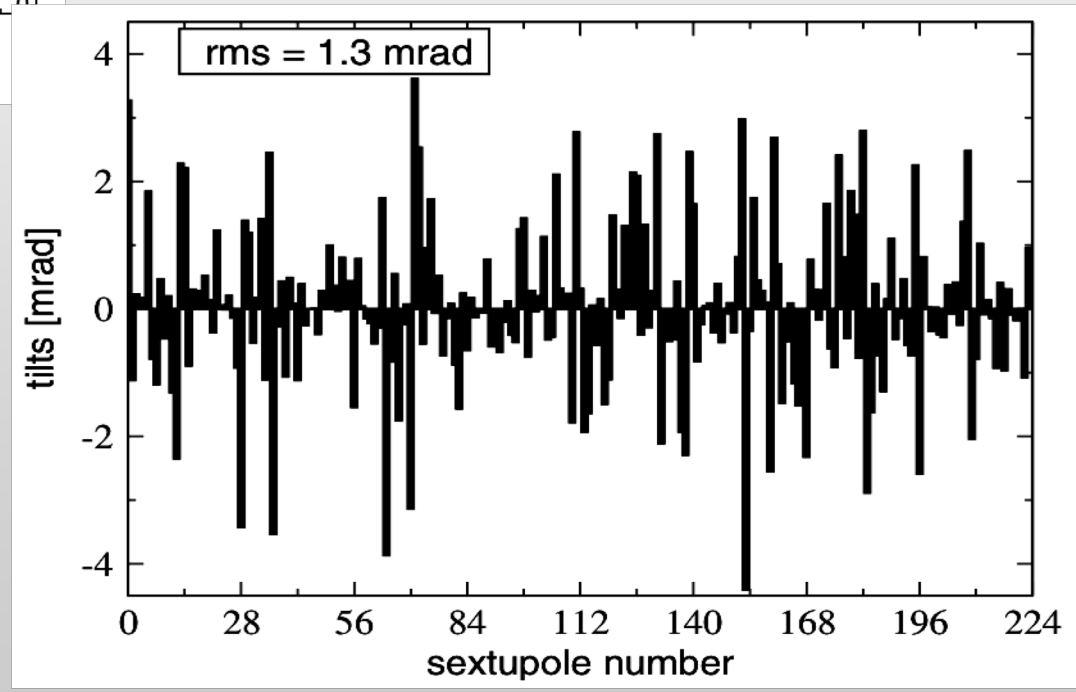
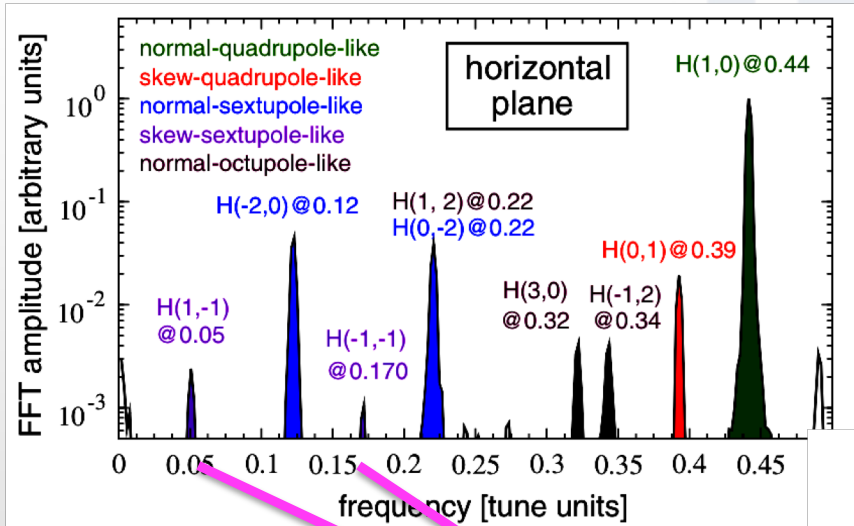
beam-based  
sextupole error model  
(strength)



PRAB, 17, 074001 (2014)

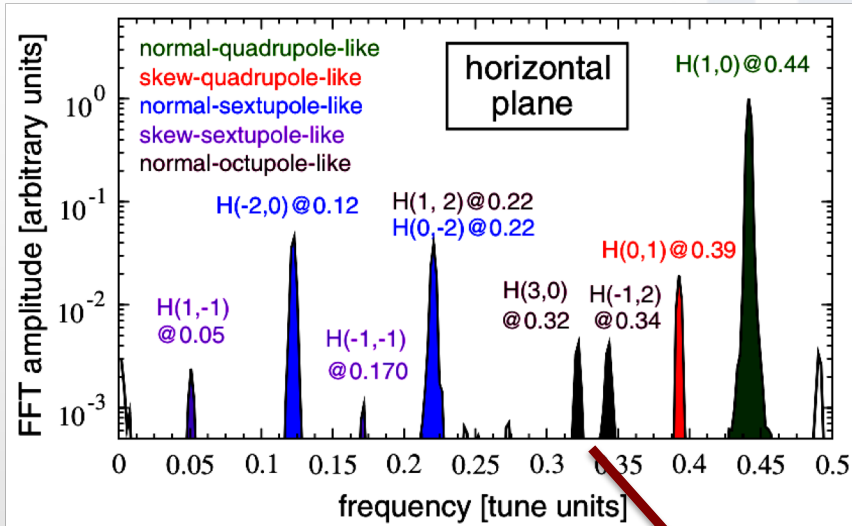
## Measurement of nonlinear CRDTs @ ESRF

beam-based  
sextupole error model  
(tilt)



PRAB, 17, 074001 (2014)

## Measurement of nonlinear CRDTs @ ESRF



beam-based  
octupolar model (in  
quads)

Quad family (average $\pm$ rms)	$K_3$ [ $\text{m}^{-3}$ ]
---------------------------------	---------------------------

QF2	$4.4 \pm 1.6$
QD3	$-6.9 \pm 0.7$
QD4	$2.5 \pm 0.8$
QF5	$-2.2 \pm 1.4$
QD6	$-0.4 \pm 2.4$
QF7	$4.0 \pm 3.3$

PRAB, 17, 074001 (2014)

## RDTs Vs chromatic functions and orbit feed-downs

The strengths of nonlinear magnets ( $K_2$ ,  $J_2$ ,  $K_3$ , ...) can be inferred “directly” from the (C)RDTs via TbT BPM data, though with all aforementioned caveats.

## RDTs Vs chromatic functions and orbit feed-downs

The strengths of nonlinear magnets ( $K_2, J_2, K_3, \dots$ ) can be inferred “directly” from the (C)RDTs via TbT BPM data, though with all aforementioned caveats.

Alternatively, their strengths can be inferred from a linear analysis (focusing & coupling) after making the beam cross the nonlinear magnets off-axis ( $\Delta x, \Delta y$ ), via feed-down fields:

$$\delta K_1 = 2(K_2 \Delta x + J_2 \Delta y)$$

$$\delta J_1 = 2(J_2 \Delta x + K_2 \Delta y)$$

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( $\Delta x, \Delta y$ ) can be generated by going off energy  $\delta p/p$  (via dispersion  $\Delta x = D_x \delta p/p$ ), with orbit bumps or controlled distortion, with crossing angle orbit @ IRs

## RDTs Vs chromatic functions and orbit feed-downs

$$\delta K_1 = 2(K_2 \Delta x + J_2 \Delta y) \qquad \delta J_1 = 2(J_2 \Delta x + K_2 \Delta y)$$

$(\Delta x, \Delta y)$  generated by going off energy  $\delta p/p$  (via dispersion  $\Delta x = D_x \delta p/p$  ).

- $\delta p/p$  error from  $\delta f_{RF}/f_{RF}$  (very accurate!) and momentum compaction (1% w.r.t. model @ ESRF)
- $D_x$  @ sextupole not observable, fit needed from data @ BPMs
- effective analysis only for chromatic sextupoles with large dispersion, not for harmonic.
- dependence of Twiss upon  $\delta p/p$ , i.e. chromatic functions and coupling as observables.



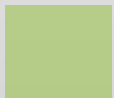
## RDTs Vs chromatic functions and orbit feed-downs

$$\frac{\partial \beta_x(j)}{\partial \delta} \simeq -\beta_x(j) + \frac{\beta_x(j)}{2 \sin(2\pi Q_x)} \sum_{m=1}^M (K_{m,1} - K_{m,2} D_{m,x}) \beta_{m,x} \cos(2\Delta\phi_{x,mj} - 2\pi Q_x)$$

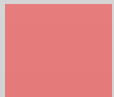
$$\frac{\partial \beta_y(j)}{\partial \delta} \simeq -\beta_y(j) - \frac{\beta_y(j)}{2 \sin(2\pi Q_y)} \sum_{m=1}^M (K_{m,1} - K_{m,2} D_{m,x}) \beta_{m,y} \cos(2\Delta\phi_{y,mj} - 2\pi Q_y)$$

$$D'_x(j) = -2D_x(j) + \frac{\sqrt{\beta_{j,x}}}{\sin(\pi Q_x)} \sum_{m=1}^M \left[ K_{m,1} - \frac{1}{2} K_{m,2} D_{m,x} \right] D_{m,x} \sqrt{\beta_{m,x}} \cos(\Delta\phi_{x,mj} - \pi Q_x)$$

$D'_y$  is a bit more complicated expression



from meas. & fit of standard on-energy ORM



from meas. & fit of 1 or 2 off-energy ORM  
the dispersive off-axis orbit across sextupoles introduces additional focusing ( $d\beta/d\delta$ ) and dispersion ( $D'$ ).

## RDTs Vs chromatic functions and orbit feed-downs

$$\frac{\partial \beta_x(j)}{\partial \delta} \simeq -\beta_x(j) + \frac{\beta_x(j)}{2 \sin(2\pi Q_x)} \sum_{m=1}^M (K_{m,1} - K_{m,2} D_{m,x}) \beta_{m,x} \cos(2\Delta\phi_{x,mj} - 2\pi Q_x)$$

to be pseudo-inverted (SVD)

$$\frac{\partial \beta_y(j)}{\partial \delta} \simeq -\beta_y(j) + \frac{\beta_y(j)}{2 \sin(2\pi Q_y)} \sum_{m=1}^M (K_{m,1} - K_{m,2} D_{m,y}) \beta_{m,y} \cos(2\Delta\phi_{y,mj} - 2\pi Q_y)$$

$$D'_x(j) = \begin{pmatrix} \frac{\partial \vec{\beta}}{\partial \delta} \\ \frac{\partial \vec{D}}{\partial \delta} \\ \frac{\partial \vec{F}_{xy}}{\partial \delta} \end{pmatrix}^{(fit)} \Rightarrow \begin{pmatrix} \vec{\beta}' \\ \vec{D}' \\ \vec{F}_{xy}' \end{pmatrix}^{(fit)} - \begin{pmatrix} \vec{\beta}' \\ \vec{D}' \\ \vec{F}_{xy}' \end{pmatrix}^{(model)} = S \begin{pmatrix} \delta \vec{K}_2^{(sext)} \\ \vec{\theta}^{(sext)} \end{pmatrix}$$

$D'_y$  is a

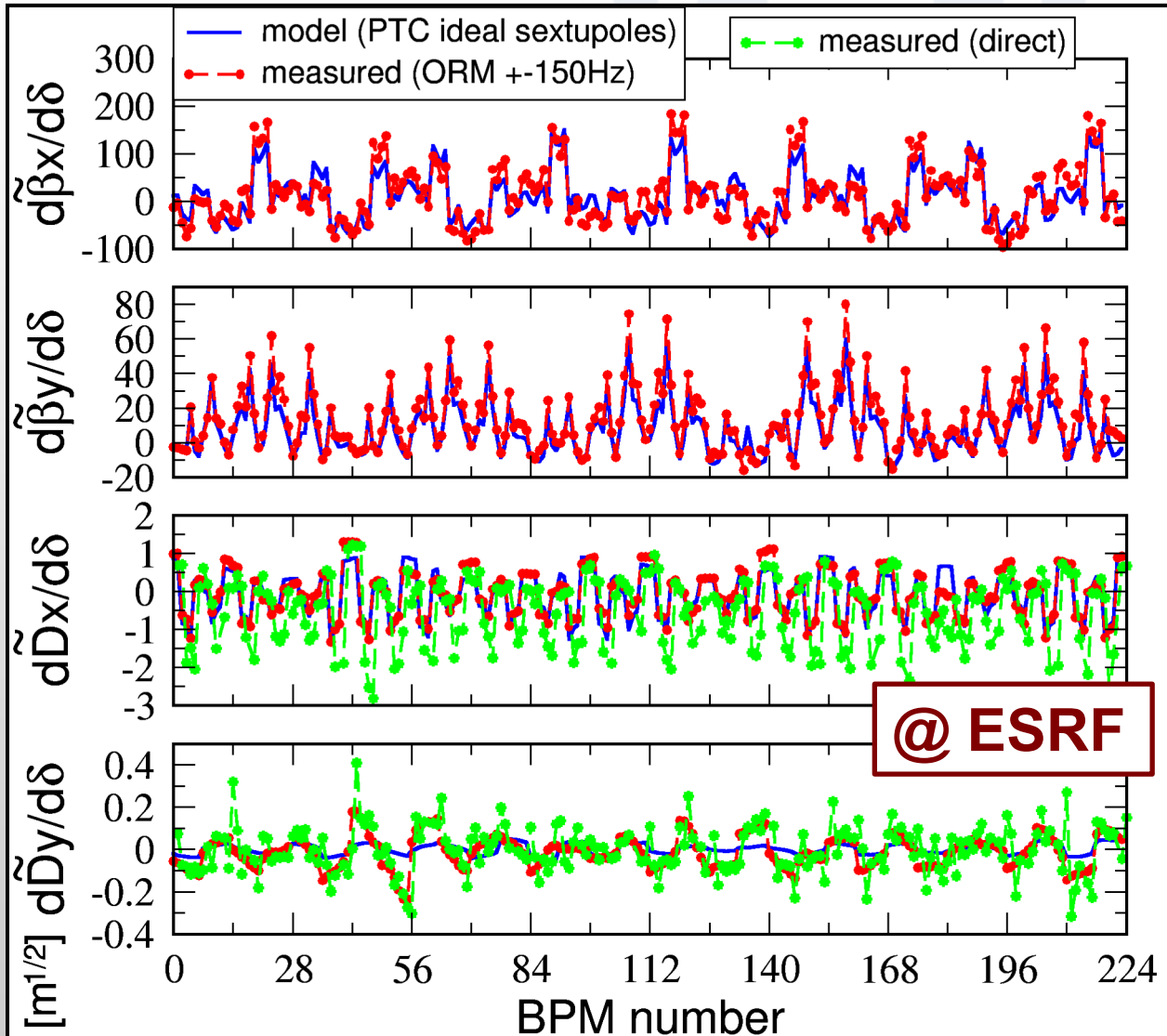
@ ESRF

from meas. & fit of standard on-energy ORM

from meas. & fit of 1 or 2 off-energy ORM

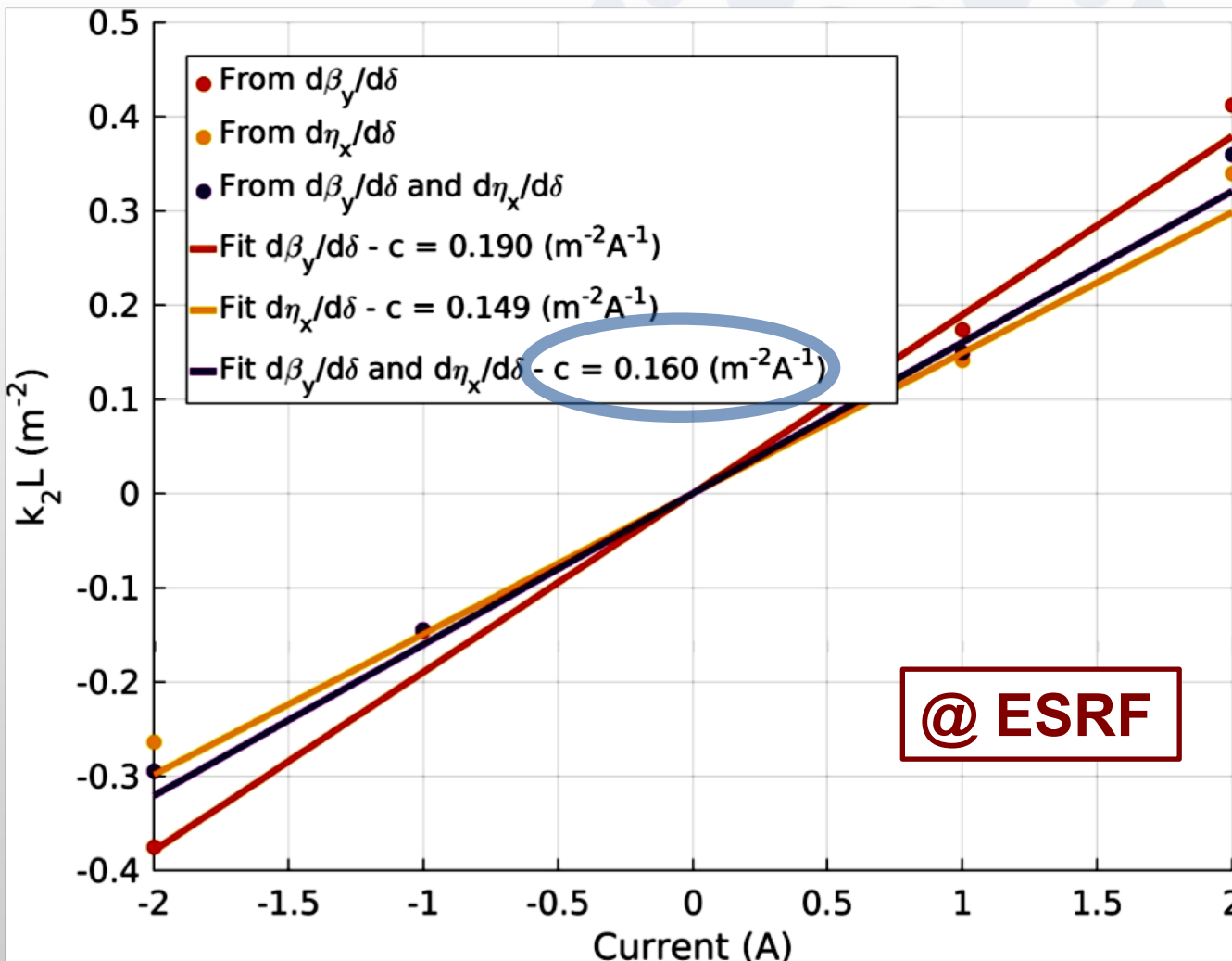
the dispersive off-axis orbit across sextupoles introduces additional focusing ( $d\beta/d\delta$ ) and dispersion ( $D'$ ).

## RDTs Vs chromatic functions and orbit feed-downs



**Sextupole  
Calibration  
from  
Chromatic  
functions  
(off-energy  
ORMs)**

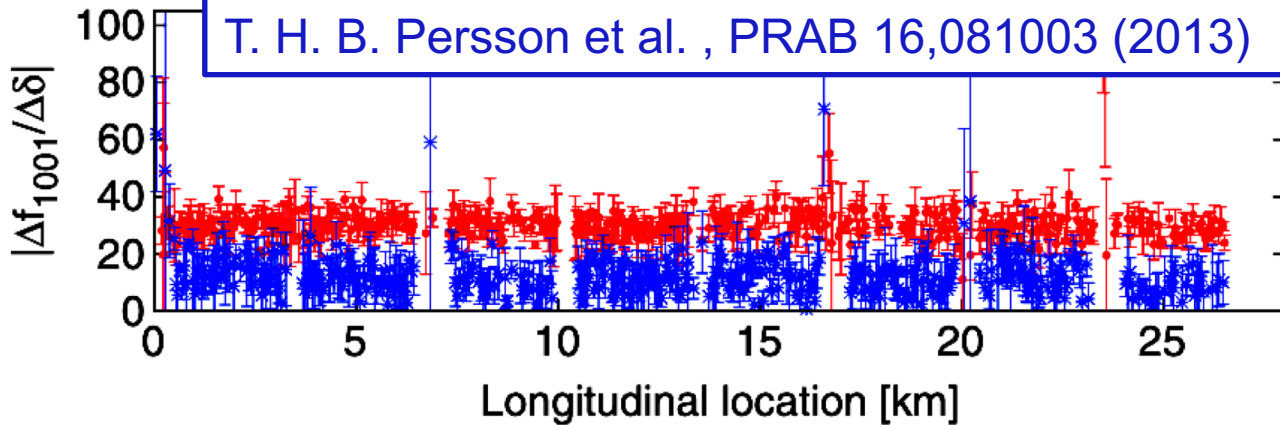
## RDTs Vs chromatic functions and orbit feed-downs



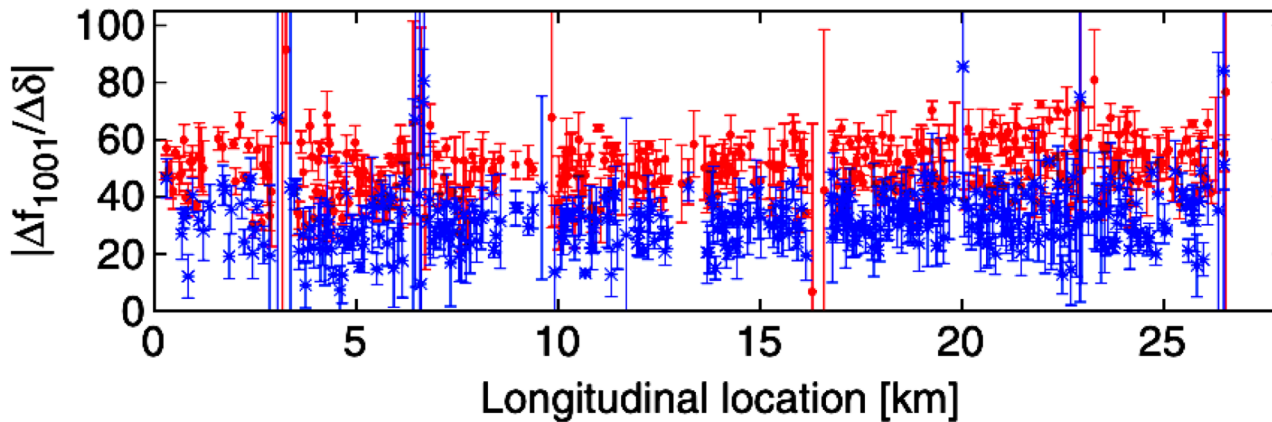
**Sextupole Calibration from Chromatic functions (off-energy ORMs)**

The calibration factor from magnetic measurements is 0.1569  $m^{-2} A^{-1}$

## RDTs Vs chromatic functions and orbit feed-downs



(a) Beam 1

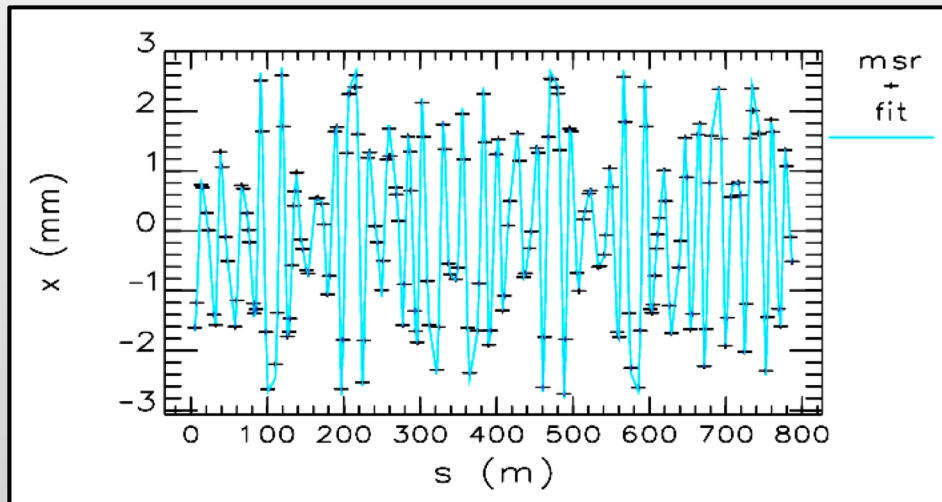


(b) Beam 2

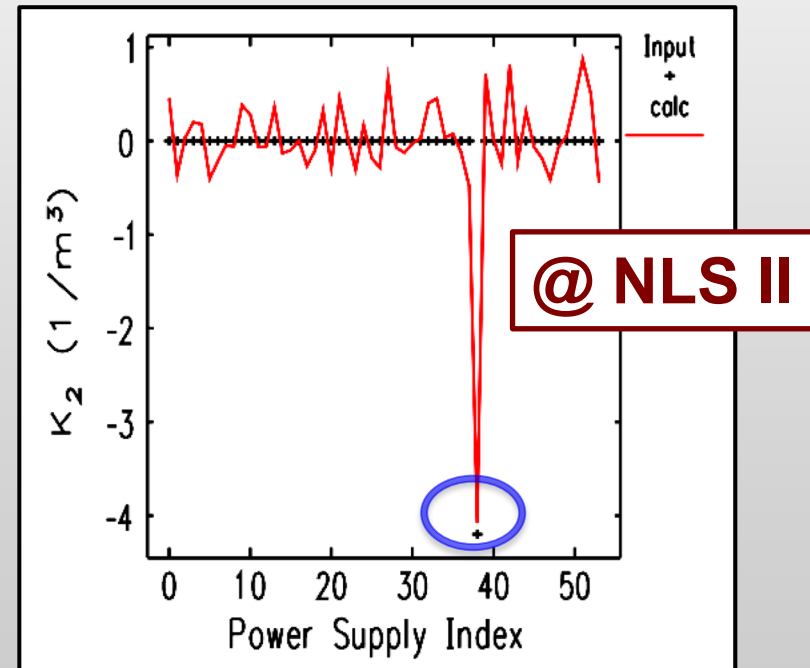
**measurment.  
& correction  
of chromatic  
coupling via  
 $\Delta f_{1001}/\Delta\delta$  &  
skew  
sextupoles  
@ LHC (TbT  
BPM data)**

## RDTs Vs chromatic functions and orbit feed-downs

- tune response to bump on sextupoles (G. Franchetti et al., PRSTAB, 11, 094001, 2008) [\*]
- betatron phase advance response to off-axis orbits @ sextupoles (W. Guo et al, PRAB 21, 081001, 2018) [\*]



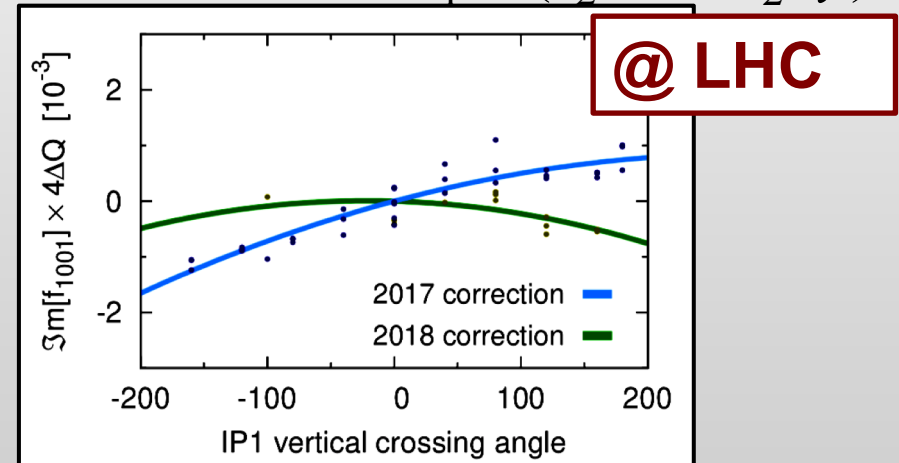
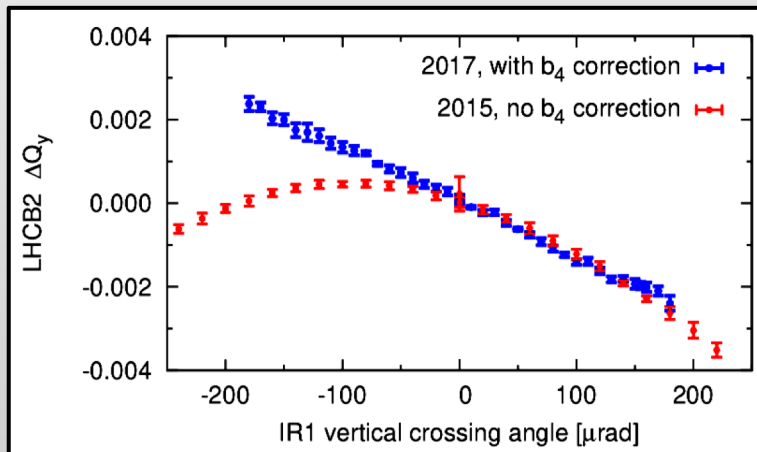
[\*] these methods may suffer from degeneracy issues (several sextupoles within an orbit bump) and no knowledge of orbit offsets ( $\Delta x, \Delta y$ ) @ sexts





## RDTs Vs chromatic functions and orbit feed-downs

- response to off-axis orbits ( $\Delta x, \Delta y$ ) on sextupoles & octupoles generated by crossing-angle schemes @ colliders' IRs (E.H. Maclean et al., CERN-ACC-2019-0029) [^]
- tune Vs crossing angle  $\delta K_1 = 2(K_2 \Delta x + J_2 \Delta y) + 3K_3(\Delta x^2 + \Delta y^2)$
- $\Delta Q_{\min}$  &  $f_{1001}$  Vs crossing angle  $\delta J_1 = 2(J_2 \Delta x + K_2 \Delta y)$



[^] goal is to correct nonlinearities @ IRs with operational  $\beta^*$  optics , not possible to use strong magnet to enhance RDTs (not used)

- Resonance Driving Terms Introductory (15')
- Linear optics errors (10')
  1. RDTs Vs beta-beating and phase advance error
  2. RDTs measurements & correction
  3. Accuracy and precision analysis
- Betatron coupling (10')
  1. RDTs measurements & correction
  2. Hadron Vs lepton machines
- Nonlinear lattice error (model) (15')
  1. Localization & detection of nonlinearities via RDTs
  2. RDTs Vs chromatic functions and orbit feed-downs





# EXTRA SLIDES



# EXTRA SLIDES

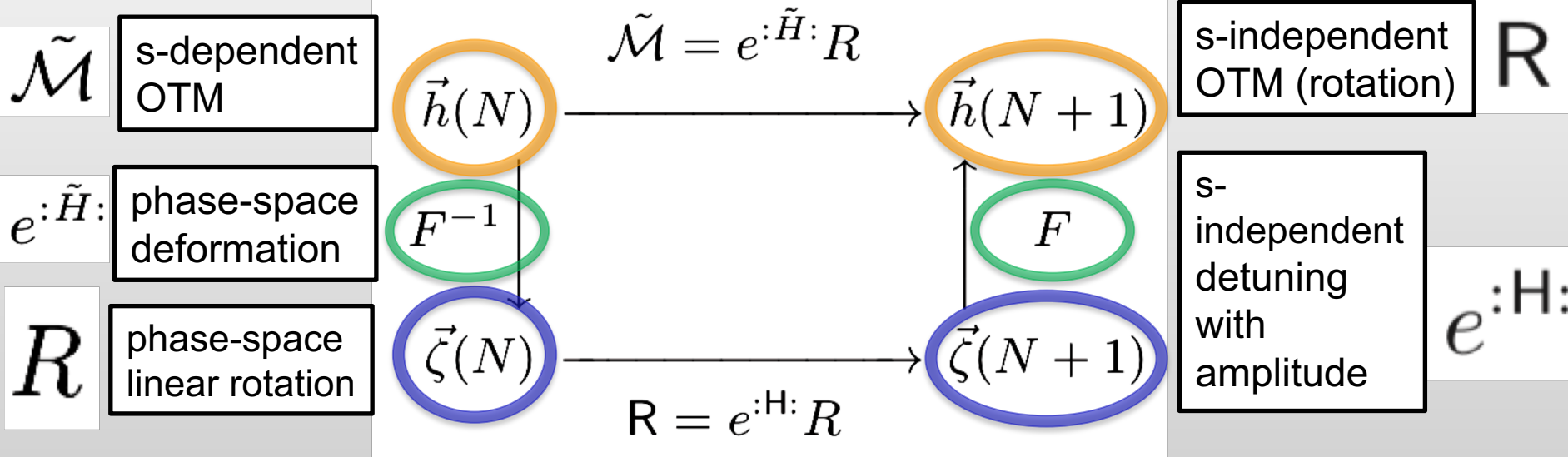
## Nonlinear one-turn map (OTM from turn $N$ to $N+1$ )

$$h_{x,\pm} = \tilde{x} \pm i\tilde{p}_x = \sqrt{2J_x} e^{\mp i(\phi_x + \phi_{x,0})}$$

complex C-S coordinates

$$\zeta_{q,\pm} = \sqrt{2I_q} e^{\mp i(\psi_q + \psi_{q,0})}$$

normal forms coordinates



$$F = \sum_{n \geq 2} \sum_{jklm}^{n=j+k+l+m} f_{jklm} \zeta_{x,+}^j \zeta_{x,-}^k \zeta_{y,+}^l \zeta_{y,-}^m$$

s-dependent normal forms transformation

## Measuring $\beta$ -beating from BPM phase advance (FFT of TbT data)

BPM phase advance = difference between the phase of the tune spectral line measured @ 2 BPMs

Castro's formula (@LEP), assumes no error between 2 BPMs

$$\beta_1^{(meas)} = \beta_1^{(mod)} \frac{\cot \Delta\phi_{21}^{(meas)} - \cot \Delta\phi_{31}^{(meas)}}{\cot \Delta\phi_{21}^{(mod)} - \cot \Delta\phi_{31}^{(mod)}}$$

Measurement error depends thus on the unknown quadrupole error. Iterations are needed

## Measuring $\beta$ -beating from BPM phase advance (FFT of TbT data)

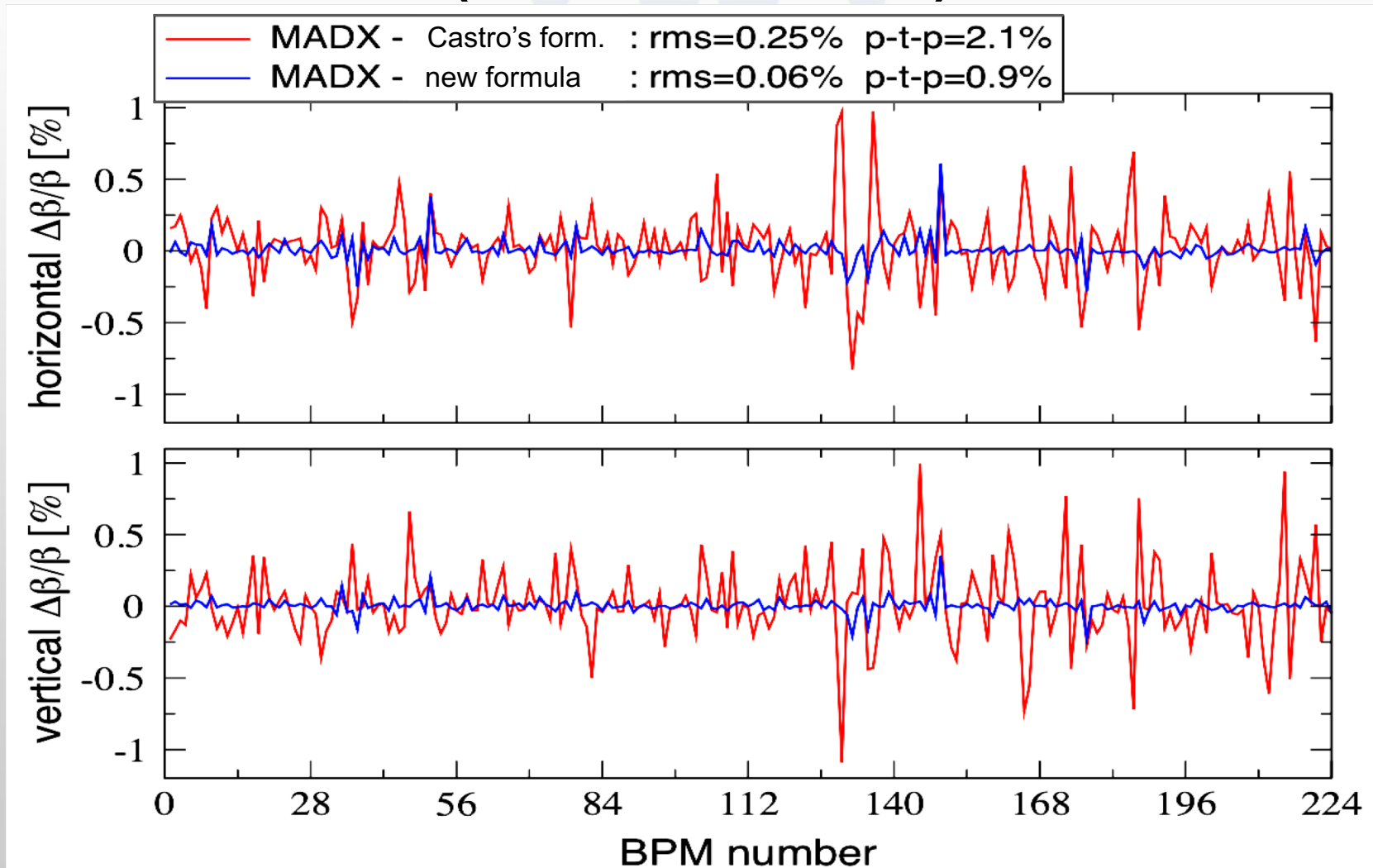
Modified Castro's formula (@ESRF, LHC) accounts for quadrupole error between 2 BPMs

$$\beta_1^{(meas)} = \beta_1^{(mod)} \frac{\cot \Delta\phi_{21}^{(meas)} - \cot \Delta\phi_{31}^{(meas)}}{\cot \Delta\phi_{21}^{(mod)} - \cot \Delta\phi_{31}^{(mod)} + (\bar{h}_{21} - \bar{h}_{31})} + O(\delta K_1^2)$$

$$\bar{h}_{ij} = \mp \frac{\sum_{j < w < i} \beta_w^{(mod)} \delta K_{w,1} \sin^2 \Delta\phi_{iw}^{(mod)}}{\sin^2 \Delta\phi_{ij}^{(mod)}}$$

not observable, though useful in simulations (HL-LHC) and to estimate measurement error

## Measuring $\beta$ -beating from BPM phase advance (FFT of TbT data)



## increasing precision in measuring $\beta$ function

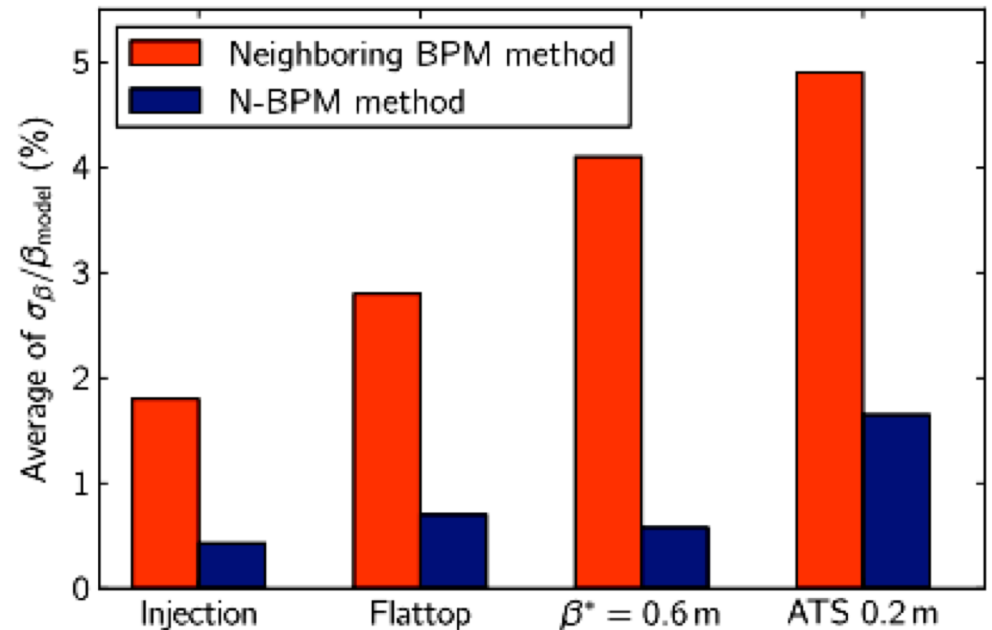
### The N-BPM method

$$\beta_1^{(meas)} = \beta_1^{(mod)} \frac{\cot \Delta\phi_{12}^{(meas)} - \cot \Delta\phi_{13}^{(meas)}}{\cot \Delta\phi_{12}^{(mod)} - \cot \Delta\phi_{13}^{(mod)}}$$

TABLE III. Systematic error of the measured  $\beta$ -function at arc BPMs for using different BPM combinations. The phase advance between consecutive BPMs is approximately  $\pi/4$ .

BPM combination	Systematic error (%)
	0.3
	0.4
	1.0
	7.1
	1.1
	1.4
	1.7
	1.8
	7.9
	22.3
	1.3
	1.9
	6.1
	1.0
	3.0
	4.5
	5.2
	1.6

### LHC 2016



## Measuring $\beta$ -beating from BPM phase advance or tune amplitude (FFT of TbT data)

$$\beta_1^{(meas)} = \beta_1^{(mod)} \frac{\cot \Delta\phi_{21}^{(meas)} - \cot \Delta\phi_{31}^{(meas)}}{\cot \Delta\phi_{21}^{(mod)} - \cot \Delta\phi_{31}^{(mod)}}$$

$$\Delta\Phi_{ij} = \Delta\phi_{ij} + \delta\phi_{ij}^{(tim)}$$

model & BPM synchronization \*  
dependent

BPM calibration  $\varepsilon$  independent

$$\beta_{x,j}^{(meas)} = \beta_{x,j}^{(mod)} \left( \frac{|H(1,0)_j|}{\langle |H(1,0)| \rangle} \right)^2 + O(\varepsilon_x, |f_{2000}|^2)$$

\*: @ ESRF 0.1  $\mu$ s p-t-p over  
2.82  $\mu$ s revolution time

model & BPM synchronization  
independent

BPM calibration  $\varepsilon$  dependent



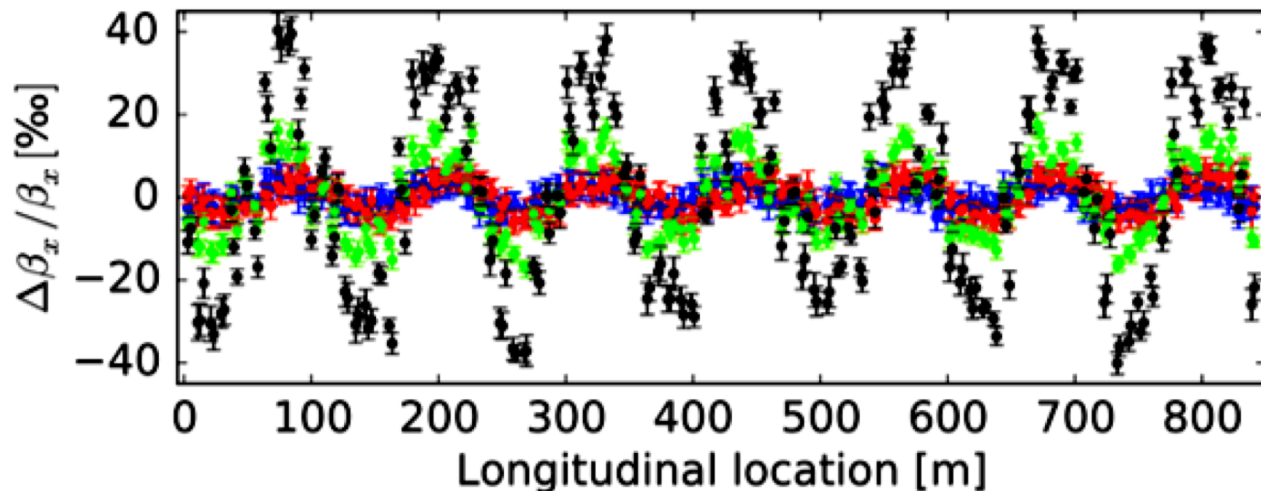
## Kick Amplitude

**artificial  $\beta$ -beating  
from TbT data**

- Limited by non-linearities – simulation

$$\beta_1^{(meas)} = \beta_1^{(mod)} \frac{\cot \Delta\phi_{12}^{(meas)} - \cot \Delta\phi_{13}^{(meas)}}{\cot \Delta\phi_{12}^{(mod)} - \cot \Delta\phi_{13}^{(mod)}}$$

The measured BPM  
phase advance  
=  
betatron BPM  
phase advance +  
non-linear terms



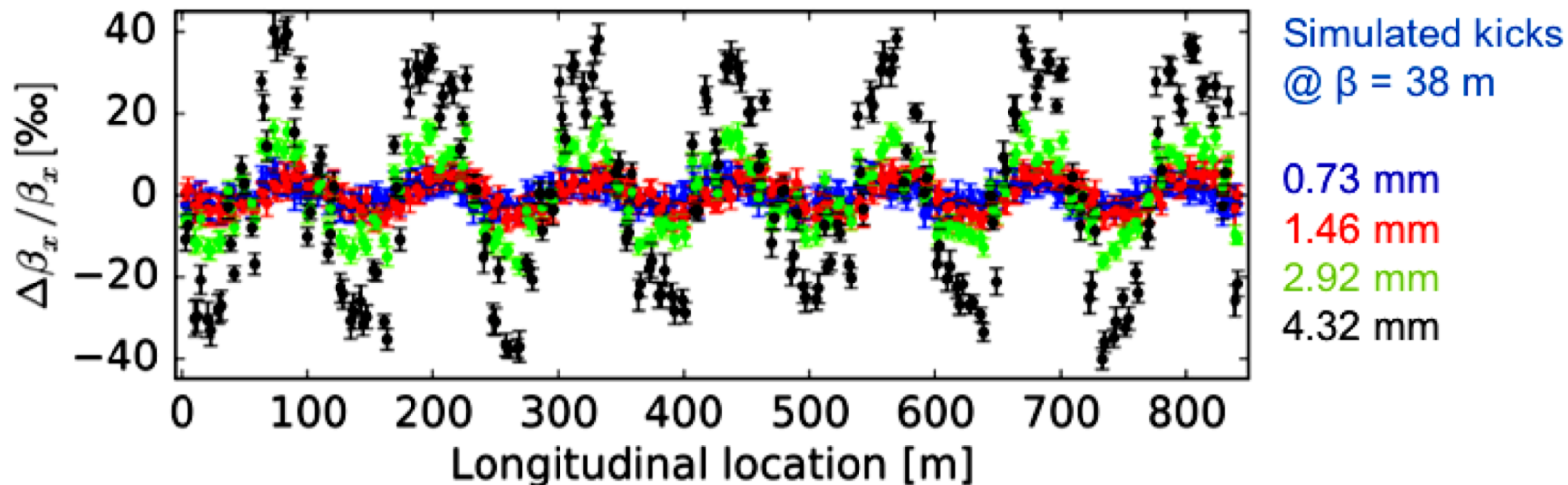
Simulated kicks  
@  $\beta = 38$  m

0.73 mm  
1.46 mm  
2.92 mm  
4.32 mm

## Kick Amplitude

**artificial  $\beta$ -beating  
from TbT data**

- Limited by non-linearities – simulation
- However has to be high enough
  - with respect to BPM resolution
  - Decoherence and number of turns



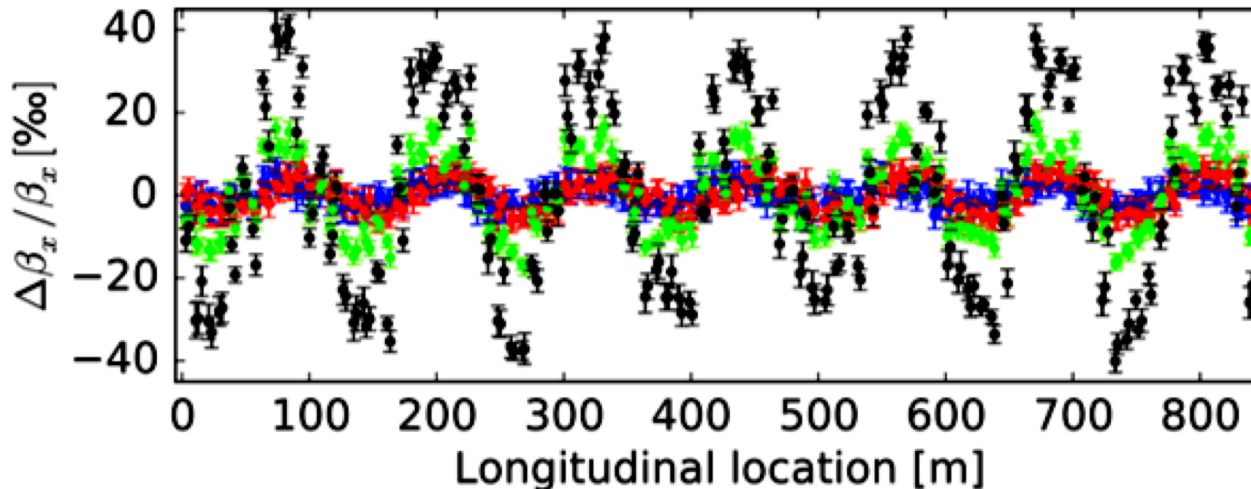
## Kick Amplitude

**artificial  $\beta$ -beating  
from TbT data**

- Limited by non-linearities – simulation
- However has to be high enough
  - with respect to **BPM resolution**
  - Decoherence and number of turns

Libera BPMs

~10  $\mu\text{m}/\sqrt{\text{Hz}}$  (TbT, 353 kHz)  
Vs  
~10  $\text{nm}/\sqrt{\text{Hz}}$  (ORM, 10 Hz  
aqn)



Simulated kicks  
@  $\beta = 38$  m

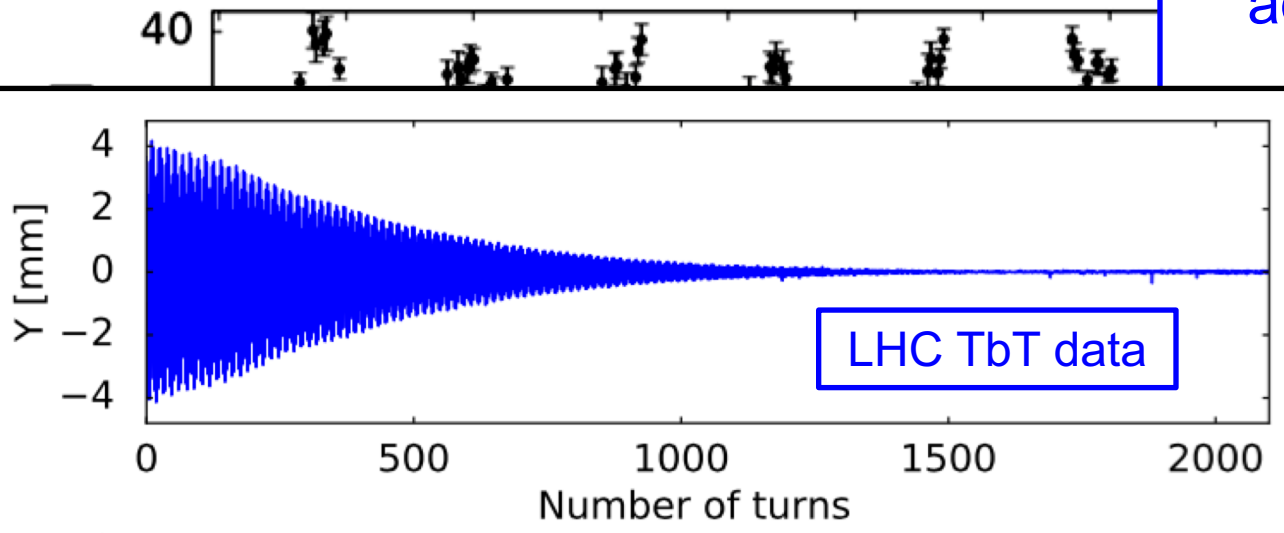
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## Kick Amplitude

**artificial  $\beta$ -beating  
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The measured BPM  
phase advance  
=  
betatron BPM phase  
advance + **non-linear  
terms**



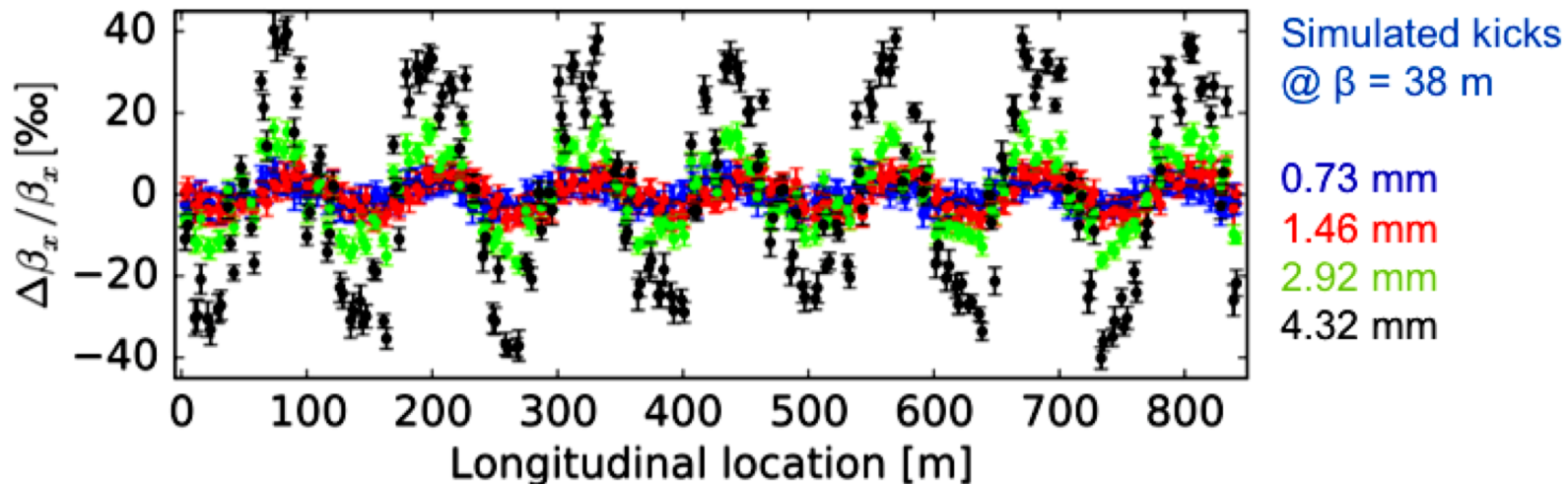
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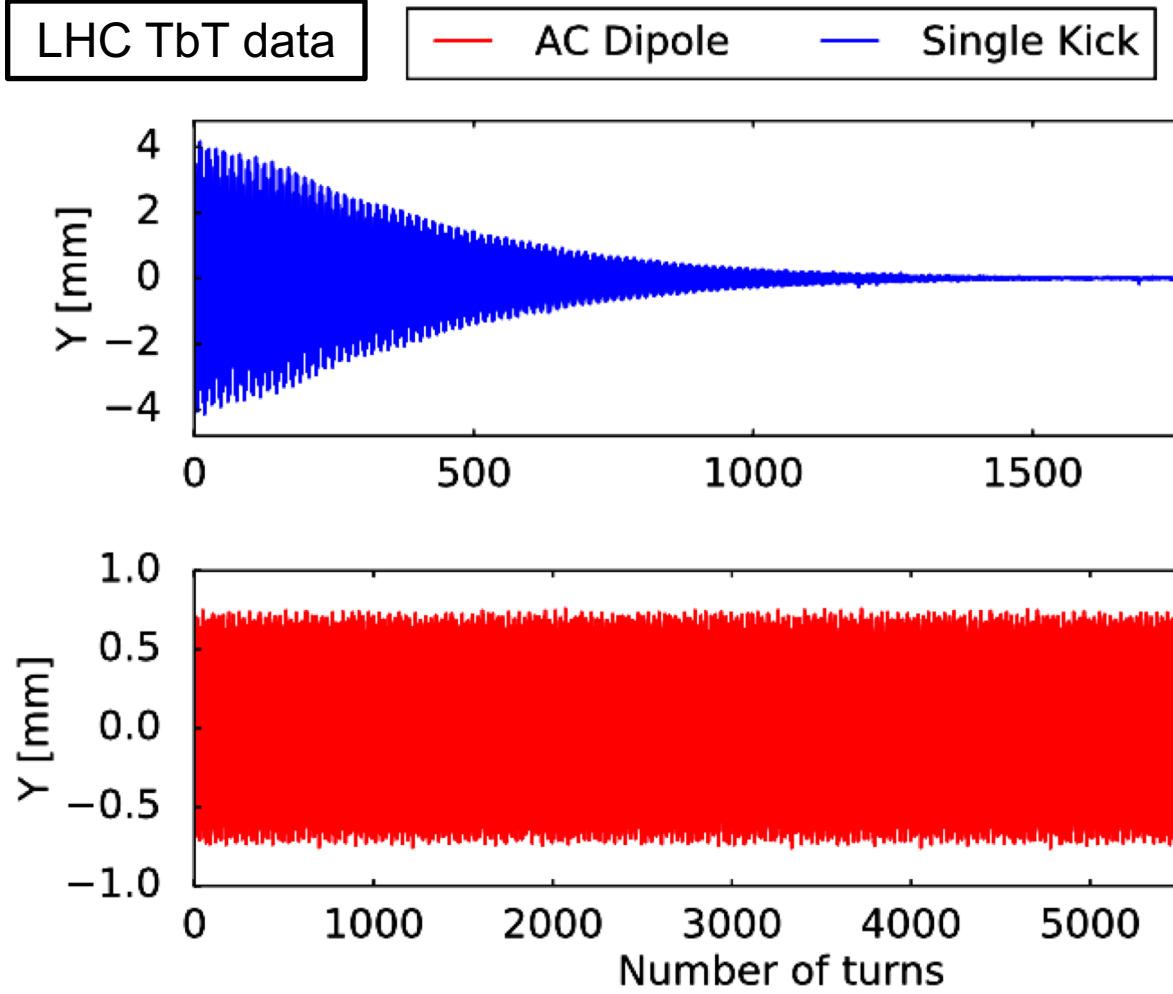
artificial  $\beta$ -beating  
from TbT data

- Limited by non-linearities – simulation
- However has to be high enough
  - with respect to BPM resolution
  - Decoherence and number of turns

$\sim 1/N^2$  (TbT)



## a possible way out: the AC dipole



- long TbT signal good for cleaning before harmonic analysis => **greater spectral res.**
- low excitation amplitude => **non-linearities avoided**
- **no emittance blowup**
- perturbations from AC dipole to be accounted for



